

December 2022

Cottonwood River Watershed Total Maximum Daily Load Report

Watershed-wide TMDLs covering TSS, *E. coli*, and lake nutrient impairments in the Cottonwood River Watershed, located in the greater Minnesota River Basin



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Photo location: Redwood River near Redwood Falls, MN

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Acronyms

1W1P	One Watershed, One Plan
AF	Anoxic factor
AFO	Animal Feeding Operation
AU	animal unit
BMP	best management practice
BWSR	Board of Water and Soil Resources
CAFO	Concentrated Animal Feeding Operation
cfu	colony-forming unit
chl- <i>a</i>	chlorophyll-a
CLP	curly-leaf pondweed
CREP	Conservation Reserve Enhancement Program
CRP	Conservation Reserve Program
DEM	Digital Elevation Model
DO	dissolved oxygen
DMR	discharge monitoring report
DNR	Minnesota Department of Natural Resources
<i>E. coli</i>	Escherichia coli
EPA	U.S. Environmental Protection Agency
FTPGW	fail to protect groundwater
HSPF	Hydrologic Simulation Program-Fortran
HUC	Hydrologic Unit Code
IBI	Index of Biotic Integrity
ITPHS	imminent threat to public health and safety
IWM	intensive watershed monitoring
km ²	square kilometer
LA	load allocation
Lb	pound
lb/yr	pounds per year
LDC	Load Duration Curve
LGU	Local Government Unit

LIDAR	Light Detection and Ranging
LWG	Local Work Group
m	meter
MAWQCP	Minnesota Agricultural Water Quality Certification Program
MDA	Minnesota Department of Agriculture
MDH	Minnesota Department of Health
mg/L	milligrams per liter
mL	milliliter
MMP	Manure Management Plan
MOS	Margin of Safety
MPCA	Minnesota Pollution Control Agency
MS4	Municipal Separate Storm Sewer System
NLCD	National Land Cover Database
NMI	Nutrient Management Initiative
NPDES	National Pollutant Discharge Elimination System
NRCS	Natural Resources Conservation Service
NTU	nephelometric turbidity units
PFA	Public Facilities Authority
PWP	Permanent Wetland Preserve
RCRCA	Redwood Cottonwood River Control Area
RIM	Reinvest in Minnesota
RR	release rate
S-tube	Secchi tube
SAV	submerged aquatic vegetation
SDS	State Disposal System
SID	Stressor Identification
SONAR	Statement of Need and Reasonableness
SRO	surface runoff
SSTS	Subsurface Sewage Treatment Systems
SWCD	Soil and Water Conservation District
SWPPP	Stormwater Pollution Prevention Plan

TALU	tiered aquatic life uses
TMDL	total maximum daily load
TP	total phosphorus
TSS	total suspended solids
µg/L	microgram per liter
WASCOB	Water and Sediment Control Basin
WCBP	Western Cornbelt Plain
WLA	wasteload allocation
WRAPS	Watershed Restoration and Protection Strategy
WRP	Wetland Reserve Program
WWTP	wastewater treatment plant

Executive Summary

Cottonwood River Watershed Approach

Intensive watershed monitoring (IWM) and stressor identification (SID) were completed between 2017 and 2020 for the Cottonwood River Watershed, which is located in the Minnesota River Basin (MPCA 2020c). Seventy river/stream reaches were assessed for their ability to support aquatic life and/or aquatic recreation. Of the assessed river/stream reaches, 19 were fully supporting of aquatic life and none fully supported aquatic recreation due to high bacterial levels. Of the 25 lakes assessed in the Cottonwood River Watershed, 5 were determined to be impaired by nutrients (total phosphorus [TP]). In addition, Double and Rock Lakes were assessed for fish Index of Biotic Integrity (IBI) and were determined to not be meeting standards (DNR 2021). Based on previous and current monitoring assessment data, there are 11 turbidity (total suspended solids [TSS]) impaired river/stream reaches, 16 bacteria impaired river/stream reaches, 26 macroinvertebrates IBI impaired river/stream reaches, and 13 fish IBI impaired river/stream reaches within the Cottonwood River Watershed. For the remainder of this Total Maximum Daily Load (TMDL) report, the river/stream reach(es) will be referred to as just “reach(es)”.

Overview of this TMDL

A TMDL represents the total mass of a pollutant that can be assimilated by the receiving water without causing that receiving water to violate water quality standards. This TMDL is a continuation of previously completed TMDLs in the Cottonwood River Watershed that have been approved by the U.S. Environmental Protection Agency (EPA) Region 5. The Cottonwood River Fecal Coliform TMDL Report (RCRCA 2013) was approved in January 2014. Prior to the fecal coliform TMDL, the State of Minnesota submitted a state-wide TMDL to address mercury in fish, which included nine reaches in the Cottonwood River Watershed, which was approved in March 2007 (MPCA 2007a).

This TMDL addresses 11 turbidity/TSS impaired reaches, 8 bacteria impaired reaches, and 7 nutrient impaired lakes in the Cottonwood River Watershed. Twenty-six macroinvertebrate IBI impaired reaches and 13 fish IBI impaired reaches in the Cottonwood River Watershed are not addressed in this TMDL and will be deferred because the water quality chemistry data was insufficient or because multiple stressors that cannot be quantified were identified. However, these reaches will be addressed through implementation of the Cottonwood River Watershed Restoration and Protection Strategies (WRAPS) Report and local water planning efforts. Addressing multiple impairments in this TMDL is consistent with Minnesota’s Water Quality Framework that seeks to develop watershed-wide protection and restoration strategies, rather than focusing on individual reach impairments.

Turbidity/Total Suspended Solids Impairments

In 2014, Minnesota adopted new water quality standards for TSS that replaced the turbidity standard. The turbidity and TSS TMDLs in this report were developed using the TSS standard.

Hydrologic Simulation Program – Fortran (HSPF) simulated flow and TSS output were used to establish load duration curves (LDCs) for the 11 turbidity/TSS impairments covered in this TMDL. The curve displays the Class 2B TSS standard of 65 mg/L. A TMDL, which includes the wasteload allocations (WLAs), load allocations (LAs), and margin of safety (MOS), was established for five flow zones along the flow duration curve: very high, high, mid, low, and very low flow conditions. Sediment sources were assessed

for the turbidity/TSS impaired reaches which indicates loading is primarily driven by near-channel sources (i.e., bed, bank, ravine erosion) and upland erosion. Implementation activities will include upland best management practices (BMPs) to reduce soil erosion in highly erodible cropland areas, and restoring and increasing water storage opportunities throughout the watershed to decrease peak discharge rates.

Bacteria (*E. coli*) Impairments

HSPF-simulated flow and monitored bacteria data for the eight bacteria-impaired reaches were used to establish LDCs. The curves were set to meet the *Escherichia coli* (*E. coli*) standard of no more than 126 organisms per 100 mL. TMDLs that include WLAs, LAs, and MOS for the bacteria-impaired reaches were established for the five flow zones described in the previous paragraph. A bacteria source assessment exercise indicates livestock is by far the largest producer of bacteria in the bacteria impaired reach watersheds. However, monitoring data also suggests exceedances during low-flow conditions, suggesting failing subsurface sewage treatment systems (SSTSs) and/or livestock animals in the stream corridors are important sources during certain hydrologic conditions. Implementation activities will need to focus on feedlot and pasture BMPs, livestock exclusion from waterways, and SSTS upgrades.

Lake Nutrient Impairments

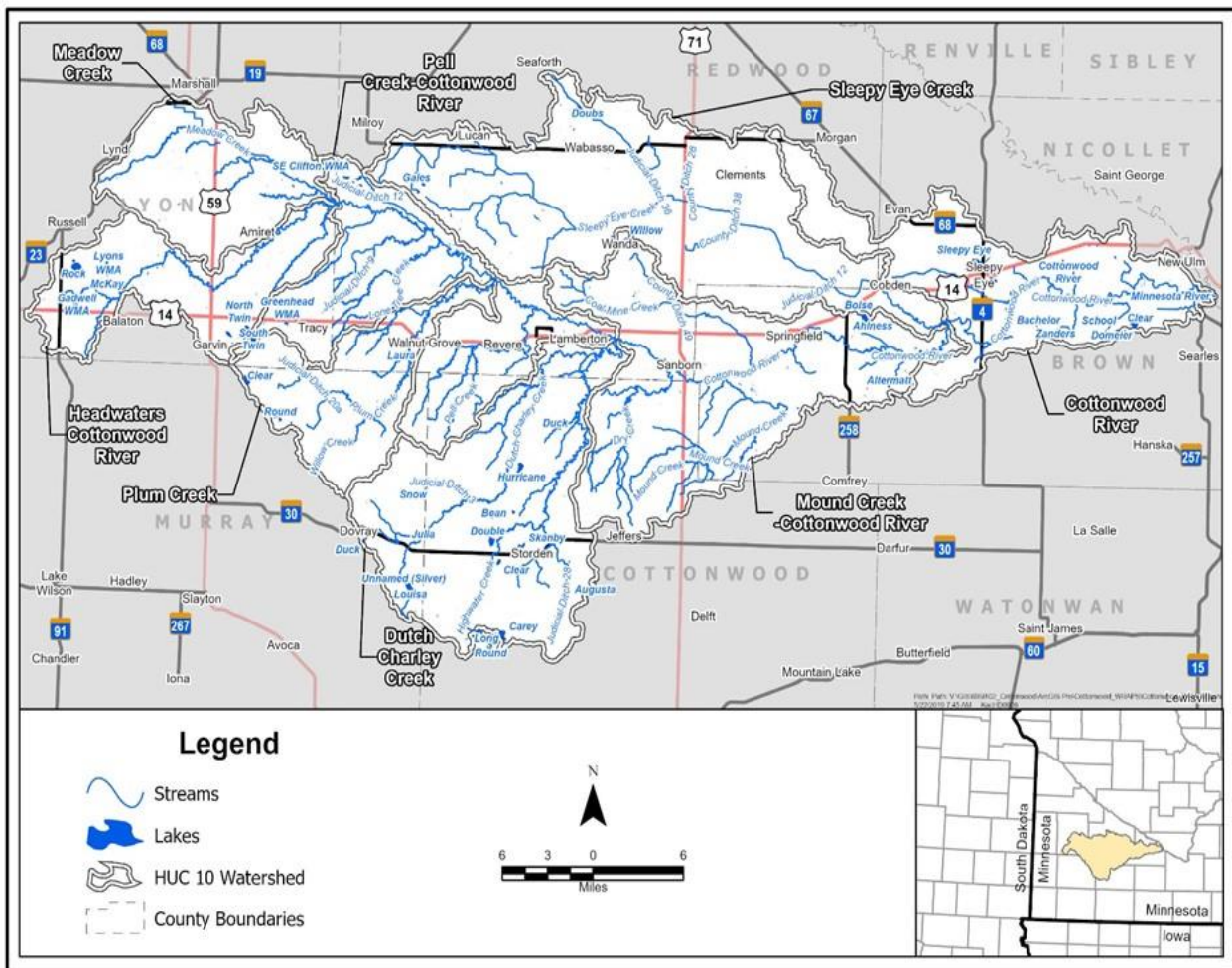
Nutrient budgets and lake response models were developed for the seven nutrient-impaired lakes in the Cottonwood River Watershed covered in this TMDL. The HSPF model was used along with in-lake monitoring data to develop nutrient budgets for each lake and set up the lake response models and TMDL equations. Pollutant source assessment for these lakes indicates all the lakes require phosphorus reductions from both internal and external (watershed) sources. For some of the lakes, internal load is a significant source of phosphorus and in-lake efforts will be important to achieve water quality standards. Watershed implementation activities will need to focus on upland BMPs to prevent phosphorus delivery to the lake. Internal load reductions will need to come from in-lake management activities such as rough fish management, alum treatment, and/or aquatic plant management. Sleepy Eye Lake (08-0045-00) was de-listed from the State's 303(d) impaired waters list in 2020 due to improved water quality conditions since it was listed as impaired in 2002. Implementation efforts included septic upgrades, sediment control practices, education, and lake dredging. Since the de-listing occurred during the development of this TMDL study, this report does not include the results of the draft TMDL for Sleepy Eye Lake. However, the lake has been identified by local stakeholders as a high priority for protection in the Cottonwood River WRAPS Report. Additionally, some of the supporting items that were developed for the Sleepy Eye Lake draft TMDL prior to its de-listing can be found in Appendix B of this TMDL.

1. Project Overview

1.1 Purpose

This TMDL addresses 11 turbidity/TSS impairments, 8 bacteria (*E. coli*) impairments, and 7 lake nutrient (phosphorus) impairments in the Cottonwood River Watershed. The drainage areas of the impaired reaches and lakes presented in this TMDL cover portions of five counties in southwest Minnesota: Lyon, Murray, Redwood, Cottonwood, and Brown (Figure 1). The largest cities in the watershed include New Ulm (population 13,362), Marshall (population 12,432), Sleepy Eye (population 3,498), Tracy (population 2,110), and Springfield (population 1,193). Other cities/townships in the watershed include Lamberton, Walnut Grove, Westbrook, and others.

Figure 1. Cottonwood River Watershed overview.



The goal of this TMDL is to quantify the pollutant reductions needed to meet state water quality standards for TSS and phosphorus for the reaches and lakes listed in Table 1 and shown in Figure 2. This TMDL is established in accordance with Section 303(d) of the Clean Water Act and provides WLAs and LAs for the watershed areas as appropriate.

Table 1. List of stream and lake impairments addressed in Cottonwood River Watershed TMDL.

Affected use: Pollutant/ Stressor	Reach/Lake ID	Reach/Lake name	Reach/Lake description	Designated use class	Listing year	Target Start/ Completion
Aquatic Life: Turbidity/TSS	07020008-502	Cottonwood River	Headwaters to Meadow Creek	2B	2020	2019/2022
	07020008-504	Cottonwood River	Plum Creek to Dutch Charley Creek	2B	2006	
	07020008-508	Cottonwood River	Coal Mine Creek to Sleepy Eye Creek	2B	2006	
	07020008-509	Cottonwood River	Sleepy Eye Creek to JD 30	2B	2020	
	07020008-517	Dutch Charley Creek	Highwater Creek to Cottonwood River	2B	2006	
	07020008-518	Dutch Charley Creek	Headwaters to Highwater Creek	2B	2006	
	07020008-519	Highwater Creek	Double Lake outlet to Dutch Charley Creek	2B	2020	
	07020008-535	Pell Creek	Headwaters to T109 R38W S29, east line	2B	2010	
	07020008-599	Sleepy Eye Creek	T109 R33W S5, west line to Cottonwood River	2B	2006	
	07020008-602 & 603 ¹	Plum Creek (JD 20A)	Headwaters to -95.576 44.177; -95.576 44.177 to Cottonwood River	2B	2006	
Aquatic Recreation: <i>E. coli</i>	07020008-502	Cottonwood River	Headwaters to Meadow Creek	2B	2020	2019/2022
	07020008-511	Judicial Ditch 30	T110 R32W S31, west line to Cottonwood River	7	2020	
	07020008-519	Highwater Creek	Double Lk outlet to Dutch Charley Creek	2B	2020	
	07020008-520	Dry Creek	T108 R36W S31, south line to Cottonwood River	2B	2020	
	07020008-521	Mound Creek	Headwaters to Cottonwood River	2B	2020	
	07020008-523	Pell Creek	T109 R37W S30, west line to Cottonwood River	2B	2020	
	07020008-604	Coal Mine Creek	Headwaters to T109 R35W S22, south line	2B	2020	
	07020008-609	Judicial Ditch 30	T110 R33W S15, west line to T110 R33W S36, east line	2B	2020	
Aquatic Recreation: Lake Nutrients	17-0054-00	Lake Bean	Sec. 14, T107 N., R38 W	2B	2010	2019/2022
	17-0056-01	Double (North Portion)	Sec. 23, T107 N., R38 W	2B	2010	

Affected use: Pollutant/ Stressor	Reach/Lake ID	Reach/Lake name	Reach/Lake description	Designated use class	Listing year	Target Start/ Completion
	42-0052-00	Rock Lake	Sec. 5 and 6, T. 109 N., R42 W	2B	2010	
	08-0011-00	Clear Lake	Sec. 11, T109 N., R31 W	2B	2020	
	08-0054-00	Altermatt Lake	Sec. 31, T109 N., R33 W	2B	2020	
	08-0096-00	Boise Lake	Sec. 12, T109 N., R34 W	2B	2020	
	08-0029-00	Bachelor Lake	Sec. 11, T109 N., R32 W	2B	2020	

¹ Plum Creek Reach 516 was split into two separate reaches, 602 and 603, during 2019 assessment process.

Figure 2. Cottonwood River Watershed impairments covered in this TMDL.

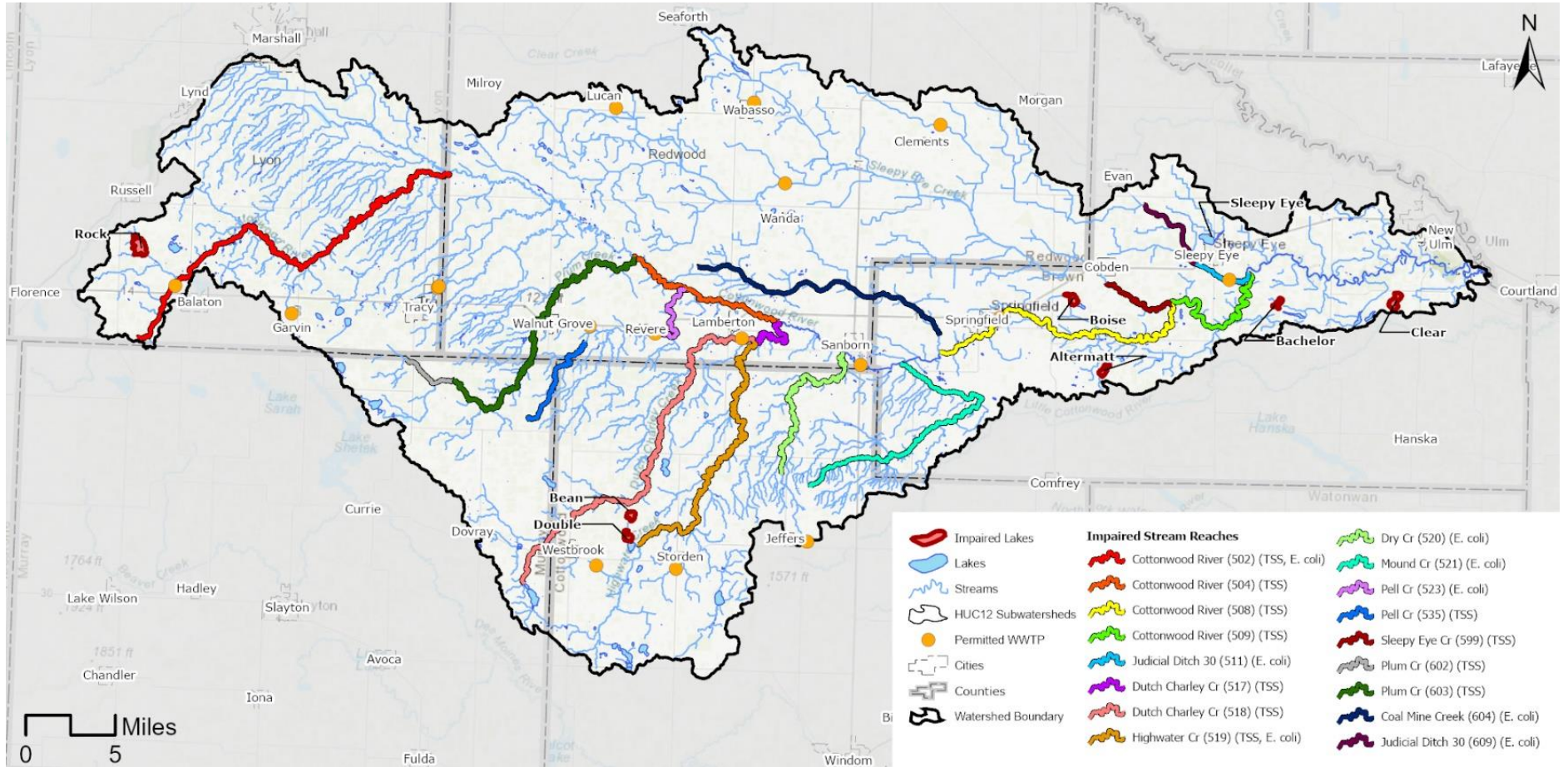


Table 2 provides a summary of the impaired stream reaches in the Cottonwood River Watershed with existing EPA-approved TMDL studies that were completed prior to this TMDL report.

Table 2. Summary of TMDLs already completed within the Cottonwood River Watershed.

Stream or Lake Name	Reach AUID (Last 3 Digits)	Pollutant(s)	TMDL Report(s)
Cottonwood River (JD30 to Minnesota River)	501	Aquatic Recreation: Fecal coliform Aquatic Life: TSS Aquatic consumption: Mercury in fish	Cottonwood River Fecal Coliform TMDL Report (RCRCA 2013) Minnesota River and Greater Blue Earth River Basin TSS TMDL Study (MPCA 2020b) <u>Minnesota Statewide Mercury Total Maximum Daily Load (MPCA 2007a)</u>
Cottonwood River (Coal Mine Creek to Sleepy Eye Creek)	508	Aquatic Recreation: Fecal coliform Aquatic consumption: Mercury in fish	Cottonwood River Fecal Coliform TMDL Report (RCRCA 2013) <u>Minnesota Statewide Mercury Total Maximum Daily Load (MPCA 2007a)</u>
Sleepy Eye Creek (Headwaters to Cottonwood River)	512	Aquatic Recreation: Fecal coliform;	Cottonwood River Fecal Coliform TMDL Report (RCRCA 2013)
Cottonwood River (Plum Creek to Dutch Charley Creek)	504	Aquatic Recreation: Fecal coliform Aquatic consumption: Mercury in fish	Cottonwood River Fecal Coliform TMDL Report (RCRCA 2013) <u>Minnesota Statewide Mercury Total Maximum Daily Load (MPCA 2007a)</u>
Dutch Charley Creek (Highwood Creek to Cottonwood River)	517	Aquatic Recreation: Fecal coliform	Cottonwood River Fecal Coliform TMDL Report (RCRCA 2013)
Plum Creek (Headwaters to Cottonwood River)	516	Aquatic Recreation: Fecal coliform	Cottonwood River Fecal Coliform TMDL Report (RCRCA 2013)
Lone Tree Creek (T109 R39W S7 westline to Cottonwood River)	524	Aquatic Recreation: Fecal coliform	Cottonwood River Fecal Coliform TMDL Report (RCRCA 2013)
Meadow Creek (Headwaters to Cottonwood River)	515	Aquatic Recreation: Fecal coliform	Cottonwood River Fecal Coliform TMDL Report (RCRCA 2013)
Cottonwood River (Headwaters to Meadow Creek)	502	Aquatic consumption: Mercury in fish	<u>Minnesota Statewide Mercury Total Maximum Daily Load (MPCA 2007a)</u>
Cottonwood River (Meadow Creek to Plum Creek)	503	Aquatic consumption: Mercury in fish	<u>Minnesota Statewide Mercury Total Maximum Daily Load (MPCA 2007a)</u>

Stream or Lake Name	Reach AUID (Last 3 Digits)	Pollutant(s)	TMDL Report(s)
Cottonwood River (Dutch Charley Creek to Dry Creek)	505	Aquatic consumption: Mercury in fish	<u>Minnesota Statewide Mercury Total Maximum Daily Load (MPCA 2007a)</u>
Cottonwood River (Dry Creek to Mound Creek)	506	Aquatic consumption: Mercury in fish	<u>Minnesota Statewide Mercury Total Maximum Daily Load (MPCA 2007a)</u>
Cottonwood River (Mound Creek to Coal Mine Creek)	507	Aquatic consumption: Mercury in fish	<u>Minnesota Statewide Mercury Total Maximum Daily Load (MPCA 2007a)</u>
Cottonwood River (Sleepy Eye Creek to Judicial Ditch 30)	509	Aquatic consumption: Mercury in fish	<u>Minnesota Statewide Mercury Total Maximum Daily Load (MPCA 2007a)</u>

The IWM efforts for the Cottonwood River Watershed identified 13 stream reaches that currently do not meet fish IBI standards and 26 stream reaches that do not meet aquatic macroinvertebrate IBI standards. A SID report was developed for these reaches to determine the primary stressors to the biological communities (MPCA, available upon request). Nonpollutant stressors (e.g., habitat, connectivity) are not subject to load quantification and therefore do not require TMDLs. If a nonpollutant stressor is linked to a pollutant (e.g., habitat issues driven by TSS or low dissolved oxygen (DO) caused by excess phosphorus) a TMDL is required. However, in many cases habitat stressors are not linked to pollutants. Impairments where chemical pollutants from anthropogenic sources are not a primary stressor to the fish and aquatic macroinvertebrate communities will not be covered in this TMDL, and instead will be addressed through the implementation of the Cottonwood River WRAPS Report and local water planning efforts.

1.2 Identification of Water Bodies

The TSS-impaired reaches were placed on the Clean Water Act Section 303(d) impaired waters list in 2006, 2010, and 2020. The bacteria-impaired reaches were placed on the 303(d) list in 2020. The nutrient-impaired lakes were placed on the 303(d) list in 2010, and 2020. All of the impaired reaches addressed in this TMDL are Class 2B (warm water). TMDLs are developed for the most restrictive use class. Class 2B waters are the most stringent of the applicable standards.

Table 1 and the [Cottonwood River Watershed Monitoring and Assessment Report](#) (which includes notes regarding aquatic life impairments for which TMDLs are not computed) summarize Cottonwood River Watershed impairments and those addressed in this TMDL. There are two reaches of Plum Creek, reaches 602 and 603, which are covered under this TMDL. These reaches were previously combined as one contiguous reach, Plum Creek reach 516. During the 2019 assessment process, reach 516 was split into two separate reaches (602 and 603) due to new tiered aquatic life uses (TALU) standards for channelized streams. This impairment will be carried forward and one TMDL will be presented that covers both reaches in this report.

1.3 Priority Ranking

The Minnesota Pollution Control Agency (MPCA) schedule for TMDL completions, as indicated on the 2022 303(d) impaired waters list, reflects Minnesota's priority ranking of this TMDL. The MPCA has aligned its TMDL priorities with the watershed approach and the WRAPS cycle. The schedule for TMDL completion corresponds to the WRAPS report completion on a 10-year cycle. The MPCA developed a state plan ([Minnesota's TMDL Priority Framework Report](#)) to meet the needs of EPA's national measure (WQ-27) under [EPA's Long-Term Vision](#) for Assessment, Restoration, and Protection under the Clean Water Act Section 303(d) Program. As part of these efforts, the MPCA identified water quality impaired segments that will be addressed by TMDLs by 2022. The Cottonwood River Watershed waters addressed by this TMDL are part of that MPCA prioritization plan to meet EPA's national measure.

2. Applicable Water Quality Standards

2.1 Designated Uses

Use classifications are defined in Minn. R. 7050.0140, and water use classifications for individual water bodies, are provided in Minn. R. 7050.0470, 7050.0425, and 7050.0430. The impaired lakes and streams covered in this TMDL are classified as class 2B waters (Table 1). This TMDL addresses the water bodies that do not meet the standards for class 2 waters, which are protected for aquatic life and recreation designated uses.

Class 2B waters are protected for the propagation and maintenance of a healthy community of cool or warm water sport or commercial fish and associated aquatic life and their habitats. Class 2B waters are also protected for aquatic recreation activities including bathing.

2.2 Turbidity/TSS

A historical perspective is important to understand the development of TSS TMDLs in this report. The class 2B turbidity standard (Minn. R. ch. 7050.0222) that was in place at the time of the impairment assessment for many reaches in the project area was 25 nephelometric turbidity units (NTUs). Impairment listings occurred when greater than 10% of data points collected within the previous 10-year period exceeded the 25 NTU standard (or equivalent values for TSS or the transparency tube). If sufficient turbidity data did not exist, transparency tube data were used to evaluate waters for turbidity impairments for the 2006 through 2014 303(d) lists of impaired waters. A transparency tube measurement less than 20 centimeters (cm) indicated a violation of the 25 NTU turbidity standard. A stream was considered impaired if more than 10% of the transparency tube measurements were less than 20 cm.

Due to weaknesses in the turbidity standards, the MPCA developed numeric TSS criteria to replace them. These TSS criteria are regional in scope and based on a combination of biotic sensitivity to the TSS concentrations and reference streams/least impacts streams as data allow. The results of the TSS criteria development were published by the MPCA in 2011. The new TSS standards were approved by EPA in January 2015. For the purpose of this TMDL, the newly adopted 65 mg/L standard for class 2B waters is used to address the turbidity impairment listings.

The 11 reaches of the Cottonwood River Watershed listed as impaired by turbidity/TSS are class 2B warm water streams. The class 2B TSS standard for streams and rivers in the Southern River Nutrient Region is 65 mg/L. This standard may not be exceeded more than 10% of the time from April through September over a multi-year data window (MPCA 2011).

Transparency values, as measured by Secchi tubes (S-tube), reliably predict TSS and can serve as surrogates. While TSS measurements themselves are generally preferred, datasets for S-tube are often more robust, and their relative strength will be considered in assessments.

Because S-tube measurements are not perfect surrogates, however, their use involves a MOS. Therefore, the S-tube surrogate thresholds for determining if a stream exceeds the TSS standard are different than for determining if a stream meets the standard.

A stream is considered to exceed the standard for TSS/S-tube if: 1) the standard is exceeded more than 10% of the days of the assessment season (April through September), as determined from a data set that gives an unbiased representation of conditions over the assessment season, and 2) there are at least three such measurements exceeding the standard.

A stream is considered to meet the standard for TSS/S-tube if the standard is met at least 90% of the days of the assessment season. A designation of meeting the standard for TSS/S-tube generally requires at least 20 suitable measurements from a data set that gives an unbiased representation of conditions over at least two different years. However, if it is determined that the data set adequately targets periods and conditions when exceedances are most likely to occur, a smaller number of measurements may suffice.

S-tube measurements that fall between the two relevant surrogate values are considered to be indeterminate in exceeding or meeting the TSS standard. For Class 2B waters in the Southern River Nutrient Region, 10 cm and 15 cm represent the lower and upper surrogate values, respectively. If a stream satisfies neither the criterion for exceeding the standard nor the criterion for meeting the standard, the stream is considered to have insufficient information regarding TSS levels.

2.3 Bacteria

With the revisions of Minnesota's water quality rules in 2008, the standard changed from a fecal coliform-based standard to an *E. coli* based standard because it is a superior potential illness indicator and costs for lab analysis are less (MPCA 2007b). The revised standards now state:

"E. coli concentrations are not to exceed 126 organisms per 100 milliliters (chronic standard) as a geometric mean of not less than five samples representative of conditions within any calendar month, nor shall more than 10% of all samples taken during any calendar month individually exceed 1,260 organisms per 100 milliliters (acute standard). The standard applies only between April 1 and October 31."

The chronic *E. coli* concentration standard of 126 organisms per 100 mL was considered reasonably equivalent to the previous chronic fecal coliform standard of 200 organisms per 100 milliliters from a public health protection standpoint. The SONAR (Statement of Need and Reasonableness) section that supports this rationale uses a log plot that shows a good relationship between these two parameters. The following regression equation was deemed reasonable to convert any data reported in fecal coliform to *E. coli* equivalents:

$$E. coli \text{ concentration (equivalents)} = 1.80 \times (\text{Fecal Coliform Concentration})^{0.81}$$

It should also be noted that most analytical laboratories report *E. coli* in terms of colony forming units per 100 milliliters (cfu/100 mL), not organisms per 100 milliliters. This TMDL will present *E. coli* data in cfu/100 mL since all of the monitored data collected was reported in these units. Bacteria TMDLs were written to achieve the bacteria water quality standard of 126 orgs/100 mL as a monthly geometric mean. Geometric mean is used in place of arithmetic mean in order to measure the central tendency of the data, dampening the effect that very high or very low values have on arithmetic means. Geometric means are calculated using the following equation:

$$\text{Geometric mean} = \sqrt[n]{x_1 * x_2 * \dots * x_n}$$

The MPCA’s Guidance Manual for Assessing the Quality of Minnesota Surface Waters for Determination of Impairment: 305(b) Report and 303(d) List (MPCA 2022) provides details regarding how waters are assessed for conformance to the *E. coli* standard.

2.4 Lake Nutrients

Under Minn. R. 7050.0150 and 7050.0222, subp. 4, all of the lakes addressed in this TMDL are shallow lakes. Shallow lakes are defined as lakes with a maximum depth of 15 feet or less, or with 80% or more of the lake area shallow enough to support emergent and submerged rooted aquatic plants (littoral zone). All seven lakes are located within the Western Cornbelt Plain (WCBP) Ecoregion. Minnesota water quality standards for TP, chlorophyll-a (Chl-*a*) and Secchi disk transparency for the WCBP Ecoregion are listed in Table 3.

In addition to meeting TP limits, Chl-*a* and Secchi disk standards must be met. In developing the lake nutrient standards for Minnesota lakes (Minn. R. ch. 7050), the MPCA evaluated data from a large cross-section of lakes within each of the state’s ecoregions (MPCA 2005). Clear relationships were established between the causal factor TP and the response variables Chl-*a* and Secchi transparency. Based on these relationships it is expected that by meeting the TP target in each lake, the Chl-*a* and Secchi disk standards will likewise be met.

Table 3. Eutrophication standards for class 2B lakes, shallow lakes, and reservoirs in the Western Corn Belt Plains ecoregion.

Parameter	WCBP Ecoregion Standards (2B shallow lakes)
Total Phosphorus [µg/L]*	90
Chlorophyll-a [µg/L]	30
Secchi Disk Transparency [meters]	0.7

* Microgram per liter or part per billion

3. Watershed and Water Body Characterization

The Cottonwood River Watershed is a major Hydrologic Unit Code (HUC)-8 watershed in the Minnesota River Basin, covering the central portion of the state. The Cottonwood River Watershed is approximately 1,314 square miles or 840,772 acres, split between five counties including: Redwood (35%), Brown (21%), Cottonwood (19%), Lyon (17%), and Murray (8%). There is no tribal land in the Cottonwood River Watershed and this TMDL does not allocate pollutant load to any federally recognized Indian tribe.

There are 36 individual HUC-12 subwatersheds in the Cottonwood River Watershed and 8 major HUC-10 subwatersheds: Headwaters –Cottonwood River, Meadow Creek, Plum Creek, Pell Creek – Cottonwood River, Dutch Charley Creek, Mound Creek – Cottonwood River, Sleepy Eye Creek, and Cottonwood River (see Figure 1). The streams and tributaries that make up these major subwatersheds flow to the Cottonwood River upstream of the confluence with the Minnesota River.

3.1 Lakes

Collectively lakes and open water areas in the Cottonwood River Watershed (07020008) account for approximately 1% of the watershed. There are seven assessed lakes impaired by excess nutrients in the watershed (see Figure 2). Lake morphometry and watershed information for each impaired lake covered in this TMDL is presented in Table 4. All seven lakes are considered shallow with average depths ranging from 1 to 11 feet. Residence time is generally short and watershed to surface area ratios vary widely from 3:1 to 15:1.

Table 4. Lake morphometry and watershed area in the Cottonwood River Watershed.

Parameter	Rock	Bean	Double (North Portion)	Clear	Altermatt	Boise	Bachelor
County	Lyon	Cottonwood	Cottonwood	Brown	Brown	Brown	Brown
Lake ID	42-0052-00	17-0054-00	17-0056-01	08-0011-00	08-0054-00	08-0096-00	08-0029-00
Lake Type	Shallow	Shallow	Shallow	Shallow	Shallow	Shallow	Shallow
Lake Surface Area [acres]	379	164	136	277	122	187	105
Ave. Depth [ft]	5.2	11.2	6.5	4.9	3.2	2.2	1.3
Max Depth [ft]	8	14	9	8	5	7	4
Residence Time [yrs]	0.9	3.2	1.2	0.8	0.4	0.4	0.4
Littoral Area [%]	100	100	100	100	100	100	100
Watershed Area ¹ [acres]	3,208	372	1,246	1,426	1,865	1,376	377
Watershed Area: Surface Area	8:1	3:1	9:1	5:1	15:1	7:1	4:1

¹ Does not include lake surface area.

3.2 Streams

The 17 impaired stream reaches in the Cottonwood River Watershed addressed in this TMDL cover approximately 280 stream miles and drain approximately 795,000 acres of land across the watershed (Figure 2, Table 5). Additional information for each impaired stream reach can be found in Appendix A. Eight bacteria-impaired reaches in the Cottonwood River Watershed were already addressed in the Cottonwood River Fecal Coliform TMDL Report (RCRCA 2013) as discussed in Section 1.1.

Table 5. Impaired stream characteristics in the Cottonwood River Watershed.

Reach Name	Impaired Reach ID ¹	Imp. Parameter	Reach Length [miles]	Watershed Area [acres]	Upstream Impaired Reach(es)
Cottonwood River: Headwaters to Meadow Creek	502	TSS, <i>E. coli</i>	42.4	64,218	None
Cottonwood River: Plum Creek to Dutch Charley Creek	504	TSS	13.4	285,997	502, 535, 602, 603
Cottonwood River: Coal Mine Creek to Sleepy Eye Creek	508	TSS	23.9	564,925	502, 504, 517, 518, 519, 520, 521, 523, 535, 602, 603, 604
Cottonwood River: Sleepy Eye Creek to JD 30	509	TSS	12.0	759,705	502, 504, 508, 517, 518, 519, 520, 521, 523, 599, 602, 603, 604
Judicial Ditch 30: T110 R32W S31, west line to Cottonwood River	511	<i>E. coli</i>	4.2	37,473	609
Dutch Charley Creek: Highwater Creek to Cottonwood River	517	TSS	7.3	133,975	518, 519
Dutch Charley Creek: Headwaters to Highwater Creek	518	TSS	39.5	61,174	None
Highwater Creek: Double Lake outlet to Dutch Charley Creek	519	TSS, <i>E. coli</i>	33.1	69,375	None
Dry Creek: T108 R36W S31, south line to Cottonwood River	520	<i>E. coli</i>	17.8	26,262	None
Mound Creek: Headwaters to Cottonwood River	521	<i>E. coli</i>	24.9	35,259	None
Pell Creek: T109 R37W S30, west line to Cottonwood River	523	<i>E. coli</i>	6.6	33,171	None
Pell Creek: Headwaters to T109 R38W S29, east line	535	TSS	10.0	8,152	None
Sleepy Eye Creek: T109 R33W S5, west line to Cottonwood River	599	TSS	6.0	176,728	None
Plum Creek: Headwaters to -95.576 44.177 (602); -95.576 44.177 to Cottonwood River (603)	602 & 603 ²	TSS	34.1	57,682	None
Coal Mine Creek: Headwaters to T109 R35W S22, south line	604	<i>E. coli</i>	17.33	29,413	None
Judicial Ditch 30: T110 R33W S15, west line to T110 R33W S36, east line	609	<i>E. coli</i>	5.8	28,452	None

¹ Only the last three digits of the impaired reach are shown in this table for the Cottonwood River (07020008) impairments.

² Plum Creek Reach 516 was split into two separate reaches, 602 and 603, during 2019 assessment process.

3.3 Subwatersheds

The drainage areas of the impaired water bodies (Figure 2) were developed using multiple data sources, starting with watershed delineations from the MPCA's HSPF model application for the Cottonwood River Watershed (Tetra Tech 2019). The model watershed boundaries are based on Minnesota Department of Natural Resources (DNR) Level 8 watershed boundaries and modified with a 30-meter digital elevation model (DEM). Where additional watershed breaks were needed to define the impairment watersheds, DNR Level 8 and Level 9 watershed boundaries and delineation were used based on contours derived from LiDAR. Maps showing specific watershed boundaries for each impaired stream reach and lake are included in Appendix A and Appendix C.

3.4 Land use

Uninterrupted prairie and wetlands originally covered a majority of the Cottonwood River Watershed. Like most areas across the Midwest, land throughout the watershed has been converted from a range of tallgrass prairie and a small number of wet prairies to a mixture of intensive agricultural uses. This conversion has resulted in various changes throughout the watersheds, such as increases in overland flow, decreases in groundwater infiltration/subsurface recharge, and increases in the nonpoint source transport of sediment, nutrients, agricultural, and residential chemicals, and feedlot runoff.

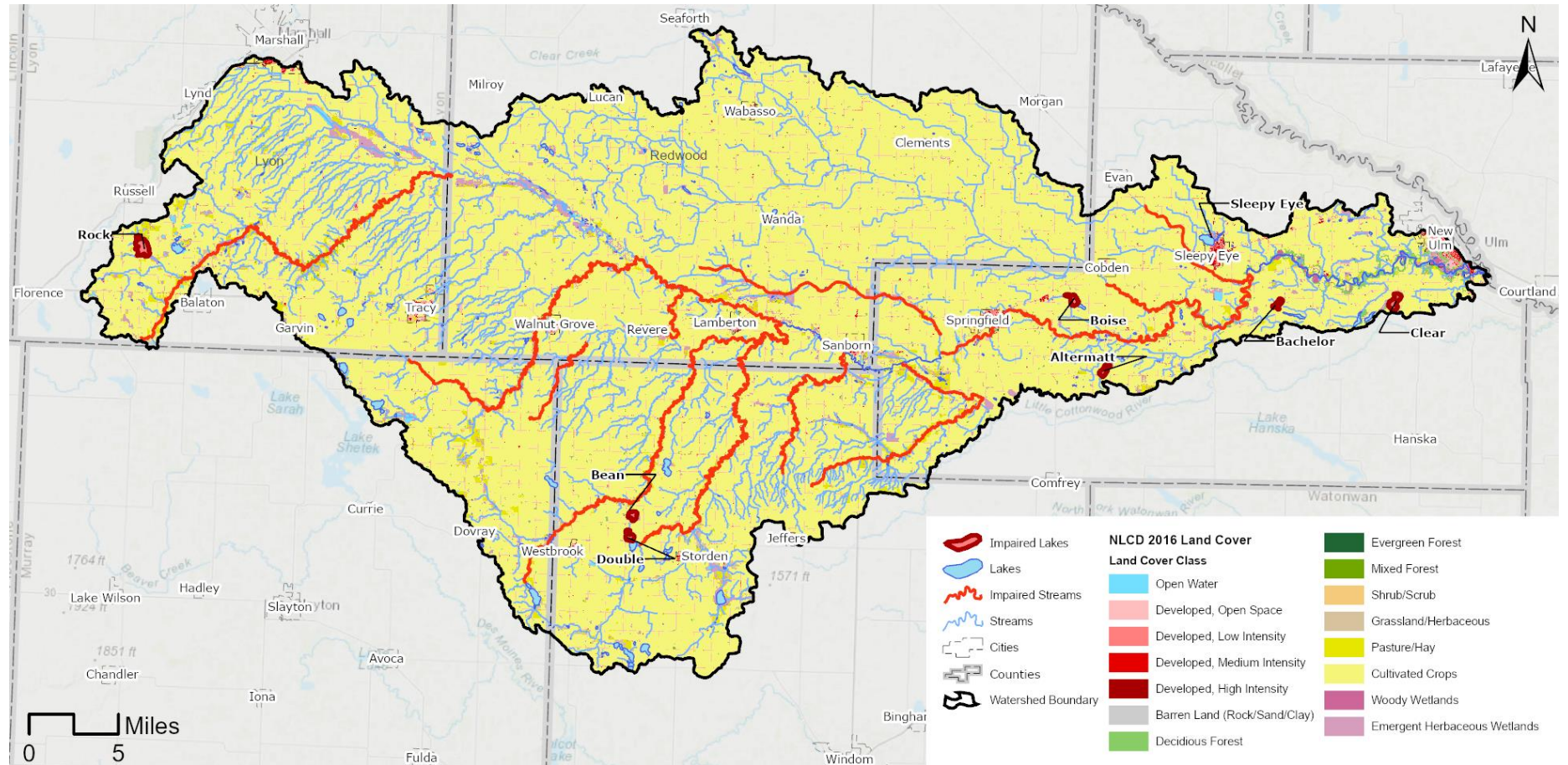
Land use within the Cottonwood River Watershed was analyzed using USGS's 2016 National Land Cover Database (NLCD). Current land use within the watershed is highly dominated by agriculture (mostly row crops,) followed by relatively small amounts of rangeland, developed land, wetlands, open water, and forest/shrub land (Table 6 and Figure 3). Row crops throughout the watersheds are predominately planted in corn, forage for livestock, and soybeans (MDA 2009 and 2010a). Rangeland typically follows stream corridors, which is a large reason for less channelization of the streams than in other regions of Minnesota.

The city of New Ulm (MS400228) is the largest city in the Cottonwood River Watershed and is located at the confluence with the Minnesota River. A small portion (~671 acres) of the city of Marshall (MS400241) is also located within the Cottonwood River Watershed near the headwaters of the Meadow Creek Subwatershed. Both the cities of New Ulm and Marshall are subject to the MPCA's Municipal Separate Storm Sewer System (MS4) Permit program (see Section 4.2.2).

Table 6. Summary of land use and watershed area for each impaired reach and lake in the Cottonwood River Watershed.

Impaired Water Body Name	Reach or Lake ID	Drainage Area [Acres]	Percent of Watershed [%]						
			Cropland	Rangeland	Developed	Forest/Shrub land	Open Water	Wetlands	Barren/Mining
Cottonwood River	502	64,218	79%	10%	5%	1%	2%	3%	<1%
Cottonwood River	504	285,997	83%	6%	6%	<1%	<1%	4%	<1%
Cottonwood River	508	564,925	84%	5%	6%	< 1%	<1%	4%	<1%
Cottonwood River	509	759,705	85%	4%	5%	< 1%	<1%	3%	<1%
Judicial Ditch 30	511	37,473	88%	1%	8%	<1%	<1%	2%	<1%
Dutch Charley Creek	517	133,975	85%	5%	5%	1%	1%	2%	<1%
Dutch Charley Creek	518	61,174	88%	3%	5%	2%	<1%	2%	<1%
Highwater Creek	519	69,375	84%	6%	5%	1%	2%	2%	<1%
Dry Creek	520	26,262	88%	4%	5%	<1%	<1%	2%	<1%
Mound Creek	521	35,259	81%	7%	5%	<1%	<1%	6%	<1%
Pell Creek	523	33,171	88%	2%	7%	1%	<1%	2%	<1%
Pell Creek	535	8,152	87%	2%	8%	< 1%	<1%	2%	<1%
Sleepy Eye Creek	599	176,728	91%	< 1%	6%	< 1%	<1%	2%	<1%
Plum Creek	602 & 603	57,682	86%	5%	5%	1%	1%	2%	<1%
Coal Mine Creek	604	29,413	86%	1%	5%	<1%	<1%	6%	<1%
Judicial Ditch 30	609	28,452	91%	1%	6%	<1%	<1%	1%	<1%
Rock	42-0052-00	3,208	74%	7%	5%	<1%	13%	<1%	<1%
Bean	17-0054-00	372	56%	<1%	6%	1%	34%	2%	<1%
Double	17-0056-01	1,246	58%	2%	6%	1%	31%	2%	<1%
Clear	08-0011-00	1,426	57%	2%	4%	5%	22%	10%	<1%
Altermatt	08-0054-00	1,865	84%	< 1%	4%	2%	7%	2%	<1%
Boise	08-0096-00	1,376	73%	< 1%	11%	<1%	12%	4%	<1%
Bachelor	08-0029-00	377	66%	<1%	2%	<1%	27%	4%	<1%
Entire Watershed	07020008	840,772	85%	4%	6%	1%	1%	3%	<1%

Figure 3. Land cover in the Cottonwood River Watershed (Source: 2016 NLCD).



3.5 Current/Historical Water Quality

All data used in the development of this TMDL were collected between 2000 and 2018 by various agencies and local partners, including the MPCA, MDA, Redwood Cottonwood River Control Area (RCRCA), area Soil and Water Conservation Districts (SWCDs), and volunteer monitoring programs. Although data prior to 2000 exists in each of the major watersheds, the more recent data represent more current conditions.

Daily average flows were simulated using the MPCAs HSPF model for the Cottonwood River Watershed. Simulated flows are available for each impaired lake and reach for model years 1996 through 2017. Cottonwood River HSPF model documentation (Tetra Tech 2019) describes the framework of the model, the data used to develop the model, and calibration/validation results.

3.5.1 TSS

TSS data were summarized by site for each TSS impaired reach in the Cottonwood River Watershed using data from 2000 to 2017 (Table 7). The TSS impairments presented in this TMDL are based upon the current TSS standard for the Southern River Nutrient Region of 65 mg/L. There is currently no TSS data available for Cottonwood River Reach 509 and Pell Creek Reach 535. However, S-tube (transparency) data were available for these reaches and were used by the MPCA to assess the TSS impairment for these reaches. The S-tube data for both reaches are presented in Table 8. As discussed in Section 2.2, 10cm represents the lower surrogate threshold for S-tube measurements while 15cm represents the upper surrogate threshold. Thus, any S-tube measurement less than 10cm is considered a violation of the TSS criterion for assessment purposes. Figure 8 through Figure 17 in Section 4.2.6 show the variability of TSS by flow condition over the most recent 10-year period (2008 through 2017) for each TSS impaired reach. The turbidity impairment listing for 07020008-535 is based on data collected between 2001 through 2004. The age of the data and relatively low exceedance rate suggest 07020008-535 should be prioritized for additional monitoring to determine candidacy for de-listing.

Table 7. Summary of TSS data for impaired reaches from 2000-2017 in the Cottonwood River Watershed (April – October).

Parameter	Cottonwood River	Cottonwood River	Cottonwood River	Dutch Charley Creek	Dutch Charley Creek	Highwater Creek	Sleepy Eye Creek	Plum Creek Reach
Reach Id	07020008-502	07020008-504	07020008-508	07020008-517	07020008-518	07020008-519	07020008-599	07020008-602 & 603
Years of Data	1	14	18	4	3	1	18	14
Sample Count	13	99	237	37	22	13	232	85
90 th Percentile [mg/L]	156	108	234	107	65	110	114	166
Mean [mg/L]	75	71	100	51	33	54	50	101
Maximum [mg/L]	215	900	563	54	304	204	648	2,670
Number of Exceedances	7	31	126	8	3	3	45	31
Frequency of Exceedances	54%	31%	53%	22%	14%	23%	19%	36%

Table 8. Summary of Secchi tube data for Cottonwood River Reach 509 and Pell Creek Reach 535 from 2000-2017 (April – October).

Parameter	Cottonwood River	Pell Creek
Reach Id	07020008-509	07020008-535
Years of Data	3	4
Sample Count	107	97
10 th Percentile [cm]	9	13.2
Mean [cm]	43.3	42.1
Low [cm]	1	5
Number of Exceedances	16	5
Frequency of Exceedances	15%	5%

3.5.2 Bacteria

Table 9 shows April through October monthly *E. coli* geometric means (2000 through 2017) for the bacteria-impaired reaches addressed in this TMDL. Older records for bacteria samples were analyzed for fecal coliform prior to switching to *E. coli* in 2006. All fecal coliform data collected prior to 2006 were converted to *E. coli* equivalents using the equation described in Section 2.3. Table 9 shows the individual chronic sample exceedances, acute exceedances, and monthly geometric means for each impaired reach. Results indicate monthly geometric means exceeded the chronic standard several times during the index period. Additionally, individual samples occasionally exceeded the acute standard for several reaches from April through October.

Table 9. Summary of *E. coli* data for Cottonwood River Watershed impaired reaches from 2000-2017.

Monitored Month(s)	Parameter	Cottonwood River Reach 502	Judicial Ditch 30 Reach 511	Highwater Creek Reach 519	Dry Creek Reach 520	Mound Creek Reach 521	Pell Creek Reach 523	Coal Mine Creek Reach 604	Judicial Ditch 30 Reach 609
Apr-Oct	Years of data	1	1	1	1	3	1	3	2
Apr-Oct	Sample count	9	9	9	9	24	9	24	15
Apr-Oct	Maximum (MPN/100 mL)	5,794	1,658	6,488	4,106	9,208	12,033	2,948	2,420
Apr-Oct	Number of individual sample exceedances	9	9	9	9	24	9	23	15
Apr-Oct	Percent of individual sample exceedances	100%	100%	100%	100%	100%	100%	96%	100%
Apr-Oct	Geometric mean	1,063	710	1,897	2,033	1,553	937	1,401	787
Apr	Sample count	0	0	0	0	0	0	0	0
	Geometric mean	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
May	Sample count	0	0	0	0	0	0	0	0
	Geometric mean	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Jun	Sample count	3	3	3	3	7	3	7	5
	Geometric mean	877*	704*	1,760*	3,248*	1,344	666*	1,156	303
Jul	Sample count	3	3	3	3	8	3	8	5
	Geometric mean	736*	551*	2,729*	2,683*	1,583	2,005*	1,740	780
Aug	Sample count	3	3	3	3	9	3	9	5
	Geometric mean	1,859*	921*	1,420*	964*	1,709	617*	1,343	2,064
Sep	Sample count	0	0	0	0	0	0	0	0
	Geometric mean	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Oct	Sample count	0	0	0	0	0	0	0	0
	Geometric mean	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

* Geometric means are calculated; however, there are fewer than the 5 required monthly samples for assessment.

Table notes:

-Red highlighted values indicate monthly geometric mean concentration exceeds the 126 organisms per 100 mL chronic standard.

-All geometric mean values presented in MPN/100 mL.

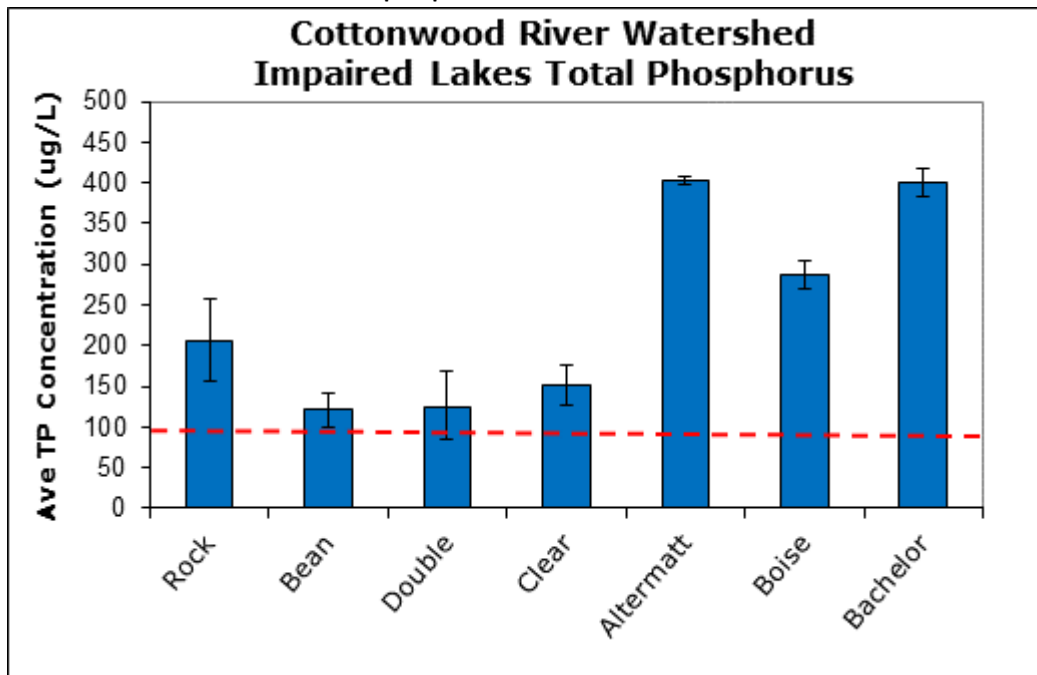
3.5.3 Lake Phosphorus and Response Variables

In general, historical in-lake water quality data collected from 2000 through 2018 was reviewed for use in this TMDL. Table 10 lists the June through September averages for TP, Chl-*a*, and Secchi depth for each impaired lake. The table also lists the data years which were used to calculate the average condition for this TMDL. All lakes indicate average summer TP, Chl-*a*, and/or Secchi depths are not meeting ecoregion-defined state standards. Figure 4 shows the average TP for each lake relative to the shallow lake standard.

Table 10. Summer growing season averages for each water quality parameter in the Cottonwood River Watershed.

Lake Name	"Average" Condition Calculation Years	In-Lake Average Condition [Calculated June – September]		
		TP Concentration [µg/L]	Chl- <i>a</i> Concentration [µg/L]	Secchi Depth [m]
WCBP Ecoregion 2B Shallow Lake Standards		90	30	0.7
Rock	2002, 2007, 2017	202 (n=12)	30 (n=12)	0.5 (n=11)
Bean	2007, 2008, 2017	122 (n=12)	49 (n=12)	1.0 (n=12)
Double	2007, 2008, 2017, 2018	124 (n=15)	52 (n=16)	0.7 (n=16)
Clear	2009, 2010, 2017	151 (n=15)	78 (n=15)	0.4 (n=19)
Altermatt	2009, 2010	403 (n=14)	138 (n=14)	0.2 (n=12)
Boise	2011, 2012	287 (n=11)	141 (n=11)	--
Bachelor	2011, 2012	400 (n=11)	183 (n=11)	--

Figure 4. Average summer growing season TP concentrations for each impaired lake in the Cottonwood River Watershed. Dotted red line indicates shallow lake phosphorus standard.



3.6 Pollutant Source Summary

The permitted sources discussed here are pollutant sources that require a National Pollutant Discharge Elimination System (NPDES) permit. Nonpermitted sources are pollutant sources that do not require an NPDES permit. All Minnesota NPDES permits are also state disposal system (SDS) permits, but some pollutant sources require SDS permit coverage alone without NPDES permit coverage (e.g., spray irrigation, large septic systems, land application of biosolids, and small feedlots).

Overland Runoff/Erosion (Rural Areas)

Nonpoint pollutant loads in rural areas can come from nonpermitted sources such as sediment erosion from upland fields, tile drainage, gully erosion, and livestock pastures in riparian zones (Schottler et al. 2013). Runoff from these sources can carry sediment, bacteria, phosphorus, and other nutrients to surface waters. For this TMDL, upland nonpoint sources of sediment and phosphorus were evaluated using the Cottonwood River Watershed HSPF Model (Tetra Tech 2019). HSPF is a comprehensive, mechanistic model of watershed hydrology and water quality that allows the integrated simulation of point sources, land and soil contaminant runoff processes, and in-stream hydraulic and sediment-chemical interactions. The results provide hourly runoff flow rates, sediment concentrations, and nutrient concentrations, along with other water quality constituents, at the outlet of any modeled subwatershed for the model time period 1996 through 2017. Model documentation contains additional details about model development and calibration (Tetra Tech 2019). Within each subwatershed, the upland areas are separated into multiple land use categories and are further parameterized based on hydrologic soil group. Simulated loads from upland areas represent the pollutant loads that are delivered to the modeled stream or lake; the loading rates do not represent field-scale soil loss estimates.

Overall, across the entire Cottonwood River HUC-8 Watershed, approximately 27% of the TSS load and 88% of the phosphorus load is from agricultural overland runoff (i.e., cultivated crops and hay/pasture lands identified in the 2016 NLCD land use layer, in addition to loading from feedlots) and other rural upland sources. Relative contributions by source vary widely between individual reaches. Sections 3.6.1 and 3.6.3 below contain more detailed discussion of the upland watershed source contributions for each impaired lake and stream reach.

Animal Feeding Operations

Livestock animals are potential sources of bacteria, phosphorus, and other nutrients to streams in the Cottonwood River Watershed, particularly when direct access is not restricted and/or where feeding structures are located adjacent to riparian areas.

Minn. R. ch. 7020 governs the permitting, standards for discharge, design, construction, operation and closure of animal feeding operations (AFOs) throughout Minnesota. By definition, an AFO is a site where animals are confined for 45 days or more in a 12-month period and vegetative cover is not maintained.

Concentrated Animal Feeding Operation (CAFO) is an EPA definition that implies not only a certain number of animals but also specific animal types. CAFO size is based on number of animals (head count) and can include large, medium, and small CAFOs. For example, 2,500 head of swine weighing 55 lbs or more is considered a large CAFO and 1,000 head of cattle other than mature dairy or veal calves are a large CAFO; but a site with 2,499 head of swine weighing 55 lbs or more and 999 head of cattle other

than mature dairy would be considered a medium CAFO. The MPCA uses the federal definition of a CAFO in its permit requirements of animal feedlots along with the definition of animal unit (AU). In Minnesota, a NPDES permit is required for facilities that exceed any of the federal large CAFO threshold numbers and discharges to waters of the United States. SDS permits are required for any facility that has a capacity of 1,000 AU or more. Facilities required to obtain SDS permit coverage may choose to obtain NPDES coverage in lieu of the SDS permit. Large CAFOs with less than 1,000 AU capacity and do not discharge to waters of the United States are not required to obtain NPDES Permit coverage.

CAFO production areas need to be designed, constructed, operated, and maintained to contain all manure, manure-contaminated runoff, or process wastewater, and direct precipitation. CAFOs and AFOs with 1,000 or more AUs must be designed to contain all manure and manure contaminated runoff from precipitation events of less than a 25-year - 24-hour storm event. Having and complying with an NPDES permit allows some enforcement protection if a facility discharges due to a 25-year - 24-hour precipitation event (approximately 5.07" in 24 hours) and the discharge does not contribute to a water quality impairment. Large CAFOs permitted with an SDS permit or those not covered by a permit must contain all runoff, regardless of the precipitation event. Therefore, many large CAFOs in Minnesota have chosen to have an NPDES permit, even if discharges have not occurred in the past at the facility. A current manure management plan (MMP), which complies with Minn. R. 7020.2225, and the respective permit is required for all CAFOs and AFOs with 1,000 or more AUs. Additionally, MMP requirements for CAFOs are more stringent than for smaller feedlots. CAFOs are inspected by the MPCA in accordance with the MPCA NPDES Compliance Monitoring Strategy approved by the EPA. All CAFOs (NPDES permitted, SDS permitted, and not required to be permitted) are inspected by the MPCA on a routine basis with an appropriate mix of field inspections, offsite monitoring, and compliance assistance.

Feedlots under 1,000 AUs and those that are not federally defined large CAFOs do not operate with permits; however, the requirements under Minn. R. chs. 7020, 7050 and 7060 still apply. Manure may accumulate in these feedlots, and vegetative cover cannot be maintained due to the density of animals. In Minnesota, feedlots with greater than 50 AUs, or greater than 10 AUs in shoreland areas, are required to register with the state. Facilities with fewer AUs are not required to register with the state. Feedlot registration enables the County and the MPCA to communicate directly with feedlot owners regarding all aspects of feedlot management including technical requirements, permitting, inspections and corrective action. Registration also helps ensure that surface waters are not contaminated by the runoff from feeding facilities, manure storage or stockpiles, and cropland with improperly applied manure. Livestock are also part of hobby farms, which are small-scale farms that are not large enough to require registration but may have small-scale feeding operations and associated manure application or stockpiles.

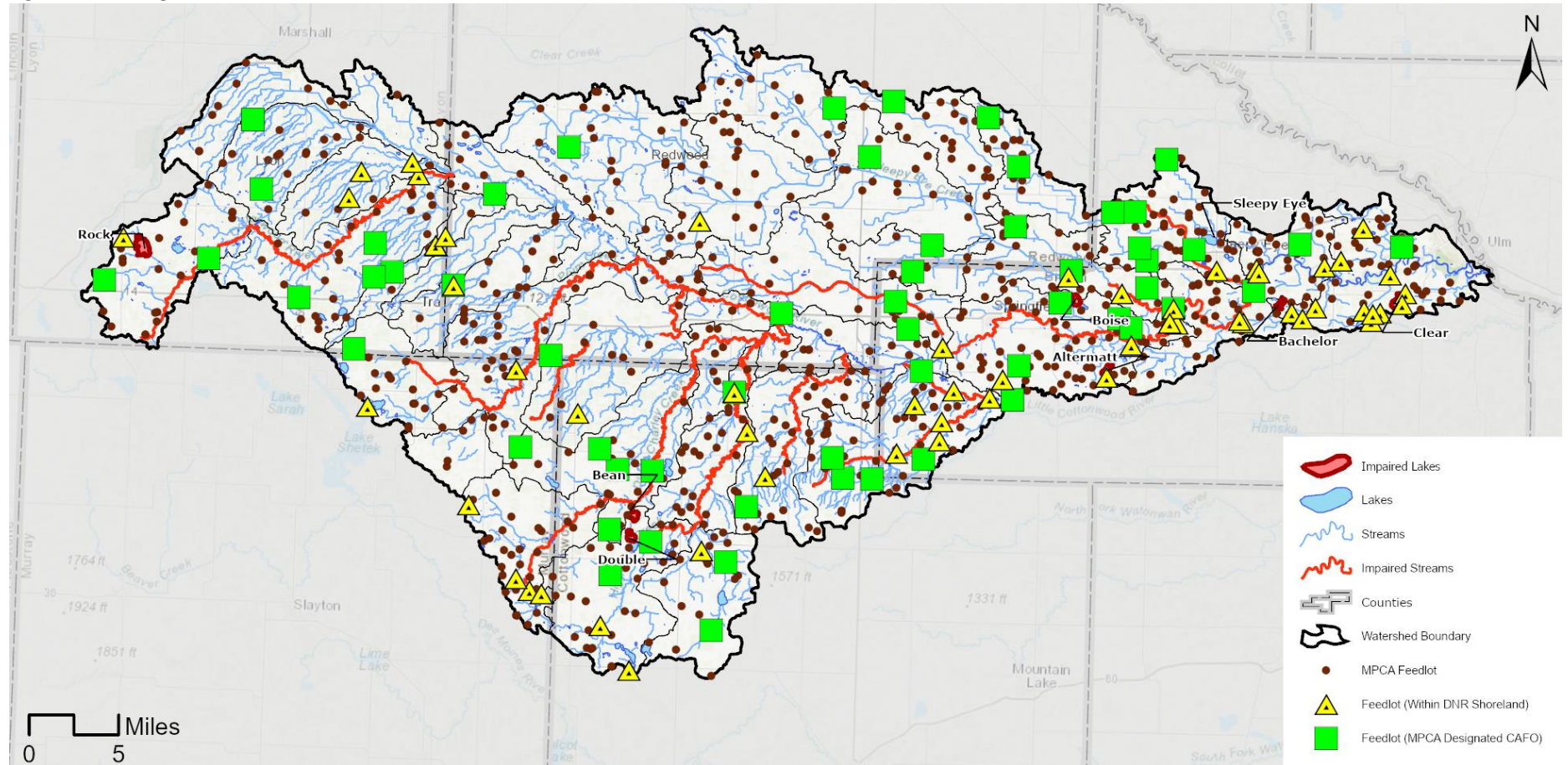
In the Cottonwood River Watershed, Redwood County is the only county that is not delegated to administer feedlot-related activities such as permitting, inspections, and compliance/enforcement. In Redwood County, the MPCA fulfills these responsibilities. Brown, Cottonwood, Lyon, and Murray Counties are delegated counties and therefore administer a county feedlot program based on the requirements of the Minn. R. 7020, Feedlot Rules. These counties have the responsibility for implementing state feedlot regulations for facilities with fewer than 1,000 AUs and do not meet the federal definition of a large CAFO that are not subject to state or federal operating permit requirements. Responsibilities include: registration, permitting, education and assistance, and complaint follow-up.

The MPCA maintains a feedlot registration database for CAFOs and registered feedlots that contains information such as feedlot locations, animal numbers, and types of animals. The database includes the maximum number of animals that each registered feedlot can hold; therefore, the actual number of livestock in registered facilities is likely lower. Livestock in nonregistered, smaller operations (e.g., hobby farms) likely contribute pollutant loads to surface waters through watershed runoff from fields and direct deposition in surface waters. The MPCA registered feedlot database indicates there were approximately 513 active feedlot facilities with over 228,065 livestock AUs throughout the Cottonwood River Watershed as of 2018 (Figure 5). Table 11 summarizes facility type and livestock numbers for each impaired reach, lake, and the entire watershed. In the Cottonwood River Watershed, there are 46 feedlots located within 1,000 feet of a lake or 300 feet of a stream or river, an area generally defined as shoreland. Thirty-seven of these feedlots in shoreland have open lots and could present a potential pollution hazard if the runoff from the open lots is not treated prior to reaching surface water. See Appendices E for a list and summary of all CAFOs in the watershed.

Table 11. MPCA active registered feedlots and feedlot type for each *E. coli* impaired reach and impaired lake in the Cottonwood River Watershed.

Impaired Reach/Lake	Impairment Type	Total Operations		CAFOs		Open Lots		Shoreland		Open Lots in Shoreland	
		Count	AUs	Operations	AUs	Operations	AUs	Operations	AUs	Operations	AUs
Cottonwood River Reach 502	<i>E. coli</i>	47	19,325	3	3,768	31	7,597	1	651	-	-
Judicial Ditch 30 Reach 511	<i>E. coli</i>	38	10,945	3	3,131	28	6,375	1	10	-	-
Highwater Creek Reach 519	<i>E. coli</i>	59	16,618	2	6,195	20	6,553	5	5,515	3	633
Dry Creek Reach 520	<i>E. coli</i>	29	5,933	1	900	19	4,087	1	84	1	84
Mound Creek Reach 521	<i>E. coli</i>	40	14,146	3	1,860	23	6,769	5	781	4	691
Pell Creek Reach 523	<i>E. coli</i>	12	1,799	-	-	9	1,724	1	15	-	-
Coal Mine Creek Reach 604	<i>E. coli</i>	12	4,013	1	1,106	9	2,081	-	-	-	-
Coal Mine Creek Reach 609	<i>E. coli</i>	29	9,557	3	3,131	21	5,741	-	-	-	-
Bean Lake	Nutrients	-	-	-	-	-	-	-	-	-	-
Double Lake	Nutrients	1	200	-	-	-	-	-	-	-	-
Rock Lake	Nutrients	6	1,631	-	-	4	560	1	651	-	-
Clear Lake	Nutrients	6	272	-	-	6	272	5	208	5	208
Altermatt Lake	Nutrients	4	1,486	-	-	4	1,486	1	549	1	549
Boise Lake	Nutrients	1	900	-	-	-	-	-	-	-	-
Bachelor Lake	Nutrients	-	-	-	-	-	-	-	-	-	-
Entire Cottonwood River Watershed	Multiple	513	228,065	64	91,155	322	98,170	46	13,108	37	5,555

Figure 5. MPCA registered feedlots in the Cottonwood River Watershed.



Manure

Manure is a by-product of animal production and large numbers of animals create large quantities of manure. This manure is usually stockpiled and then spread over agricultural fields to help fertilize the soil. When stored and applied properly, this beneficial re-use of manure provides a natural source for crop nutrition. Manure, however, can pose water quality concerns when it is not applied properly or leaks or spills from nearby fields, storage pits, lagoons, tanks, etc. Animal waste contains high amounts of fecal bacteria, phosphorus, and nitrogen, and therefore when delivered to surface and groundwater can cause high bacteria levels, eutrophication, and oxygen demand (i.e., low oxygen levels) that negatively impacts human health, aquatic organisms, and aquatic recreation.

The Minnesota Feedlot rules include regulations regarding the requirements for MMPs and land application of manure. The MPCA has developed templates, guides and standards for the development and implementation of MMPs, manure nutrient management and application rates. MMPs are required when producers apply for a feedlot permit, or when a facility has 300 or more AUs and does not use a licensed commercial applicator. MMPs are designed to help ensure that application rates do not exceed crop nutrient needs, and that setbacks from waters and drain tile intakes are observed.

Based on the MPCA feedlot staff analysis of feedlot demographics, knowledge, and actual observations, there is a significant amount of late winter solid manure application (before the ground thaws). During this time the manure can be a source of nutrients and pathogens in rivers and streams, especially during precipitation events. For feedlots with NPDES permits, surface applied solid manure is prohibited during the month of March. Winter application of manure (December through February) for permitted sites requires fields are approved in their MMP and the feedlot owner/operator must follow a standard list of setbacks and BMPs.

Short term stockpile sites are defined in Minn. R. ch. 7020 and are considered temporary. Any stockpile kept for longer than a year must be registered with the MPCA and would be identified as part of a feedlot facility. Because of the temporary status of the short-term stockpile sites, and the fact they are usually very near or at the land application area, they are included with the land applied manure.

Winter application of surface applied liquid manure is prohibited except for emergency manure application as defined by the NPDES permit. “Winter application” refers to application of manure to frozen or snow-covered soils, except below the soil surface. [Minn. R. 7001].

Incorporating manure is the preferred BMP for land application of manure and should result in less runoff losses. This TMDL does not explicitly estimate or model the contribution of manure to surface waters in the Cottonwood River Watershed; however, nutrient loads modeled by HSPF are calibrated using monitored, in-stream water quality data at several points throughout the watershed and manure contributions to nutrient loads are therefore implicit.

The active feedlot spatial dataset was extracted from the Minnesota Geospatial Commons. Feedlot data was intersected with impaired reach watersheds and queried to only include active feedlot registration. Table 12 provides a breakdown of AUs within each *E. coli* impaired reach and impaired lake by animal type: beef cattle, dairy cattle, swine, sheep, horses, and poultry. The “other” category encompasses AUs that do not fit into the category (i.e., llamas or alpaca). The MPCA feedlot dataset includes several subdivisions of beef cattle by age and weight; dairy cattle are similarly divided. The beef cattle animal count includes the following: steer, heifer, cow/calf pairs, and calves. Dairy cattle were summed from

the following categories: cattle less than 1,000 lbs, heifers, calves, and cattle greater than 1,000 lbs. Poultry includes turkeys, chickens, and fowl produced for consumption.

Table 12. MPCA registered livestock animal types within each *E. coli* impaired reach and impaired lake drainage area in the Cottonwood River Watershed.

Impaired Reach/Lake	Impairment Type	Active Operations	Total AUs	Animal Units (AUs)						
				Beef Cattle	Dairy Cattle	Swine	Sheep	Horse	Poultry	Other
Cottonwood River Reach 502	<i>E. coli</i>	47	19,325	8,944	6	10,045	87	-	243	-
Judicial Ditch 30 Reach 511	<i>E. coli</i>	38	10,945	3,530	1,159	6,224	20	12	-	-
Highwater Creek Reach 519	<i>E. coli</i>	59	16,618	8,490	2,630	5,035	432	8	3	20
Dry Creek Reach 520	<i>E. coli</i>	29	5,933	4,485	390	1,008	2	18	1	29
Mound Creek Reach 521	<i>E. coli</i>	40	14,146	8,395	59	5,677	8	7	-	-
Pell Creek Reach 523	<i>E. coli</i>	12	1,799	1,730	-	60	8	1	-	-
Coal Mine Creek Reach 604	<i>E. coli</i>	12	4,013	1,051	190	1,665	-	-	1,107	-
Coal Mine Creek Reach 609	<i>E. coli</i>	29	9,625	3,380	861	5,380	-	4	-	-
Bean Lake	Nutrients	-	-	-	-	-	-	-	-	-
Double Lake	Nutrients	1	200	-	-	200	-	-	-	-
Rock Lake	Nutrients	6	1,631	474	-	1,071	86	-	-	-
Clear Lake	Nutrients	6	272	85	140	30	-	17	-	-
Altermatt Lake	Nutrients	4	1,486	1,294	-	192	-	-	-	-
Boise Lake	Nutrients	1	900	-	-	900	-	-	-	-
Bachelor Lake	Nutrients	-	-	-	-	-	-	-	-	-
Entire Watershed	All	639	168,537	79,039	10,940	73,041	1,065	204	4,047	199

Urban Stormwater

Cities and developed areas can be a source of sediment, bacteria, and nutrients to surface waters through the impact of urban systems on stormwater runoff. Stormwater runoff, which delivers and transports pollutants to surface waters, is generated in the watershed during precipitation events. The sources of pollutants in stormwater are many, including decaying vegetation (leaves, grass clippings, etc.), domestic and wild animal waste, soil, and deposited particulates from the air, road salt, and oil and grease from vehicles.

Although land cover in the Cottonwood River Watershed is predominantly cultivated crops, there are a few medium sized cities located throughout the watershed. The city of New Ulm (MS400228; population 13,287) and a small portion of the city of Marshall (MS400241; population 13,608) are located in the eastern and western portion of the watershed, respectively. These cities are the only communities in the watershed that are subject to the MPCA's MS4 General Permit (MNR040000) program. MS4s are defined by the EPA as stormwater conveyance systems owned or operated by an entity such as a state, city, township, county, district, or other public body having jurisdiction over disposal of stormwater or other wastes. The municipal stormwater permit holds permittees responsible for stormwater discharging from the conveyance system they own and/or operate. The conveyance system includes ditches, roads, storm sewers, stormwater ponds, etc. Under the NPDES stormwater program, permitted MS4 entities are required to obtain a permit, then develop and implement an MS4 Stormwater Pollution Prevention Program (SWPPP), which outlines a plan to reduce pollutant discharges, protect water quality, and satisfy water quality requirements in the Clean Water Act. An annual report is submitted to the MPCA each year by the permittee documenting progress on implementation of the SWPPP.

In addition to New Ulm and Marshall, there are 26 smaller municipalities throughout the Cottonwood River Watershed that are not subject to MS4 permits (Table 13). Sediment and phosphorus loading from urban areas (both MS4 and non-MS4 communities) was estimated using the Cottonwood River Watershed HSPF model. The HSPF model estimates that urban areas account for approximately 8% of the TSS load and 3% of the TP load across the entire Cottonwood River Watershed. Sections 3.6.1 and 3.6.3 present urban TSS and TP source contributions for the individual reach and lake impairments covered in this TMDL.

Table 13. Municipalities in the Cottonwood River Watershed.

City/Township	County	Downstream Impairment(s)	Area in Watershed [acres]	Population	Sewered (Sanitary)	MS4
Amiret*	Lyon	504, 508	84	235	Individual	No
Balaton	Lyon	502, 504, 508, 509	65	524	Ponds	No
Clements	Redwood	509, 599	243	185	Ponds	No
Cobden	Brown	599	635	23	MSTS****	No
Dotson*	Brown	508	672	10**	Individual	No
Dovray	Murray	518	74	69	MSTS****	No
Dudley*	Lyon	504, 508	696	10**	Individual	No
Evan	Brown	--	2	51	Ponds	No
Garvin	Lyon	502, 504, 508, 509	170	120	Ponds	No
Jeffers	Cottonwood	508	80	419	Ponds	No
Lamberton	Redwood	504, 508, 509, 517, 518	474	844	Ponds	No
Leavenworth*	Brown	508	530	267	Individual	No
Lucan	Redwood	509, 599	195	175	Ponds	No
Marshall***	Lyon	504, 508, 509	699	12,432	Mechanical	Yes
New Ulm***	Brown	--	2,878	13,362	Mechanical	Yes
Revere	Redwood	504, 508, 509, 523	368	100	Ponds	No
Rowena*	Redwood	599	780	20**	Individual	No
Sanborn	Redwood	508, 509	1,356	337	Ponds	No
Sleepy Eye	Brown	511,	1,340	3,498	Ponds	No
Springfield	Brown	508, 509	1,193	2,039	Mechanical	No
Storden	Cottonwood	508, 509, 517, 519	208	248	Ponds	No
Tracy	Lyon	504, 508, 509	1,434	2,110	Ponds	No
Wabasso	Redwood	509, 599	544	636	Mechanical	No
Walnut Grove	Redwood	504, 508, 509, 603, 523	685	821	Mechanical	No
Wanda	Redwood	509, 599	168	59	Ponds	No
Westbrook	Cottonwood	518, 508, 509, 517, 519	424	756	Ponds	No

*Unincorporated

**2010 Census Population

***Value from previous TMDL report (RCRCA 2013)

****Mid-size Subsurface Treatment System (MSTS)

Near-Channel Sources

Near-channel sources of sediment and nutrients are those in close proximity to the stream channel, including bluffs, banks, ravines, and the stream channel itself. Hydrologic changes in the landscape and altered precipitation patterns driven by climate change can lead to increased TSS and sediment-bound phosphorus in surface waters. Subsurface drainage tiling, channelization of waterways, land cover alteration, and increases in impervious surfaces all decrease detention time in the watershed and increase flow from fields and in streams. Draining and tiling wetland areas can decrease water storage on the landscape, which can lead to lower evapotranspiration and increased river flow (Schottler et al. 2013).

The straightening and ditching of natural rivers increase the slope of the original watercourse and moves water off the land at a higher velocity in a shorter amount of time. These changes to the way water moves through a watershed and how it makes its way into a river can lead to increases in water velocity, scouring of the river channel, and increased erosion of the river banks (Schottler et al. 2013, Lenhart et al. 2013).

For the purposes of this TMDL, near-channel TSS and TP loading from ravines, bluffs, and streambanks were estimated using the Cottonwood River Watershed HSPF model. The HSPF sediment simulation is based on multiple research efforts from various watersheds in the Minnesota River Basin. The partitioning of watershed and near-channel sources is based primarily on analysis of sediment cores (Schottler et al. 2010) and sediment mass balance studies for the Le Sueur River and Greater Blue Earth River watersheds (Gran et al. 2011; Bevis 2015). The model parameters developed for these watersheds were applied to the rest of the Minnesota River Basin, including the Cottonwood River Watershed. Model documentation (Tetra Tech 2016 and 2019) contains additional details about the model development and calibration. HSPF model output suggests approximately 65% of the TSS load and 4% of the TP load at the outlet of the Cottonwood River Watershed comes from near-channel sources. Sections 3.6.1 and 3.6.3 below contain more detailed discussion of the modeled near-channel source contributions for each impaired stream reach.

Additionally, the Cottonwood River Watershed Characterization Report (DNR 2020) provides an in-depth discussion of the processes, sources, and potential strategies to address near-channel sources in the Cottonwood River Watershed. This report includes the following components: characterization of the watershed, analysis of historical and existing hydrological data, assessment of geomorphic conditions and stream connectivity throughout the watershed.

Internal Loading (Lakes)

For many lakes, especially shallow lakes, internal loading can represent a significant portion of the annual TP load. Internal load can come from several sources including soluble phosphorus release from the sediment, rough fish (i.e., common carp), submerged aquatic vegetation (SAV), wind resuspension and physical disturbances such as motorized boat traffic.

Under anoxic conditions at the lake bottom, weak iron-phosphorus adsorption bonds on sediment particles break, releasing phosphorus into the water column. In shallow lakes that undergo intermittent mixing of the water column throughout the growing season, the released phosphorus can mix with surface waters throughout the summer and become available for algal growth. In deeper lakes with a more stable summer stratification period, the released phosphorus has the potential to remain in the bottom water layer throughout much of the growing season until stratification breaks down in late summer or fall. In many lakes, high sediment phosphorus release rates (RRs) are the result of a large pool of phosphorus in the lake bottom that has accumulated over several decades of watershed loading to the lake. Thus, even if significant watershed load reductions have been achieved through BMPs and other efforts, internal loading from the sediment can remain high and in-lake water quality may not improve.

Common carp and other rough fish uproot aquatic macrophytes during feeding and spawning and re-suspend bottom sediments, releasing phosphorus into the water column and decreasing water clarity.

Additionally, wind energy and motor boat traffic in shallow depths can disturb sediment that can be mixed into the water column and represent another potential source of internal load.

Certain SAV species such as invasive curly-leaf pondweed (CLP) can outcompete and suppress native vegetation species. CLP begins its growth cycle earlier in the season compared to other species and typically dies back in mid-summer. As a result, lakes with heavy CLP infestation can have little or no submerged vegetation by late summer. This can cause lower DO levels, increased sediment re-suspension, and phosphorus release from sediment. Eurasian watermilfoil, which is present in many lakes throughout Minnesota, is not considered a phosphorus source during the summer growing season, but is an invasive species that can out-compete native vegetation and negatively impact recreational activity.

Septic and Unsewered Communities

Failing SSTS near waterways can be a source of bacteria, phosphorus, and nitrogen to streams and lakes, especially during low flow periods when these sources continue to discharge and runoff driven sources are not active. SSTS can fail for a variety of reasons including excessive water use, poor design, physical damage, and lack of maintenance. Common limitations that contribute to failure include seasonal high-water table, fine-grained soils, bedrock, and fragipan (i.e., altered subsurface soil layer that restricts water flow and root penetration). SSTS can fail hydraulically through surface breakouts or hydrologically from inadequate soil filtration.

The MPCA differentiates between systems that fail to protect groundwater (FTPGW) and those that are an imminent threat to public health and safety (ITPHS). Generally, FTPGW systems are those that do not provide adequate treatment and may contaminate groundwater. For example, a system deemed failing to protect groundwater may have a functioning, intact tank and soil absorption system, but fails to protect groundwater by providing a less than sufficient amount of unsaturated soil between where the sewage is discharged and the periodically saturated soil level or bedrock. FTPGW systems can also include, but are not limited to the following:

- Seepage pits/cesspools/drywells/leaching pits
- Systems with less than the required vertical separation
- Systems not abandoned in accordance with Minn. R. 7080.2500

Systems considered ITPHS are severely failing or were never designed to provide adequate raw sewage treatment. These include SSTS and straight pipe systems that transport raw or partially treated sewage directly to a lake, stream, drainage system, or ground surface. ITPHS systems can include, but are not limited to the following:

- Straight pipes
- Sewage surfacing in the yard
- Sewage backing up into the home
- Unsafe tank lids
- Structurally unsound tanks
- Unsafe electrical conditions

Currently, the exact number and status of SSTs in the Cottonwood River Watershed is unknown. However, each year every county in the state reports estimated FTPGW and ITPHS compliance rate estimates to the MPCA. This TMDL report's bacteria source assessment (Section 3.6.2) and lake nutrient source assessment (Section 3.6.3) utilizes the most recent estimated rates reported by the county to the MPCA (Table 14; MPCA personal communication 2018). It should be noted that these rates are county-wide estimates and were developed using a wide range of methods and resources and are intended for planning purposes only.

Table 14. Estimated SSTs compliance rates by county in the Cottonwood River Watershed (MPCA personal communication 2018).

County	FTPGW SSTs	ITPHS SSTs
Brown	20%	24%
Cottonwood	40%	39%
Lyon	24%	5%
Murray	15%	10%
Redwood	30%	5%

Note: Estimated compliance rates reported by county and supplied to MPCA. Intended for planning purposes only.

Municipal and Industrial Wastewater

Domestic, commercial, and industrial wastewaters are collected and treated by municipalities before being discharged to water bodies as municipal wastewater effluent. Treated industrial wastewaters and cooling waters from industries, businesses, and other privately owned facilities may also be discharged to surface waters. Both municipal and industrial wastewater dischargers must obtain NPDES permits. There are no industrial wastewater dischargers in the watershed.

There are 16 active permitted municipal wastewater facilities that discharge to the impaired reaches covered in this TMDL (Table 15). Other permitted wastewater facilities that do not discharge pollutants of concern for this TMDL include Erickson Handi Mart (509) and Highwater Ethanol, LLC (517 and 518).

Table 15. Municipal wastewater treatment facilities within the impaired reach watersheds in the Cottonwood River Watershed.

Facility Name	NPDES ID#	Facility Type	Impaired Reach(es)
Balaton WWTP	MN0020559	Municipal	502, 504, 508, 509
Clements WWTP	MNG580094	Municipal	509, 599
Garvin WWTP	MNG580101	Municipal	502, 504, 508, 509
Jeffers WWTP*	MNG580111	Municipal	
Lamberton WWTP	MNG580100	Municipal	508, 509, 517, 518
Lucan WWTP	MNG580112	Municipal	509, 599
Revere WWTP	MNG580114	Municipal	504, 508, 509, 523
Sanborn WWTP	MNG580115	Municipal	508, 509
Sleepy Eye WWTP	MNG580041	Municipal	511
Springfield WWTP	MN0024953	Municipal	508, 509
Storden WWTP	MNG580106	Municipal	517, 508, 509, 519
Tracy WWTP	MN0021725	Municipal	504, 508, 509
Wabasso WWTP	MN0025151	Municipal	509, 599

Facility Name	NPDES ID#	Facility Type	Impaired Reach(es)
Walnut Grove WWTP	MN0021776	Municipal	504, 508, 509, 523
Wanda WWTP	MNG580126	Municipal	509, 599
Westbrook WWTP	MNG580127	Municipal	517, 508, 509, 519

*Jeffers WWTP is physically located in the Cottonwood River Watershed but discharges outside of the watershed via JD 9 to Little Cottonwood River (Minnesota River-Mankato Watershed)

Construction and Industrial Stormwater

Construction stormwater is regulated through an NPDES permit (MNR100001). Untreated stormwater that runs off construction sites often carries sediment to surface water bodies. Because phosphorus travels adsorbed to sediment, construction sites can also be a source of phosphorus to surface waters. Phase II of the stormwater rules adopted by the EPA requires an NPDES permit for a construction activity that disturbs one acre or more of soil; a permit is needed for smaller sites if the activity is either part of a larger development or if the MPCA determines that the activity poses a risk to water resources. Coverage under the construction stormwater general permit requires sediment and erosion control measures that reduce stormwater pollution during and after construction activities.

Industrial stormwater is regulated through an NPDES permit (MNR050000) or Nonmetallic Mining & Associated Activities general permit (MNG490000) when stormwater discharges have the potential to come into contact with materials and activities associated with the industrial activity. It is estimated that a small percent of the project area is permitted through the industrial stormwater permit, and industrial stormwater is not considered a significant source. On average, there is one permitted industrial stormwater site in every 53 square miles of the Cottonwood River Watershed.

On average, based on watershed-wide data, less than 0.2% of the watershed area is permitted under the construction and industrial stormwater permit in any given year. Thus, construction and industrial stormwater is not considered a significant source of sediment, and phosphorus throughout the Cottonwood River Watershed.

Natural Bacterial Reproduction

It has been suggested that *E. coli* bacteria has the capability to reproduce naturally in water and sediment and therefore should be taken into account when identifying bacteria sources. Two Minnesota studies describe the presence and growth of “naturalized” or “indigenous” strains of *E. coli* in watershed soils (Ishii et al. 2010), and ditch sediment and water (Sadowsky et al. 2015). The latter study, supported with Clean Water Land and Legacy funding, was conducted in the Seven Mile Creek Watershed, an agricultural landscape in south central Minnesota. DNA fingerprinting of *E. coli* from sediment and water samples collected in Seven Mile Creek from 2008 through 2010 resulted in the identification of 1,568 isolates comprised of 452 different *E. coli* strains. Of these strains, approximately 64% were represented by a single isolate, suggesting new or transient sources of *E. coli*. The remaining 36% of strains were represented by multiple isolates, suggesting persistence of specific *E. coli*. Discussions with the primary author of the Seven Mile Creek study suggest that while 36% might be used as a rough indicator of “background” levels of bacteria at this site during the study period, this percentage is not directly transferable to the concentration and count data of *E. coli* used in water quality standards and TMDLs. Additionally, because the study is not definitive as to the ultimate origins of this bacteria, it would not be appropriate to consider it as “natural” background.

Natural reproduction of *E. coli* is included in the LA; however, it is not broken out as a separate allocation.

Below is a summary of other recent studies that have found the persistence of *E. coli* in soil, beach sand, and sediments throughout the year in the United States without the continuous presence of sewage or mammalian sources.

- An Alaskan study (Adhikari et al. 2007) found that total coliform bacteria in soil were able to survive for six months in subfreezing conditions.
- A study in Michigan (Marino and Gannon 1991) documented survival and growth of fecal coliform in storm sewer sediment.
- Two studies in Maryland (Park et al. 2016; Pachepsky et al. 2016) demonstrated that release of *E. coli* from streambed sediments during baseflow periods is substantial and that water column *E. coli* concentrations are dependent on not only land management practices but also in-stream processes.

3.6.1 Stream TSS Source Summary

As discussed in the previous section, sediment loading to streams can come from both external and internal sources. External sources of TSS include sediment loading from permitted sources such as construction and industrial stormwater, runoff from urban areas, wastewater effluent; as well as nonpermitted sources such as overland erosion from cropland, hay/pasture, forest, and rangeland. Potential internal sources of sediment include bank erosion and in-channel algal production. This TMDL used the Cottonwood River Watershed HSPF model to evaluate sediment loading from various sources to each of the 11 TSS impaired reaches. Figure 6 and Table 15 present HSPF predicted annual TSS loads to each impaired reach by major source category.

Chl-*a* data for each impaired reach was also reviewed to determine whether algae growth is a potential source of turbidity/TSS and poor water clarity. Six of the 11 impaired reaches have Chl-*a* data (Table 16). Chl-*a* concentrations in four of the six reaches with data have at least one exceedance of the State's eutrophication criteria of 35 µg/L for streams in the South River Nutrient Region, suggesting algae may be a source of turbidity/TSS. Most of these exceedances occurred during late summer (August and September) low flow conditions. More data will need to be collected to fully assess algal turbidity in the TSS impaired reaches.

Figure 6. TSS contributions by source for each impaired reach estimated using the Cottonwood River Watershed HSPF model.

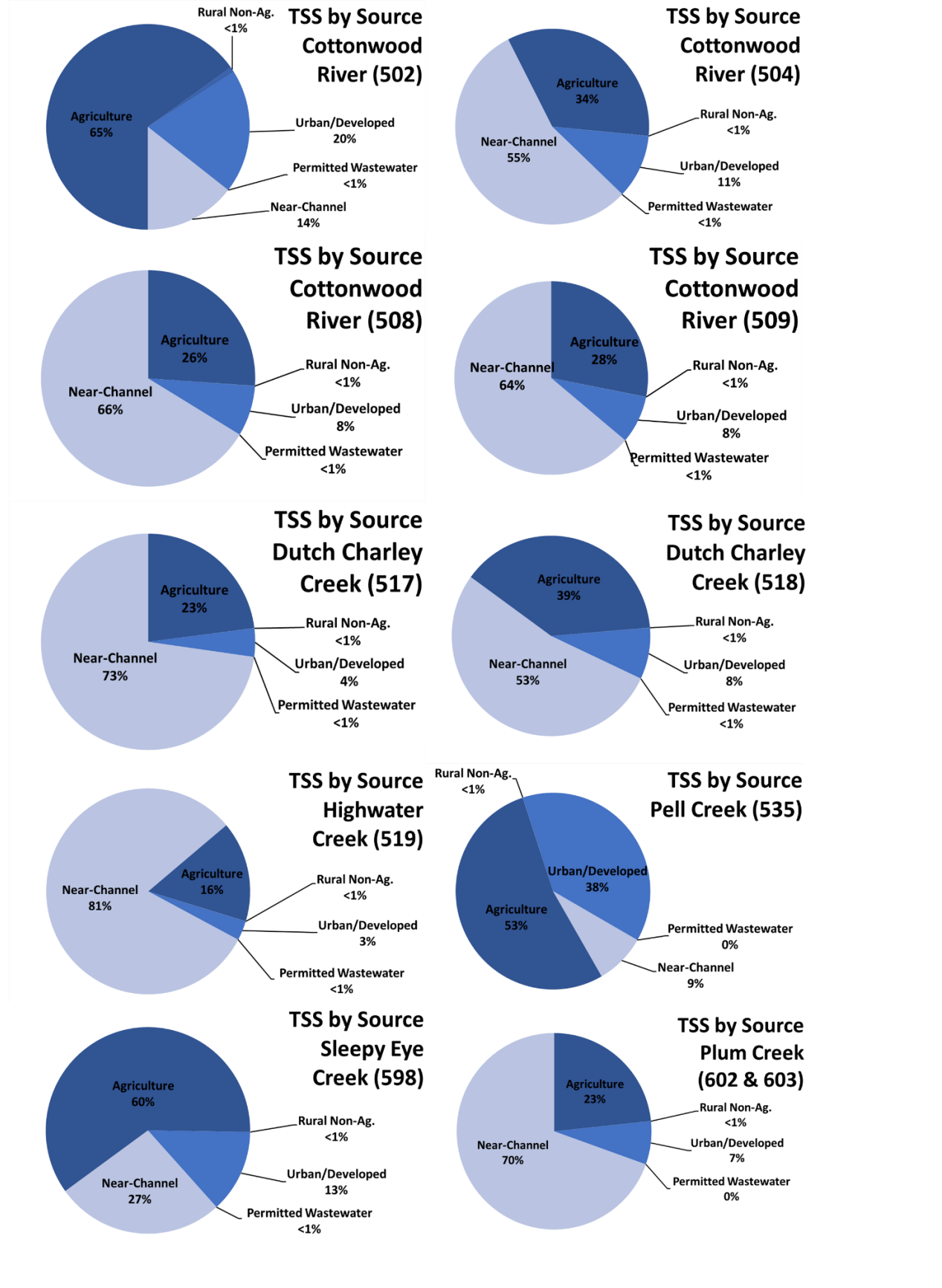


Table 16. TSS source assessment by land use category in the Cottonwood River Watershed.

Note: Numbers in this table are based on HSPF average annual TSS loads for model years 1996-2017.

Impaired Reach Description	Reach ID	Units	HSPF Model Estimates						Total	Chl- α Data
			Agriculture ¹	Rural Non-Ag. ²	Urban/Developed ³	Permitted Wastewater	Near-Channel ⁴			
Cottonwood River: Headwaters to Meadow Creek	502	tons/yr	1,578	21	472	2	349	2,423	Of the 15 samples collected, none exceed 35 $\mu\text{g/L}$ (average = 5 $\mu\text{g/L}$)	
		percent	65%	<1%	20%	<1%	14%	100%		
Cottonwood River: Plum Creek to Dutch Charley Creek	504	tons/yr	9,020	15	2,799	27	14,660	26,521	Of the 8 samples collected, none exceed 35 $\mu\text{g/L}$ (average = 16 $\mu\text{g/L}$)	
		percent	34%	<1%	11%	<1%	55%	100%		
Cottonwood River: Coal Mine Creek to Sleep Eye Creek	508	tons/yr	18,824	20	5,461	35	47,800	72,140	Of the 8 samples collected, two exceed 35 $\mu\text{g/L}$ (average = 24 $\mu\text{g/L}$)	
		percent	26%	<1%	8%	<1%	66%	100%		
Cottonwood River: Sleepy Eye Creek to JD 30	509	tons/yr	24,596	46	6,961	26	55,824	87,452	No data has been collected	
		percent	28%	<1%	8%	<1%	64%	100%		
Dutch Charley Creek: Highwater Creek to Cottonwood River	517	tons/yr	7,044	6	1,303	10	22,299	30,662	Of the 8 samples collected, one exceeds 35 $\mu\text{g/L}$ (average = 15 $\mu\text{g/L}$)	
		percent	23%	<1%	4%	<1%	73%	100%		
Dutch Charley Creek: Headwaters to Highwater Creek	518	tons/yr	2,202	2	472	2	3,016	5,694	No data has been collected	
		percent	39%	<1%	8%	<1%	53%	100%		
Highwater Creek: Double Lake outlet to Dutch Charley Creek	519	tons/yr	3,898	16	751	3	20,025	24,693	Of the 10 samples collected, one exceeds 35 $\mu\text{g/L}$ (average = 10 $\mu\text{g/L}$)	
		percent	16%	<1%	3%	<1%	81%	100%		
Pell Creek: Headwaters to T109 R38W S29, east line	535	tons/yr	208	<1	149	--	33	390	No data has been collected	
		percent	53%	<1%	38%	0%	9%	100%		
	599	tons/yr	5,410	1	1,172	5	2,393	8,981		

Impaired Reach Description	Reach ID	Units	HSPF Model Estimates						Chl- <i>a</i> Data
			Agriculture ¹	Rural Non-Ag. ²	Urban/Developed ³	Permitted Wastewater	Near-Channel ⁴	Total	
Sleepy Eye Creek: T109 R33W S5, west line to Cottonwood River		percent	60%	<1%	13%	<1%	27%	100%	Of the 17 samples collected, two exceed 35 µg/L (average = 14 µg/L)
Plum Creek: Headwaters to Cottonwood River	602, 603	tons/yr	1,942	2	592	--	5,786	8,322	No data has been collected
		percent	23%	<1%	7%	0%	70%	100%	

¹ Includes cultivated cropland, grassland, hay/pasture

² Includes forest and shrubland, groundwater, wetlands and open water

³ Includes MS4 and non-MS4 urban stormwater and city/county/state roadways

⁴ Includes bluff and bed/bank erosion

3.6.2 Stream *E. coli* Source Summary

The primary *E. coli* sources considered for this TMDL include livestock, stormwater runoff from urban areas, wildlife, wastewater treatment plants (WWTPs), and ITPHS SSTS. Use of watershed models for estimating relative contributions of *E. coli* sources delivered to streams is difficult and generally has high uncertainty. Thus, a simpler desktop bacteria accounting exercise was conducted to provide a general estimate of the total amount of bacteria produced by each potential source within the impaired reach watersheds. This exercise was done using various GIS layers and other information, including: MPCA registered feedlot GIS layer, literature rates of livestock and domestic animals, 2010 census data for urban and rural areas, SSTS failure rates reported by county, and DNR wildlife population studies. Appendix A presents results of the desktop bacteria production exercise for each impaired reach watershed. Table 17 below provides a general summary of the accounting exercise along with notes and discussion of local knowledge, data gaps, and additional information that would further refine our understanding of bacteria sources of the impaired reaches. It is important to point out that the desktop bacteria production exercise is not based on a quantitative assessment of *E. coli* loads delivered to surface waters. At this time, there is no microbial source tracking information (e.g., DNA fingerprinting) available to determine the exact source(s) of elevated bacteria observed within each impaired reach.

In general, livestock animals were by far the biggest bacteria producer within all the impaired reach drainage areas. Bacteria production for ITPHS AUs across the impaired reach drainage areas was significantly low compared to livestock production. The production exercise estimates that there are ~125 ITPHS SSTS systems throughout the eight impaired reach drainage areas. Although these numbers are relatively low, ITPHS systems that discharge near the impaired reach or a major tributary may be a critical source, particularly during low flow conditions.

Review of discharge monitoring data (Appendix B) from the seven point-source dischargers (see Section 4.3.2) located within the impaired reach watersheds suggest *E. coli* effluent concentrations are typically well below the *E. coli* standard. Thus, these point sources are not considered a source of concern. Since urban/developed land accounts for less than 10% (Table 6) of the land use within the impaired reach drainage areas, urban sources (i.e., domestic pets) represent a very small portion of the total bacteria produced in the watersheds.

Wildlife, which includes deer and waterfowl, also represents a small portion of the bacteria produced in the impaired reach watersheds. Deer and waterfowl numbers in the impaired reach watersheds were estimated using areal rates reported in the Deer Population Model (DNR 2011a) and Waterfowl Breeding Population Survey (DNR 2011b) studies. Thus, these estimates do not identify or directly account for areas in which wildlife inputs may be elevated. These could include but are not limited to open water areas with high waterfowl densities and lawns or golf courses near streams where geese or other waterfowl congregate.

Table 17. E. coli source summary for each impaired reach covered in this TMDL. Based on data collected between 2000 – 2017.

Impaired Reach	Cropland/Manure	Livestock/Pastures near Streams	Wildlife	Urban	WWTPs	SSTS	Upstream Reach(es)	In-stream (sediment)	Notes
Cottonwood River Reach 502	•	○	-	-	X	●/○	X	?	<ul style="list-style-type: none"> Exceedances occur during high (100%), mid (100%) and low (100%) flow conditions. No samples collected during very high or very low flow conditions. 3% of the MPCA registered livestock in the watershed are in close proximity to streams/waterways.
Judicial Ditch 30 Reach 511	•	-	-	-	-	●/○	•	?	<ul style="list-style-type: none"> Exceedances occur during high (100%) and mid (100%) flow conditions. No samples collected during very high, low, or very low flow conditions. Less than 1% of the MPCA registered livestock in the watershed are in close proximity to streams/waterways.
Highwater Creek Reach 519	•	•	-	-	-	●/○	X	?	<ul style="list-style-type: none"> Exceedances occur during very high (100%), high (100%) and mid (100%) flow conditions. No samples collected during low or very low flow conditions. 33% of the MPCA registered livestock in the watershed are in close proximity to streams/waterways.
Dry Creek Reach 520	•	○	-	-	X	●/○	X	?	<ul style="list-style-type: none"> Exceedances occur during very high (100%), high (100%) and mid (100%) flow conditions. No samples collected during low or very low flow conditions. 1% of the MPCA registered livestock in the watershed are in close proximity to streams/waterways.
Mound Creek Reach 521	•	○	-	-	X	●/○	X	?	<ul style="list-style-type: none"> Exceedances occur during very high (100%), high (100%), mid (100%) and low (100%) flow conditions. No samples collected during very low flow conditions. 6% of the MPCA registered livestock in the watershed are in close proximity to streams/waterways.
Pell Creek Reach 523	•	-	-	-	-	●/○	X	?	<ul style="list-style-type: none"> Exceedances occur during high (100%) and mid (100%) flow conditions. No samples collected during very high, low, or very low flow conditions. Less than 1% of the MPCA registered livestock in the watershed are in close proximity to streams/waterways.
Coal Mine Creek Reach 604	•	-	-	-	X	●/○	X	?	<ul style="list-style-type: none"> Exceedances occur during very high (100%), high (94%), mid (100%) and low (100%) flow conditions. No samples collected during very low flow conditions. None of the MPCA registered livestock in the watershed are in close proximity to streams/waterways.
Judicial Ditch 40 Reach 609	•	-	-	-	X	●/○	X	?	<ul style="list-style-type: none"> Exceedances occur during high (100%), mid (100%) and low (100%) flow conditions. No samples collected during very high or very low flow conditions. None of the MPCA registered livestock in the watershed are in close proximity to streams/waterways.

Key: • High potential contributor ○ Moderate potential contributor - Low potential contributor X Not considered a source at this time? Limited or no information available to assess.

3.6.3 Lake Phosphorus Source Summary

Lake response models were set up for each of the seven impaired lakes in the Cottonwood River Watershed to evaluate phosphorus sources and estimate annual phosphorus budgets. The lake response model selected for this exercise was the Canfield-Bachmann lake equation (Canfield and Bachmann, 1981). This equation estimates the lake phosphorus sedimentation rate, which is needed to predict the relationship between in-lake phosphorus concentrations and phosphorus load inputs. The phosphorus sedimentation rate is an estimate of net phosphorus loss from the water column through sedimentation to the lake bottom, and is used in concert with user supplied lake-specific characteristics such as annual phosphorus loading, mean depth, and hydraulic flushing rate to predict in-lake phosphorus concentrations. Model predictions are then compared to measured data to evaluate how well the model describes the lake system. If necessary, the model parameters are adjusted appropriately to achieve an approximate match to monitored data.

The five major phosphorus sources defined in the lake response models are atmospheric load, loading from SSTs, watershed load, loading from upstream impaired lakes, and internal load. Methods for estimating each of these sources are described below in more detail.

Atmospheric Loads

Atmospheric inputs of phosphorus from wet and dry deposition were estimated using published rates based on annual precipitation (Barr Engineering 2004). The atmospheric deposition values used for dry (<25 inches), average, and wet precipitation years (>38 inches) are 24.9, 26.8, and 29.0 kg/km²-year, respectively. These values are equivalent to 0.22, 0.24, and 0.26 lbs/acre/year for dry, average, and wet years, respectively.

SSTS Loads

Phosphorus loading from SSTs to each impaired lake was estimated using methods similar to the Lower Minnesota River Watershed TMDL (MPCA 2020a). First, the total number of people in each lakeshed was estimated 1) for households in shoreland areas (i.e., near the lake); and 2) for households outside shoreland (i.e., farther from lakes). To estimate the number of people living immediately adjacent to each lake, aerial photos were used to count the number of homes/cabins. This number was then multiplied by number of people per household (assumed to be 2.55 on average for the Minnesota River Basin; Barr Engineering 2004) and an adjustment factor to account for the assumption that approximately half of homes/cabins adjacent to lakes are used only four months each year (adjustment factor was 2/3). To estimate the number of people living farther from lakes, 2010 U.S. Census data was used, and the estimated number of people adjacent to each lake was subtracted from Census-estimated lakeshed numbers. Phosphorus load from SSTs was assumed to be 1.978 lbs of TP per person per year (Barr Engineering 2004) and was used in conjunction with the estimates above to obtain TP loading to SSTs each year.

To determine the TP loading leaving SSTs and entering each impaired lake, loads were calculated for each of the three types of SSTs: those labeled compliant, FTPGW, or ITPHS (see SSTs discussion in Section 3.6). Because the compliance status of SSTs in each lakeshed is not known at this time, 2018 county-wide estimated compliance rates were used for this calculation (Table 14; MPCA personal communication 2018). Phosphorus removal rates for SSTs in each of these compliance groups were

then applied: for SSTs adjacent to lakes, 80% removal rates were assumed for compliant systems, while 57% removal rates were assumed for both failing and ITPHS SSTs (Barr Engineering 2004). For SSTs farther from lakes, 90%, 70%, and 57% removal rates were assumed for compliant, failing, and ITPHS SSTs, respectively (Barr Engineering 2004). The phosphorus removal and soil phosphorus attenuation percentages assumed for conforming and nonconforming SSTs in this analysis are within the range of literature values (Viraraghavan and Warnock 1975; Reckhow and Simpson 1980; Kellogg et al. 1995; EPA 2002b; ENSR 2003) as reported by Barr Engineering in 2004. Finally, the sum was taken of phosphorus loading from all compliance groups and from households both adjacent to and farther from lakes to obtain TP loading to each impaired lake from SSTs.

Watershed Loads

Watershed flow and phosphorus loads to each impaired lake were estimated using the Cottonwood River Watershed HSPF model (Appendix D). HSPF-predicted average annual watershed runoff depths and TP concentrations to each impaired lake in the Cottonwood River Watershed ranged from 5 to 18 inches/year and 211-429 µg/L, respectively. HSPF utilizes several individual subroutines/models and assumptions to model hydrology and pollutant loading rate and transport, and therefore the watershed load to each lake can be further analyzed and broken down by sub-categories such as feedlots, manure, groundwater, bluff erosion, bed/bank erosion, and individual land uses (i.e., developed, forest, cropland, grassland, etc.). Figure 7 shows the HSPF-predicted average annual watershed TP inputs to each impaired lake while Appendix C contains a more detailed description of the HSPF-predicted watershed load broken down by the sub-categories described above. As shown in Appendix C, an overwhelming majority of the watershed load to each lake comes from cropland. The HSPF results presented in Appendix C are also summarized in Table 18.

Upstream Impaired Lake Loads

Double Lake is the only lake in the Cottonwood River Watershed that contains an upstream impaired lake (Bean Lake) in its drainage area. Outflow volumes from Bean Lake were estimated using the HSPF model and routed directly into Double Lake within the lake response model. Average TP loads from Bean Lake to Double Lake were then calculated by multiplying the HSPF-predicted flow volume by the average summer growing season monitored TP concentrations for Bean Lake.

Internal Loads

Internal loading for the Cottonwood River Watershed impaired lakes was estimated through a model residual approach whereby the other four sources (atmosphere, SSTs, watershed, and upstream lakes) were added to the models first, and then, if necessary, additional load was added to calibrate the models. This TMDL assumes that the additional loads are likely attributed to internal phosphorus loading from sediment, rough fish (i.e., common carp), vegetation (i.e., CLP) and/or wind/boat resuspension. It is also possible that a portion of the additional load needed to calibrate the models are the result of one (or more) of the other four sources being under-represented, or one or more loading source(s) that is not currently accounted for in the TP source assessment.

Although it is difficult and/or cost prohibitive to directly measure phosphorus inputs from sediment, fish, vegetation, and wind/boating, there are ways to evaluate whether these sources have significant potential to contribute to internal load. For example, internal loading from sediments can be estimated by combining sediment phosphorus RR estimates with an anoxic factor (AF) calculation (Nürnberg 2004).

Sediment phosphorus RRs were assessed as part of this TMDL for Double Lake by collecting intact sediment cores and incubating them in the laboratory under anoxic conditions. Results of this analysis (Table 18 and Appendix C) indicate that Double Lake (RR = 9.2 mg/m²/day) has high potential for sediment phosphorus release under anoxic conditions. The AF estimates the period of anoxia over the lake sediments and is calculated using temperature-DO profiles. AFs are often difficult to measure in shallow lakes, such as Double Lake, since they can have intermittent anoxic periods that aren't measured with routine monitoring. Nonetheless, AF was estimated for Double Lake (<5 days/year) using available temperature-DO profile data and then multiplied by the laboratory measured phosphorus RR and total area of Double Lake to estimate gross internal load. Results indicate that sediment release of phosphorus may be accounting for approximately 12% of the internal load in Double Lake. Watershed inputs to the lake will need to be monitored and compared to HSPF predicted model output in order to validate the lake response model and the impact of internal loading.

In-lake water quality, particularly in shallow lakes, is closely linked to the health and structure of the lake's biological communities. Water quality degradation can occur when certain aquatic invasive species (i.e., common carp) are present in high densities or certain native species (i.e., black bullhead, fathead minnow) become over-abundant thus creating an imbalanced fishery. Common carp uproot vegetation and re-suspend sediment which, when there are high densities of carp in a lake, can lead to increased water turbidity, reduced vegetation coverage, and lower waterfowl populations. Recent research suggests that these impacts begin to occur at common carp densities of ~100 kg of carp biomass/hectare (89 lbs/acre) (Bajer et al. 2009). In 2018, Wenck Associates, Inc. conducted common carp population assessments for Double Lake using standard electroshocking methods described in (Bajer and Sorensen 2012). Results of the Double Lake assessment indicate the lake has a common carp density (208 lbs/acre) that is more than double the critical threshold (89 lbs/acre), suggesting that common carp (and possibly other fish) are contributing to poor water quality and habitat degradation. Appendix C contains a detailed discussion of the common carp assessments for Double Lake. Sleepy Eye Lake (delisted in 2020) is also included.

Double Lake was the only impaired lake in the Cottonwood River Watershed assessed for common carp densities; however, at least one DNR trap and gill net survey has been performed on four impaired lakes covered in this TMDL. Three impaired lakes did not have a DNR fisheries survey on record. Common carp along with certain native fishes (i.e., largemouth bass) avoid standard trap and gill nets used by the DNR, therefore, other techniques such as the electroshocking method described above are needed to accurately estimate population numbers and densities that can be used to inform management strategies. That said, the DNR trap and gill net surveys provide a good indicator of the presence/absence of common carp, black bullhead and other species that may impact water quality. Review of historic DNR trap and gill net surveys noted the presence of black bullhead and common carp in four of the seven lakes (Table 18 and Appendix C). In many of the lakes, black bullhead and/or common carp comprised a large percentage of the fish sampled in the trap and gill nets and therefore it is likely that these species are impacting water quality in these systems.

The final phosphorus source assessment results for each impaired lake are shown in Figure 6 (phosphorus lbs per year). Table 18 provides a summary of the source categories that are of most concern for each impaired lake, based on the quantitative lake response model results (Figure 7) as well

as the sediment core and common carp survey results for Double Lake, the DNR fish surveys, and anecdotal information.

Figure 7. Average annual TP contributions by source based on HSPF and lake response modeling results in the Cottonwood River Watershed.

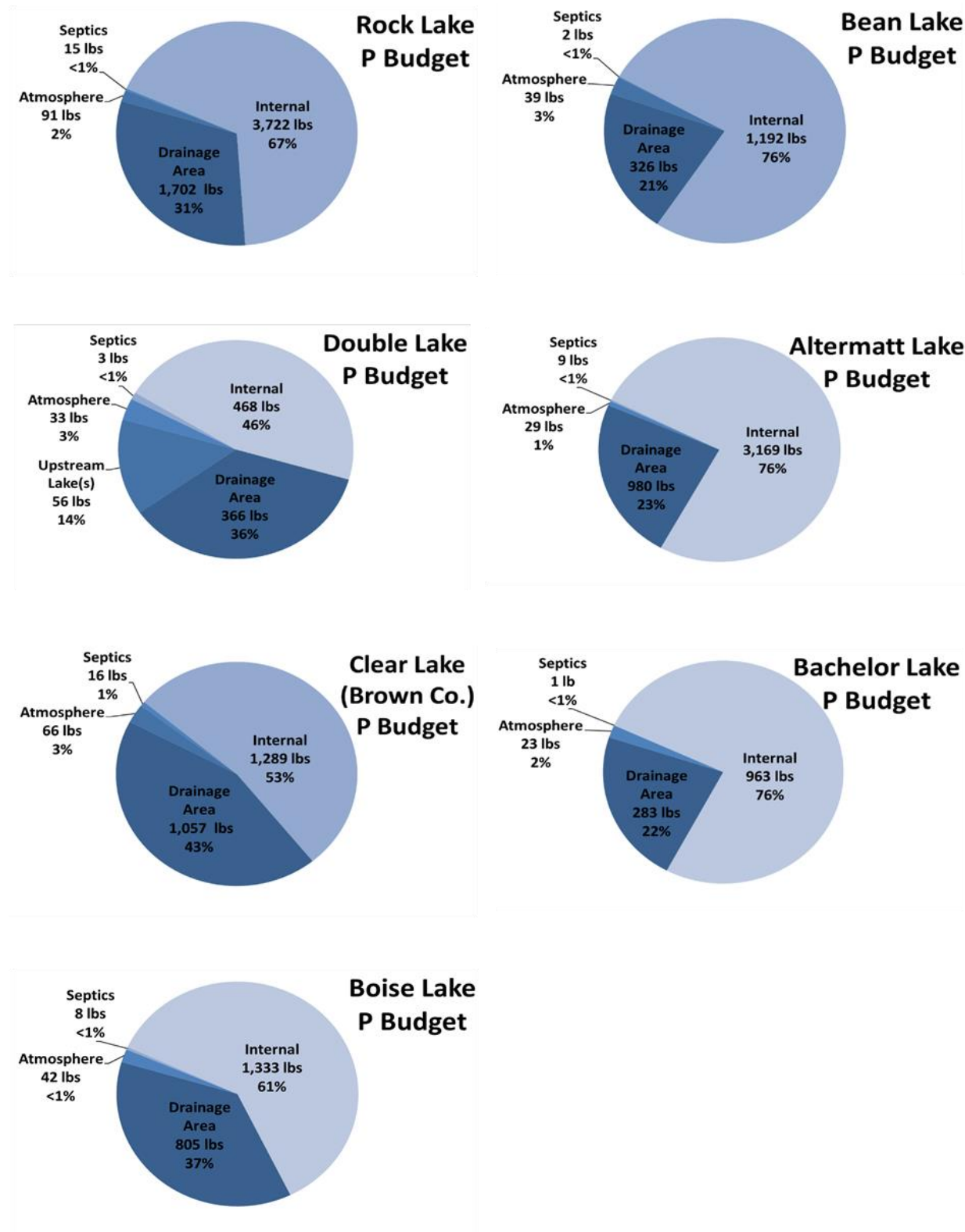


Table 18. TP source summary for each impaired lake covered in this TMDL.

Lake Name	Watershed Sources					Internal Sources			Upstream Impaired Lake(s)	Notes
	Agriculture ¹	Urban	SSTS	WWTPs	Upstream Lakes	Sediment Release	Aquatic Vegetation (i.e., curly-leaf pondweed)	Rough Fish (i.e., common carp)		
Rock	●	x	○	x	x	Δ	Δ	Δ	NA	DNR fish surveys observed a large presence of black bullhead and moderate presence of common carp in 2014. The internal loading rate (32.1 mg/m ² /day) based on the model residual approach is extremely high. The HSPF predicted average annual watershed TP concentration (286 μg/L) exceeds the 150 μg/L eutrophication standard.
Bean	●	x	○	x	x	Δ	Δ	Δ	NA	DNR fish surveys observed a very large presence of black bullhead and relatively low presence of common carp in 2014. The internal loading rate (17.9 mg/m ² /day) based on the model residual approach is high. The HSPF predicted average annual watershed TP concentration (211 μg/L) exceeds the 150 μg/L eutrophication standard.
Double (N. Pottion)	●	x	○	x	○	○	Δ	●	Bean	DNR fish surveys observed a large presence of black bullhead and moderate presence of common carp in 2015. A common carp population assessment conducted in 2018 suggested biomass density (~208 lbs/acres) was more than double the critical threshold (89 lbs/acre). Lab measured sediment RR (9.2 mg/m ² /day) is high compared to other lakes, however, DO profiles indicate low potential for anoxia (DO <2.0 mg/L) near the sediment/water interface. The HSPF predicted average annual watershed TP concentration (429 μg/L; does not include Lake Benton contribution) exceeds the 150 μg/L eutrophication standard.
Clear (Brown Co.)	●	x	○	x	x	Δ	Δ	Δ	NA	DNR fish surveys observed a large presence common carp and moderate presence of black bullhead in 2017. The internal loading rate (40.6 mg/m ² /day) based on the model residual approach is extremely high. The HSPF predicted average annual watershed TP concentration (167 μg/L; does not include Lake Benton contribution) exceeds the 150 μg/L eutrophication standard.
Altermatt	●	x	○	x	x	Δ	Δ	Δ	NA	No DNR fish surveys have been conducted on this lake. The internal loading rate (35.7 mg/m ² /day) based on the model residual approach is extremely high.

Lake Name	Watershed Sources					Internal Sources			Upstream Impaired Lake(s)	Notes
	Agriculture ¹	Urban	SSTS	WWTPs	Upstream Lakes	Sediment Release	Aquatic Vegetation (i.e., curly-leaf pondweed)	Rough Fish (i.e., common carp)		
										The HSPF predicted average annual watershed TP concentration (356 µg/L) exceeds the 150 µg/L eutrophication standard.
Boise	●	x	○	x	x	Δ	Δ	Δ	NA	No DNR fish surveys have been conducted on this lake. The internal loading rate (10.7 mg/m ² /day) based on the model residual approach is high. The HSPF predicted average annual watershed TP concentration (329 µg/L) exceeds the 150 µg/L eutrophication standard.
Bachelor	●	x	○	x	x	Δ	Δ	Δ	NA	No DNR fish surveys have been conducted on this lake. The internal loading rate (12.7 mg/m ² /day) based on the model residual approach is high. The HSPF predicted average annual watershed TP concentration (349 µg/L) exceeds the 150 µg/L eutrophication standard.

● Primary source ○ Secondary source x Not considered a primary or secondary source at this time Δ Potential source however not enough data/info available at this time to evaluate
Includes cropland, pasture/grassland, and feedlots. See Appendix C for more detail of each sub-category predicted by the HSPF model.

4. TMDL Development

4.1 TMDL Overview

A TMDL represents the total mass of a pollutant that can be assimilated by the receiving water without causing that receiving water to violate water quality standards. The TMDL is described as an equation with four different components, as described below:

$$\text{TMDL} = \text{LC} = \Sigma \text{WLA} + \Sigma \text{LA} + \text{MOS} + \text{RC}$$

Where:

LC = loading capacity; or the greatest pollutant load a water body can receive without violating water quality standards;

WLA = wasteload allocation; or the portion of the TMDL allocated to existing or future permitted point sources of the relevant pollutant;

LA = load allocation, or the portion of the TMDL allocated to existing or future nonpoint sources of the relevant pollutant;

MOS = margin of safety, or an accounting of uncertainty about the relationship between pollutant loads and receiving water quality. The MOS can be provided implicitly through analytical assumptions or explicitly by reserving a portion of loading capacity (EPA 1999).

RC = reserve capacity, an allocation of future growth. This is an MPCA-required element, if applicable (not applicable in this TMDL).

Per Code of Federal Regulations (40 CFR 130.2(1)), TMDLs can be expressed in terms of mass per time, toxicity or other appropriate measures. For this TMDL, the TMDLs, allocations and margins of safety are expressed in mass/day. Each of the TMDL components is discussed in greater detail in the following sections.

4.1.1 Model Approach

The Cottonwood River Watershed HSPF model was used to estimate watershed runoff and pollutant loading to the impaired lakes and reaches included in this TMDL. HSPF is a comprehensive watershed model of hydrology and water quality that includes modeling land surface and subsurface hydrologic and water-quality processes, which are linked and closely integrated with corresponding stream, wetland and reservoir processes. HSPF model applications can be used to determine critical environmental conditions (e.g., low/high flows or seasons) for the impaired segments by providing continuous flow and concentration predictions throughout the system.

HSPF models for the Cottonwood River Watershed were originally developed in 2012 and then updated in 2016 and 2019 to support this TMDL and other planning and management efforts in the watershed (Tetra Tech 2016 and 2019). The HSPF models predict the range of flows that have historically occurred in the modeled area, the load contributions from a variety of point and nonpoint sources in a watershed, and the source contributions when paired flow and concentration data are limited. Supporting documentation is available which discuss modeling methodologies, data used, and calibration results for the three major watershed HSPF models (Tetra Tech 2016 and 2019).

4.1.2 Load Duration Curve Approach

Pollutant loading capacity for the TSS and *E. coli* impaired stream reaches were developed using LDCs. LDCs incorporate flow and water quality across the reach flow zones, and provide loading capacities and a means of estimating load reductions necessary to meet water quality standards. To develop the LDCs, HSPF-simulated average daily flow values from 2008 through 2017 for each reach were multiplied by the appropriate water quality standard and converted to daily loads to create “continuous” LDCs. Because this method uses a long-term record of daily flows, virtually the full spectrum of allowable loading capacities is represented by the resulting curve.

In the TMDL equation tables of this TMDL, only five points on the entire loading capacity curve are depicted: very high flows (0% to 10%), high flows (10% to 40%), mid flows (40% to 60%), low flows (60% to 90%) and very low flows (90% to 100%). For simplicity, only the median (or midpoint) load of each flow zone is used to show the TMDL equation components in the TMDL tables. However, it should be understood that the entire curve represents the TMDL and is what is ultimately approved by the EPA. For the purposes of this TMDL, the baseline year for implementation will be 2012, which represents the mid-range year of the HSPF flow record used to construct the LDCs (See Section 8.2.3).

4.1.3 Natural Background Consideration

Natural background was given consideration in the development of LA in this TMDL. Natural background is the landscape condition that occurs outside of human influence. Minn. R. 7050.0150, subp. 4, defines the term “natural causes” as the multiplicity of factors that determine the physical, chemical, or biological conditions that would exist in a water body in the absence of measurable impacts from human activity or influence. Natural background conditions refer to inputs that would be expected under natural, undisturbed conditions. Natural background sources can include inputs from natural geologic processes such as soil loss from upland erosion and stream development, atmospheric deposition, and loading from forested land, wildlife, etc. For each impairment, natural background levels are implicitly incorporated in the water quality standards used by the MPCA to determine/assess impairment and therefore natural background is accounted for and addressed through the MPCA’s water body assessment process. Natural background conditions were also evaluated, where possible, within the modeling and source assessment portion of this TMDL. These source assessment exercises indicate natural background inputs are generally low compared to livestock, cropland, streambank, wastewater treatment facilities, failing SSTSs, and other anthropogenic sources.

Based on the MPCA’s water body assessment process and the TMDL source assessment exercises, there is no evidence at this time to suggest that natural background sources are a major driver of any of the impairments and/or affect the water bodies’ ability to meet state water quality standards. For all impairments addressed in this TMDL study, natural background sources are implicitly included in the LA portion of the TMDL allocation tables and TMDL reductions should focus on the major anthropogenic sources identified in the source assessment. Federal law instructs an agency to distinguish between natural and nonpoint source loads “[w]herever possible.” 40 CFR § 130.2(g). However, Minnesota law does not compel the MPCA to develop a separate LA for natural background sources. For more information, see [Crystal Lake TMDL Court of Appeals Decision](#); Filed February 4, 2019.

4.2 TSS - Streams

4.2.1 Loading Capacity Methodology

LDCs were used to represent the loading capacity (LC) for each TSS impaired reach. The flow component of the LC curve is based on the HSPF-simulated daily average flows (2008 through 2017), and the concentration component is the TSS concentration criteria of 65 mg/L. TSS LDCs for each impaired reach are shown in Section 4.2.6. On these figures, the red curve represents the allowable TSS LC of the reach for each daily flow. The median (or midpoint) load of each flow zone is used to represent the total LC in the TMDL tables. Each reach's LC can be compared to current conditions by plotting the measured load during each water quality sampling event (black circles in Figure 8 through Figure 17). Each value that is above the curve represents an exceedance of the water quality standard, while those below the line are below the water quality standard.

The existing concentration for each impaired reach was calculated as the 90th percentile of observed TSS concentrations for all flow zones for the months that the standard applies (April through September). The 90th percentile was used because the TSS standard states that the numeric criterion (65 mg/L) may be exceeded for no more than 10% of the time. The overall estimated concentration-based percent reduction needed to meet each TMDL was calculated as the existing concentration minus the TSS standard (65 mg/L), divided by the existing concentration. Also plotted in each LDC figure is the 90th percentile monitored TSS load for each individual flow zone (solid green circles). Plotting these individual loads help determine what flow zones and practices should be targeted to achieve the overall reduction goal for each impaired reach.

4.2.2 Wasteload Allocation Methodology

The WLAs for TSS were divided into three categories: NPDES permitted wastewater dischargers, NPDES MS4 stormwater, and NPDES permitted construction and industrial stormwater. The following sections describe how each WLA category was determined. The NPDES permitted livestock CAFOs are zero discharge facilities and are given a WLA of zero and should not impact water quality in the watershed as a point source. Therefore, it is not necessary to put them in the TSS TMDL tables in Section 4.2.6. Also, straight pipe septic systems are illegal and receive a WLA of zero. Therefore, it is not necessary to put them in the TSS TMDL tables.

NPDES Permitted Wastewater Dischargers

There are 14 active regulated NPDES wastewater dischargers in the Cottonwood River TSS impaired reach drainage areas that have been assigned TSS effluent limits. Facility maximum daily effluent TSS loads were established and provided by the MPCA and are a function of the facility design flows and permitted TSS concentration limits (Table 19). WLAs for each facility were calculated by multiplying the TSS effluent concentration limit, permitted facility design flow, and a unit conversion factor. All dischargers have TSS effluent concentration limits less than the TSS standard of 65 mg/L. Therefore, facilities that discharge consistent with their WLAs are not a cause for in-stream exceedances of the TSS standard within their receiving water bodies and no permit modifications are needed at this time for the TSS impairments. WLAs for continuously discharging municipal WWTPs were calculated based on the average wet weather design flow, equivalent to the wettest 30-days of influent flow expected over the

course of a year. Controlled municipal pond discharge WWTP WLAs were calculated based on the maximum daily volume that may be discharged in a 24-hour period.

Table 19. TSS allocations for NPDES permitted wastewater dischargers in the Cottonwood River Watershed.

Impaired Reach	Facility Name and System Type	NPDES ID#	Flow used for WLA* (MGD)	Permitted Concentration (mg/L)	Wasteload Allocation (lbs/day)
502, 504, 508, 509	Balaton WWTP/Pond	MN0020559	0.816	45	306
509, 599	Clements WWTP/Pond	MNG580094	0.163	45	61
502, 504, 508, 509	Garvin WWTP/Pond	MNG580101	0.169	45	63
508, 509, 517, 518	Lamberton WWTP/Pond	MNG580100	1.303	45	489
509, 599	Lucan WWTP/Pond	MNG580112	0.684	45	257
504, 508, 509	Revere WWTP/Pond	MNG580114	0.150	45	56
508, 509	Sanborn WWTP/Pond	MNG580115	0.342	45	128
508, 509	Springfield WWTP/Mechanical	MN0024953	0.780	30	195
517, 508, 509, 519	Storden WWTP/Pond	MNG580106	0.264	45	99
504, 508, 509	Tracy WWTP/Pond	MN0021725	3.495	45	1,312
509, 599	Wabasso WWTP/Mechanical	MN0025151	0.113	30	28
504, 508, 509	Walnut Grove WWTP/Mechanical	MN0021776	0.203	30	51
509, 599	Wanda WWTP/Pond	MNG580126	0.179	45	67
509, 517, 508, 519	Westbrook WWTP/Pond	MNG580127	1.629	45	611

*Average wet weather design flow or maximum daily pond flow in million gallons per day (MGD)

NPDES Permitted MS4 Stormwater

The city of Marshall, which contributes to reaches 504, 508, and 509, is the only city subject to the NPDES/SDS MS4 General Permit (MNR040000), within the Cottonwood River TSS impaired reach watersheds covered by this TMDL. Figure 2 and Appendix A show the city of Marshall’s municipal boundary and its location in the Cottonwood River Watershed. The city covers approximately 699 acres in the Cottonwood River Watershed, which is 0.2%, 0.1%, and 0.1% of the land area in the reach 504, 508, and 509 drainage areas, respectively. TSS allocations for the City of Marshall were calculated by multiplying each reach’s MS4 percent drainage area coverage (percentages stated above) by the total watershed loading capacity (determined by LDCs). However, as there was a TSS unimpaired assessed reach (07020008-601) between the city of Marshall’s outfall and the TSS impaired reaches, the City of Marshall isn’t required to make any reductions to meet the assigned WLAs.

NPDES Permitted Construction and Industrial Stormwater

Construction stormwater is regulated by NPDES General Permit (MNR100001) for any construction activity disturbing a) one acre or more of soil, b) less than one acre of soil if that activity is part of a "larger common plan of development or sale" that is greater than one acre, or c) less than one acre of soil, but the MPCA determines that the activity poses a risk to water resources. The WLA for stormwater

discharges from sites where there are construction activities reflects the number of construction sites expected to be active in the impaired reach watershed at any one time. Industrial stormwater is regulated by NPDES General Permit (MNR050000) or Nonmetallic Mining & Associated Activities General Permit (MNG490000) if the industrial activity has the potential for significant materials and activities to be exposed to stormwater discharges.

A categorical WLA was assigned to all construction activity in the watershed. Current acres under a Construction and Industrial Stormwater Permit in each major watershed were available through the MPCA's Permit database. The amount of land under Construction and Industrial Stormwater Permits in the Cottonwood River Watershed was divided by the total area of the watershed to determine the percent of permitted land. Results of this analysis show that approximately 0.15% of land in the Cottonwood River Watershed is currently under a Construction and Industrial Stormwater Permit. To determine the WLAs for these activities, total loading capacity in each flow zone was multiplied by the appropriate construction and industrial coverage percentage.

4.2.3 Load Allocation Methodology

As stated in the TMDL equation, the LA is comprised of the nonpoint source load that is allocated to an impaired reach after the WLAs (point sources, construction, and industrial stormwater) and MOS were determined and subtracted from the total LC for each reach and flow zone. This residual remaining LC is meant to represent all nonregulated (nonpoint) sources of TSS upstream of the impaired reach (summarized in Section 3.6). The LA, also referred to as the watershed LA, includes nonpoint pollution sources that are not subject to NPDES Permit requirements such as wind-blown materials, soil erosion from stream channel and upland areas, and natural background. The LA also includes runoff from agricultural lands, runoff from feedlots not operating under a NPDES or SDS permit, and non-NPDES stormwater runoff.

Given the complexity of sediment dynamics and a lack of sufficient historical data in the Cottonwood River Watershed, attempting to allocate a specific natural background load to any river or stream reach would result in a margin of error that in itself may be more than the estimated allocation. As such, the LA implicitly includes natural background without designating its own allocation. Schottler et al. (2010) and other resources included in Section 3.6 discuss this matter further.

4.2.4 Margin of Safety

The MOS is a portion of the TMDL that is set aside to account for the uncertainties associated with achieving water quality standards. The MOS can be either implicitly or explicitly defined as a set-aside amount. An explicit MOS was calculated as 5% of the loading capacity. Five percent was considered an appropriate MOS since the LDC approach minimizes a great deal of uncertainty. The LDC calculations are based on TSS target concentrations and modeled flow data that has been calibrated to long-term monitored flow data. Most of the uncertainty with this calculation is therefore associated with the HSPF-modeled flow output for each reach. The Cottonwood River HSPF model was calibrated and validated using 21 years (1996 through 2017) of flow data from five gaging stations throughout the watershed (Tetra Tech 2019). Calibration results indicate that the HSPF model is a valid representation of hydrological and chemical conditions in the watershed. See Appendix D of this TMDL for the HSPF model calibration and validation results. The TSS stream LDCs were developed using HSPF-modeled daily flow

data from April through September. The TSS TMDLs applied a MOS to each flow zone along the duration curves by subtracting 5% of the flow zones loading capacity.

4.2.5 Seasonal Variation and Critical Conditions

Both seasonal variation and critical conditions are accounted for in this TMDL through the application of LDCs. LDCs evaluate water quality conditions across all flow zones including high flow, runoff conditions where sediment transport tends to be greatest. Seasonality is accounted for by addressing all flow conditions in a given reach.

4.2.6 TSS TMDL Summary

The TMDL allocation tables (Table 20 through Table 29) present the total LC (Total Load (TMDL) in tables), the MOS, the WLAs (wasteload in tables) and the remaining watershed LAs (load in tables) for the TSS impaired reaches. Allocations for this TMDL were established using the 65 mg/L TSS standard. TMDL allocations for all reaches include the entire watershed draining to each impaired reach (See Figure 2 and Appendix A). For example, allocations for Cottonwood River reach 504 include the watersheds draining to Pell Creek reach 535 and Plum Creek reach 516, as well as the watersheds draining to all nonimpaired reaches upstream of these impairments.

The following rounding conventions were used in the TMDL tables:

- Values ≥ 1.0 reported in lbs/yr have been rounded to the nearest lb.
- Values < 1.0 reported in lbs/yr have been rounded to one significant digit so that the value is greater than zero and a number is displayed in the table.

While some of the numbers in the tables show multiple digits, they are not intended to imply great precision; this is done primarily to make the arithmetic accurate.

The bottom line of the table shows the estimated load reduction for all flow zones and is calculated based on the difference between the 90th percentile monitored TSS concentration (all available data April through September 2008 through 2017) and the 65 mg/L TSS standard. Since the TSS monitoring data is biased to higher flows (i.e., 50% to 72% of TSS samples collected during very high and high flow conditions), a flow zone correction was applied when calculating the percentile TSS concentration. This was done by multiplying each flow zone's 90th percentile monitored TSS concentration by the flow zone's frequency of occurrence. The following equation was used for this calculation:

$$90^{\text{th}} \text{ Percent. TSS Conc.} = (0.1 * \text{TSS}_{\text{very high}}) + (0.3 * \text{TSS}_{\text{high}}) + (0.2 * \text{TSS}_{\text{mid}}) + (0.3 * \text{TSS}_{\text{low}}) + (0.1 * \text{TSS}_{\text{very low}})$$

At this time, there is not enough information or data available to estimate or calculate the existing (current conditions) load contribution from each of the WLA and LA sources presented in each table. Thus, the estimated load reduction for each flow zone applies to all sources. See Section 8 of this TMDL and the WRAPS report for further information on which sources and geographical locations within the impaired reach watersheds should be targeted for sediment reduction BMPs and restoration strategies. TSS LDCs (Figure 8 through Figure 17) for reaches in the Cottonwood River Watershed generally show TSS load exceedances during high and very high flows. TSS loading during high and very high flows is likely most related to near-channel (bank erosion) and agricultural sources (overland erosion from cropland, hay/pasture, and rangeland). Restoration and protection efforts should focus on these sources.

Figure 8. Cottonwood River Reach 502 TSS load duration curve and monitored loads and exceedances.

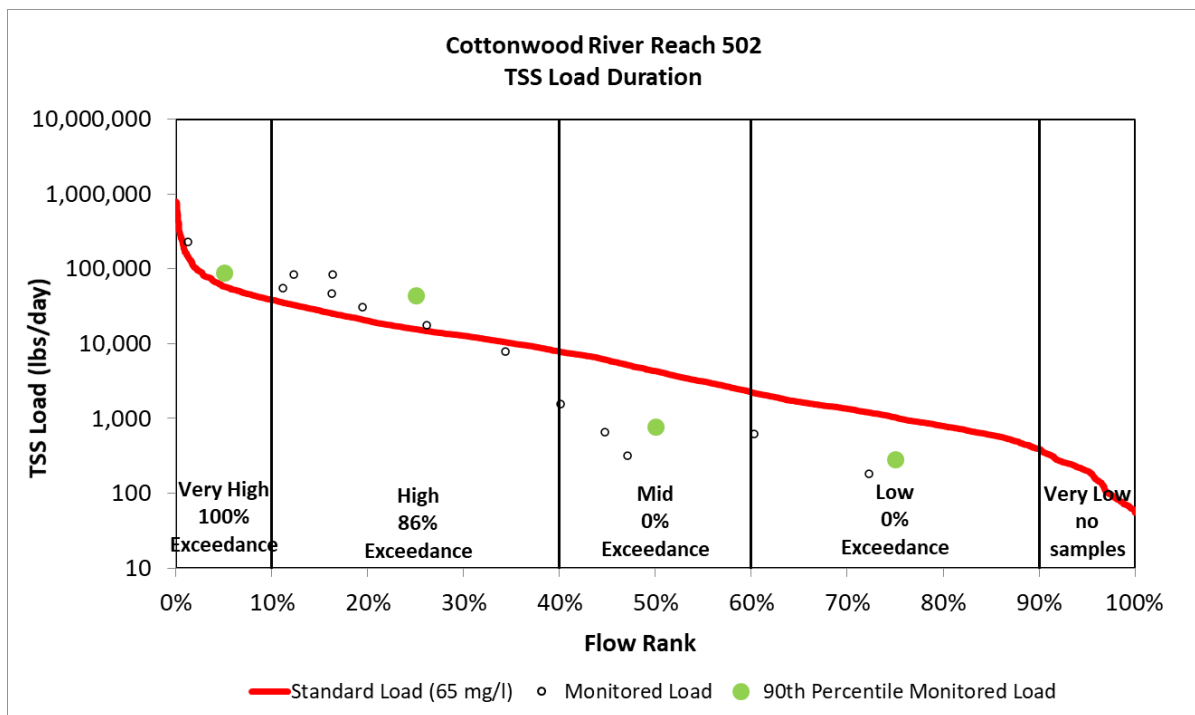


Table 20. TSS TMDL summary for Cottonwood River Reach 502.

Total Suspended Solids		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		TSS load (lbs/day)				
Wasteload	Garvin WWTP (MNG580101)	63	63	63	63	**
	Balaton WWTP (MN0020559)	306	306	306	306	**
	Construction/Industrial SW	86	23	6	2	**
	Total WLA	455	392	375	371	**
Load	Total LA	54,513	14,430	3,708	608	**
	MOS	2,893	780	215	52	10
	Total load	57,861	15,602	4,298	1,031	199
Existing 90th percentile concentration (mg/L)***		75				
Overall estimated percent reduction***		13%				

* Model simulated flow for HSPF reach 90 (2008-2017) was used to develop the flow zones and LCs for this reach.

** The permitted wastewater design flows exceed the stream flow in the indicated flow zone(s). The allocations are expressed as an equation rather than an absolute number: allocation = (flow contribution from a given source) x (65 mg/L or NPDES permit concentration) x (conversion factors). The LA is the remainder after the WLA is applied.

*** Water quality monitoring station(s) used to estimate reductions: S009-440.

Figure 9. Cottonwood River Reach 504 TSS load duration curve and monitored loads and exceedances.

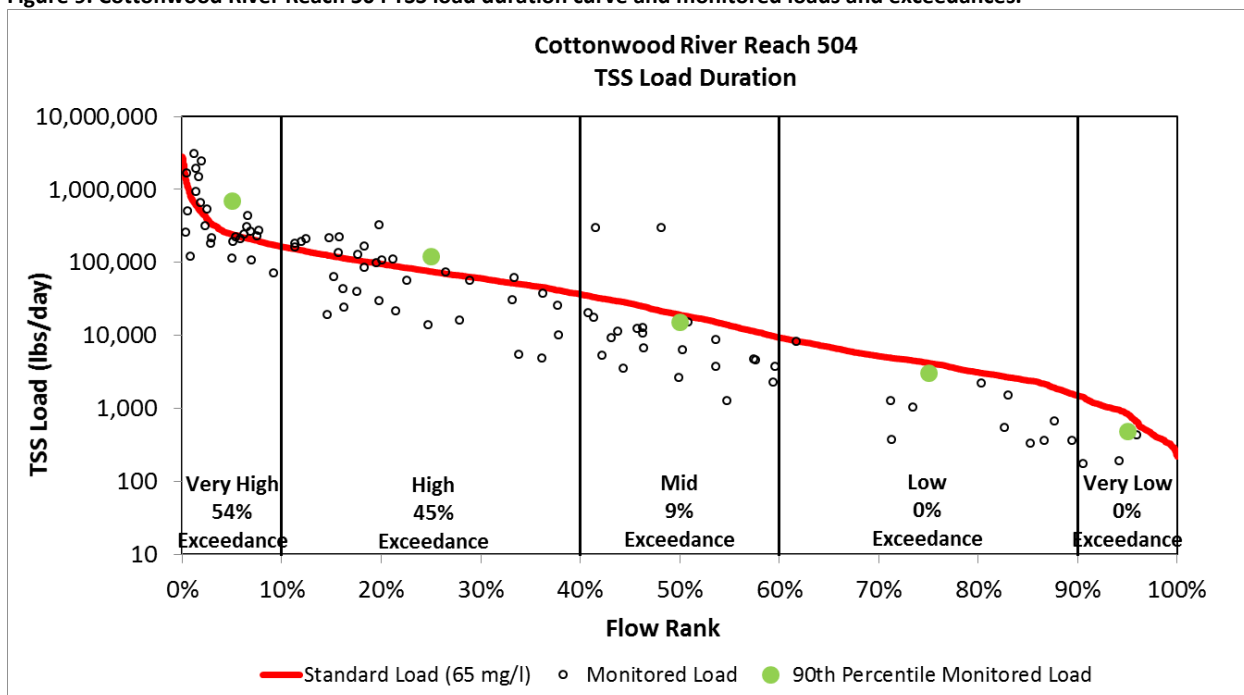


Table 21. TSS TMDL summary for Cottonwood River Reach 504.

Total Suspended Solids		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		TSS load (lbs/day)				
Wasteload	Garvin WWTP (MNG580101)	63	63	63	63	**
	Revere WWTP (MNG580114)	56	56	56	56	**
	Tracy WWTP (MN0021725)	1,312	1,312	1,312	1,312	**
	Balaton WWTP (MN0020559)	306	306	306	306	**
	Walnut Grove WWTP (MN0021776)	51	51	51	51	**
	City of Marshall MS4 (MS400241)***	591	184	47	10	**
	Construction/Industrial SW	360	112	29	6	**
	Total WLA	2,739	2,084	1,864	1,804	**
Load	Total LA	227,061	69,361	16,411	2,179	**
	MOS	12,095	3,760	962	210	42
	Total load	241,895	75,205	19,237	4,193	836
	Existing 90th percentile concentration (mg/L)****	78				
	Overall estimated percent reduction****	17%				

* Model simulated flow for HSPF reach 250 (2008-2017) was used to develop the flow zones and LCs for this reach.

** The permitted wastewater design flows exceed the stream flow in the indicated flow zone(s). The allocations are expressed as an equation rather than an absolute number: allocation = (flow contribution from a given source) x (65 mg/L or NPDES permit concentration) x (conversion factors). The LA is the remainder after the WLA is applied.

*** Although a small portion of the city of Marshall falls within the drainage area for this reach, reductions are not required (see Section 4.2.2).

**** Water quality monitoring station(s) used to estimate reductions: S002-247.

Figure 10. Cottonwood River Reach 508 TSS load duration curve and monitored loads and exceedances.

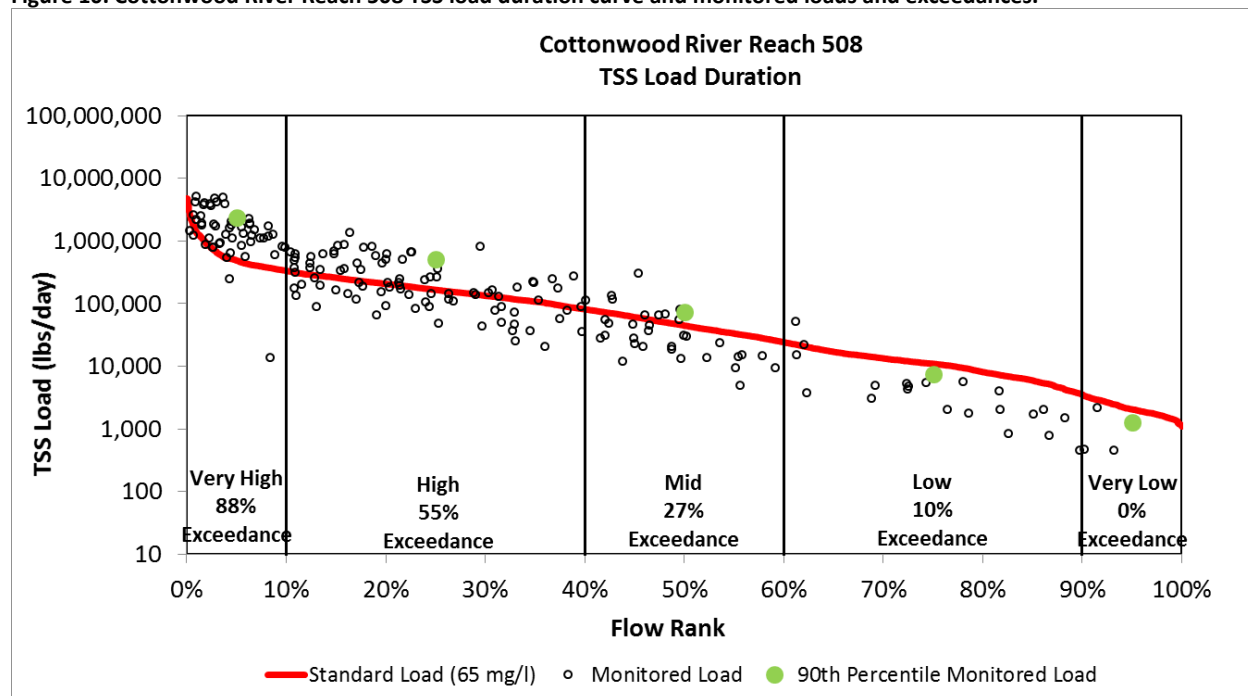


Table 22. TSS TMDL summary for Cottonwood River Reach 508.

Total Suspended Solids		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		TSS load lbs/day				
Wasteload	Sanborn WWTP (MNG580115)	128	128	128	128	**
	Springfield WWTP (MN0024953)	195	195	195	195	**
	Balaton WWTP (MN0020559)	306	306	306	306	**
	Garvin WWTP (MNG580101)	63	63	63	63	**
	Revere WWTP (MNG580114)	56	56	56	56	**
	Tracy WWTP (MN0021725)	1,312	1,312	1,312	1,312	**
	Walnut Grove WWTP (MN0021776)	51	51	51	51	**
	Storden WWTP (MNG580106)	99	99	99	99	**
	Westbrook WWTP (MNG580127)	611	611	611	611	**
	Lamberton WWTP (MNG580100)	489	489	489	489	**
	City of Marshall MS4 (MS400241)***	591	184	47	10	**
	Construction/Industrial SW	726	247	66	16	**
	Total WLA	4,627	3,741	3,423	3,336	**
Load	Total LA	458,470	153,751	38,880	7,114	**
	MOS	24,374	8,289	2,226	550	103
	Total load	487,471	165,781	44,529	11,000	2,059
	Existing 90th percentile concentration (mg/L)***	130				
	Overall estimated percent reduction***	50%				

* Model simulated flow for HSPF reach 370 (2008-2017) was used to develop the flow zones and LCs for this reach.

** The permitted wastewater design flows exceed the stream flow in the indicated flow zone(s). The allocations are expressed as an equation rather than an absolute number: allocation = (flow contribution from a given source) x (65 mg/L or NPDES permit concentration) x (conversion factors). The LA is the remainder after the WLA is applied.

*** Although a small portion of the city of Marshall falls within the drainage area for this reach, reductions are not required (see Section 4.2.2).

**** Water quality monitoring station(s) used to estimate reductions: S001-920.

Figure 11. Cottonwood River Reach 509 TSS load duration curve and HSPF simulated TSS loads and exceedances.

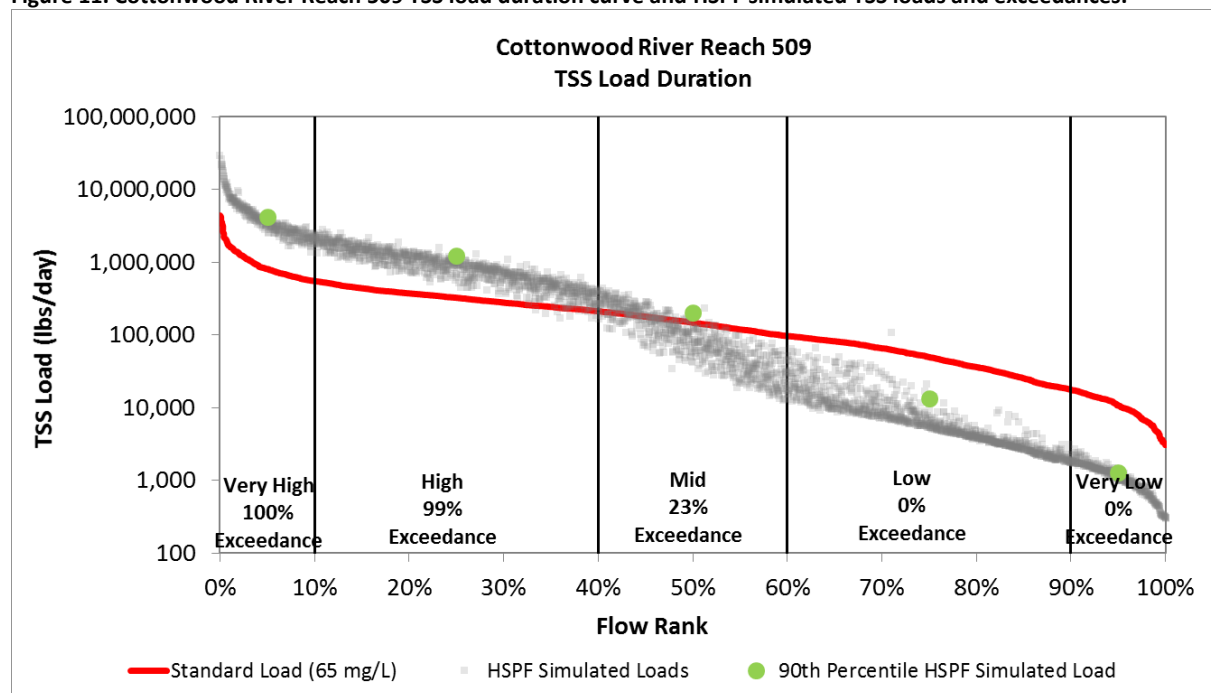


Table 23. TSS TMDL summary for Cottonwood River Reach 509.

Total Suspended Solids		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		TSS load (lbs/day)				
Wasteload	Sanborn WWTP (MNG580115)	128	128	128	128	**
	Springfield WWTP (MN0024953)	195	195	195	195	**
	Balaton WWTP (MN0020559)	306	306	306	306	**
	Garvin WWTP (MNG580101)	63	63	63	63	**
	Revere WWTP (MNG580114)	56	56	56	56	**
	Tracy WWTP (MN0021725)	1,312	1,312	1,312	1,312	**
	Walnut Grove WWTP (MN0021776)	51	51	51	51	**
	Storden WWTP (MNG580106)	99	99	99	99	**
	Westbrook WWTP (MNG580127)	611	611	611	611	**
	Lamberton WWTP (MNG580100)	489	489	489	489	**
	Lucan WWTP (MNG580112)	257	257	257	257	**
	Wanda WWTP (MNG580126)	67	67	67	67	**
	Clements WWTP (MNG580094)	61	61	61	61	**
	Wabasso WWTP (MN0025151)	28	28	28	28	**
	City of Marshall MS4 (MS400241)***	591	184	47	10	**
Construction/Industrial SW	968	339	91	23	**	
	Total WLA	5,282	4,246	3,861	3,756	**
Load	Total LA	611,988	211,942	54,449	10,661	**
	MOS	32,488	11,378	3,069	759	180
	Total load	649,758	227,566	61,379	15,176	3,598
	Existing 90th percentile concentration (mg/L)**	104				
	Overall estimated percent reduction**	38%				

* Model simulated flow for HSPF reach 430 (2008-2017) was used to develop the flow zones and LCs for this reach.

** The permitted wastewater design flows exceed the stream flow in the indicated flow zone(s). The allocations are expressed as an equation rather than an absolute number: allocation = (flow contribution from a given source) x (65 mg/L or NPDES permit concentration) x (conversion factors). The LA is the remainder after the WLA is applied.

*** Although a small portion of the city of Marshall falls within the drainage area for this reach, reductions are not required (see Section 4.2.2).

**** The impairment listing for this reach is based on Secchi Tube data (see Table 8) as no TSS data has been collected for this reach. Therefore, reductions are based on HSPF simulated TSS loads/concentrations.

Figure 12. Dutch Charley Creek Reach 517 TSS load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

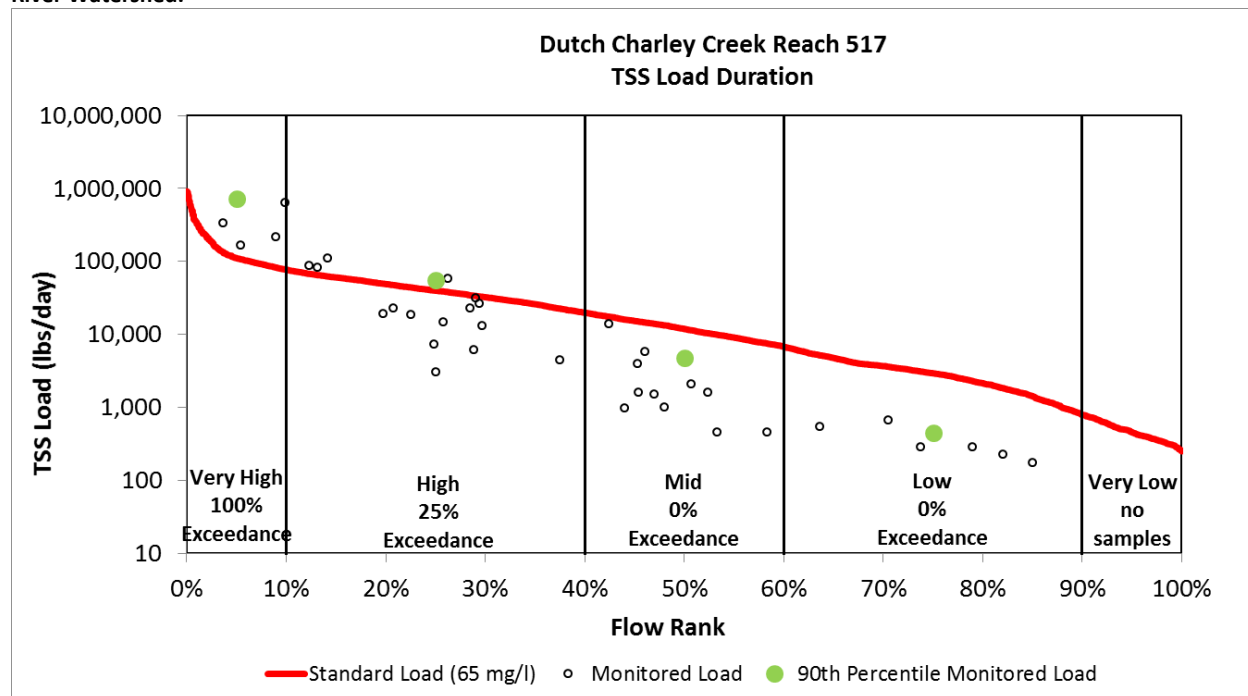


Table 24. TSS TMDL summary for Dutch Charley Creek Reach 517.

Total Suspended Solids		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		TSS load (lbs/day)				
Wasteload	Storden WWTP (MNG580106)	99	99	99	99	**
	Westbrook WWTP (MNG580127)	611	611	611	611	**
	Lamberton WWTP (MNG580100)	489	489	489	489	**
	Construction/Industrial SW	165	59	18	4	**
	Total WLA	1,364	1,258	1,217	1,203	**
Load	Total LA	104,035	36,612	10,094	1,589	**
	MOS	5,547	1,993	595	147	23
	Total load	110,946	39,863	11,906	2,939	456
Existing 90th percentile concentration (mg/L)***		79				
Overall estimated percent reduction***		18%				

* Model simulated flow for HSPF reach 281 (2008-2017) was used to develop the flow zones and LCs for this reach.

** The permitted wastewater design flows exceed the stream flow in the indicated flow zone(s). The allocations are expressed as an equation rather than an absolute number: allocation = (flow contribution from a given source) x (65 mg/L or NPDES permit concentration) x (conversion factors). The LA is the remainder after the WLA is applied.

*** Water quality monitoring station(s) used to estimate reductions: S001-915.

Figure 13. Dutch Charley Creek Reach 518 TSS load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

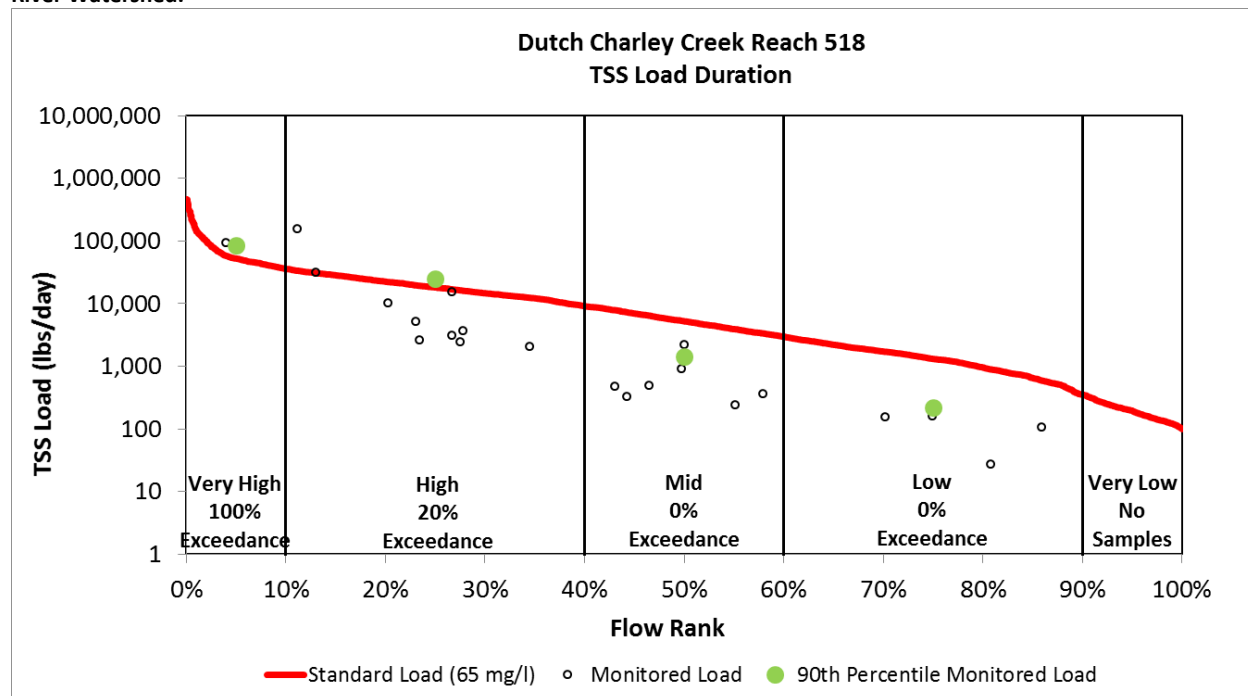


Table 25. TSS TMDL summary for Dutch Charley Creek Reach 518.

Total Suspended Solids		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		TSS load (lbs/day)				
Wasteload	Lamberton WWTP (MNG580100)	489	489	489	489	**
	Construction/Industrial SW	78	27	8	2	**
	Total WLA	567	516	497	491	**
Load	Total LA	49,303	16,749	4,468	756	**
	MOS	2,625	909	261	66	10
	Total load	52,495	18,174	5,226	1,313	194
Existing 90th percentile concentration (mg/L)***		****				
Overall estimated percent reduction***		5%				

* Model simulated flow for HSPF reach 267 (2008-2017) was used to develop the flow zones and LCs for this reach.

** The permitted wastewater design flows exceed the stream flow in the indicated flow zone(s). The allocations are expressed as an equation rather than an absolute number: allocation = (flow contribution from a given source) x (65 mg/L or NPDES permit concentration) x (conversion factors).

*** Water quality monitoring station(s) used to evaluate reductions: S004-879.

**** The 90th percentile flow-zone corrected monitored TSS concentration is at or below 65 mg/L and therefore a 5% load reduction is recommended to ensure the TSS standard is met. There were 22 TSS measurements collected in this reach from 2008-2017 and therefore more monitoring would help determine if reductions beyond 5% are needed.

Figure 14. Highwater Creek Reach 519 TSS load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

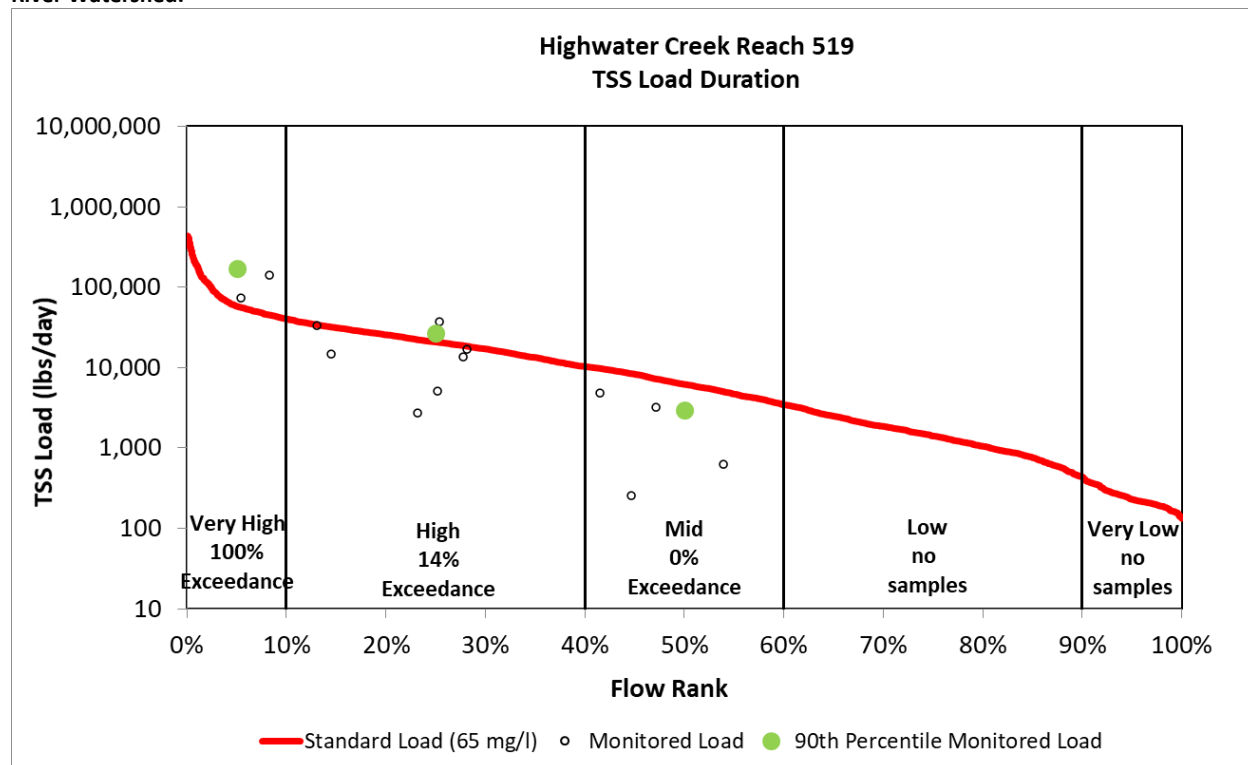


Table 26. TSS TMDL summary for Highwater Creek Reach 519.

Total Suspended Solids		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		TSS load (lbs/day)				
Wasteload	Storden WWTP (MNG580106)	99	99	99	99	**
	Westbrook WWTP (MNG580127)	611	611	611	611	**
	Construction/Industrial SW	86	31	9	2	**
	Total WLA	796	741	719	712	**
Load	Total LA	53,847	18,990	5,136	622	**
	MOS	2,876	1,038	308	70	11
	Total load	57,519	20,769	6,163	1,404	229
	Existing 90th percentile concentration (mg/L)***	****				
Overall estimated percent reduction***		5%				

* Model simulated flow for HSPF reach 279 (2008-2017) was used to develop the flow zones and LCs for this reach.

** The permitted wastewater design flows exceed the stream flow in the indicated flow zone(s). The allocations are expressed as an equation rather than an absolute number: allocation = (flow contribution from a given source) x (65 mg/L or NPDES permit concentration) x (conversion factors). The LA is the remainder after the WLA is applied.

*** Water quality monitoring station(s) used to evaluate reductions: S009-443.

**** The 90th percentile flow-zone corrected monitored TSS concentration is at or below 65 mg/L and therefore a 5% load reduction is recommended to ensure the TSS standard is met. There were 22 TSS measurements collected in this reach from 2008-2017 and therefore more monitoring would help determine if reductions beyond 5% are needed.

Figure 15. Pell Creek Reach 535 TSS load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

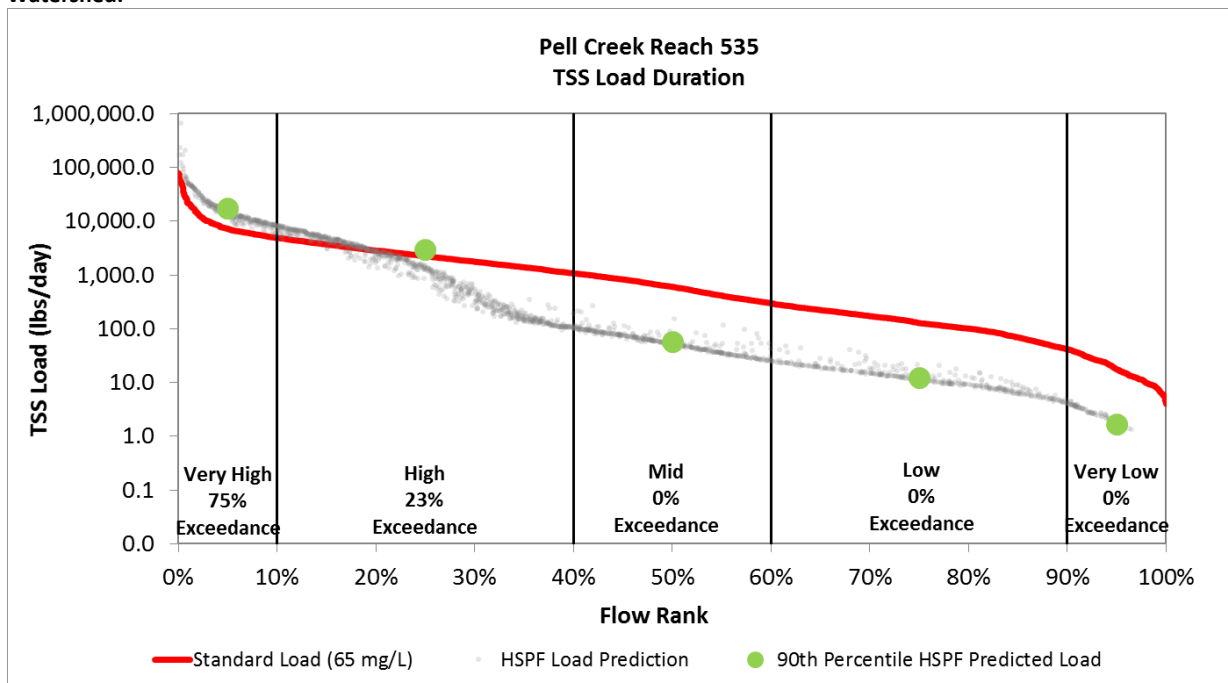


Table 27. TSS TMDL summary for Pell Creek Reach 535.

Total Suspended Solids		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		TSS load (lbs/day)				
Wasteload	Construction/Industrial SW	11	3	0.9	0.2	0.03
	Total WLA	11	3	0.9	0.2	0.03
Load	Total LA	6,789	2,113	569	121	17
	MOS	358	111	30	6	0.9
Total load		7,158	2,227	600	127	18
Existing 90th percentile concentration (mg/L)**		***				
Overall estimated percent reduction**		5%				

* Model simulated flow for HSPF reach 211 (2008-2017) was used to develop the flow zones and LCs for this reach.

** The impairment listing for this reach is based on Secchi Tube data (see Table 8) as no TSS data have been collected for this reach. Therefore, reductions were evaluated using HSPF simulated TSS loads/concentrations.

*** The 90th percentile flow-zone corrected HSPF simulated TSS concentration is at or below 65 mg/L and therefore a 5% load reduction is recommended to ensure the TSS standard is met. No TSS measurements have been collected in this reach. Future monitoring would help determine if reductions beyond 5% are needed.

Figure 16. Sleepy Eye Creek Reach 599 TSS load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

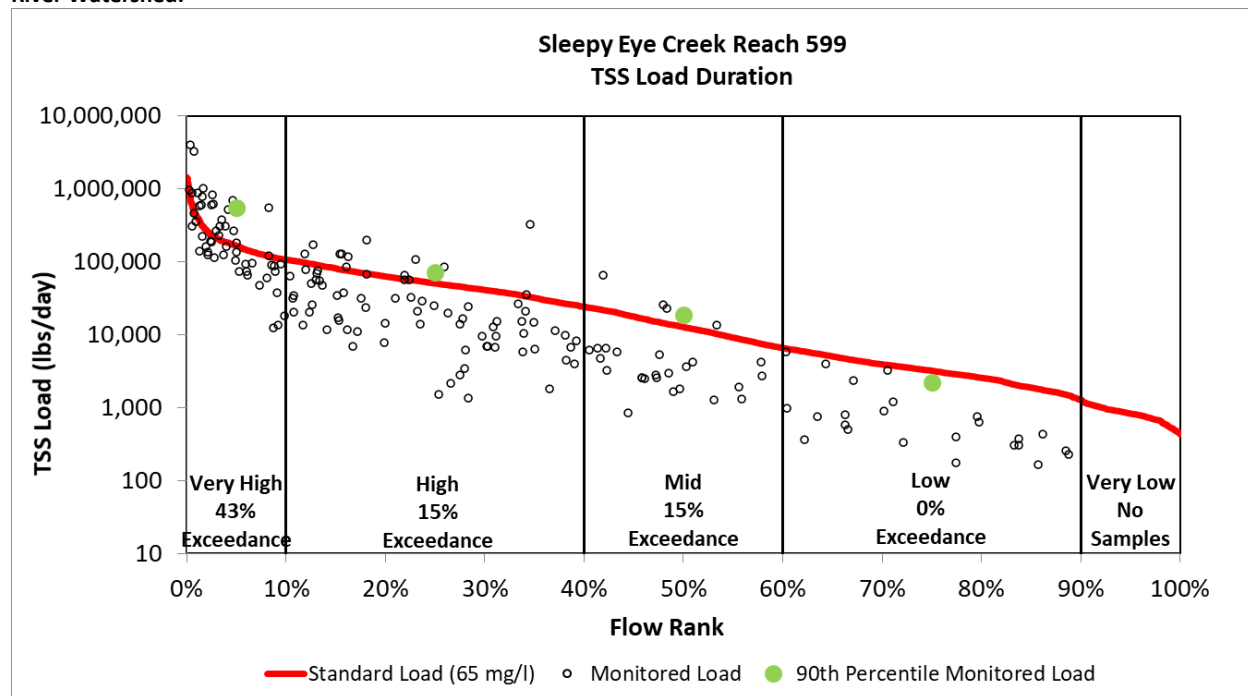


Table 28. TSS TMDL summary for Sleepy Eye Creek Reach 599.

Total Suspended Solids		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		TSS load (lbs/day)				
Wasteload	Clements WWTP (MNG580094)	61	61	61	61	61
	Lucan WWTP (MNG580112)	257	257	257	257	257
	Wabasso WWTP (MN0025151)	28	28	28	28	28
	Wanda WWTP (MNG580126)	67	67	67	67	67
	Construction/Industrial SW	246	75	19	5	1
	Total WLA	659	488	432	418	414
Load	Total LA	156,318	47,368	11,601	2,619	366
	MOS	8,262	2,519	633	160	41
	Total load	165,239	50,375	12,666	3,197	821
Existing 90th percentile concentration (mg/L)**		85				
Overall estimated percent reduction**		24%				

* Model simulated flow for HSPF reach 407 (2008-2017) was used to develop the flow zones and LCs for this reach.

** Water quality monitoring station(s) used to estimate reductions: S001-919.

Figure 17. Plum Creek Reach 602 and 603 TSS load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

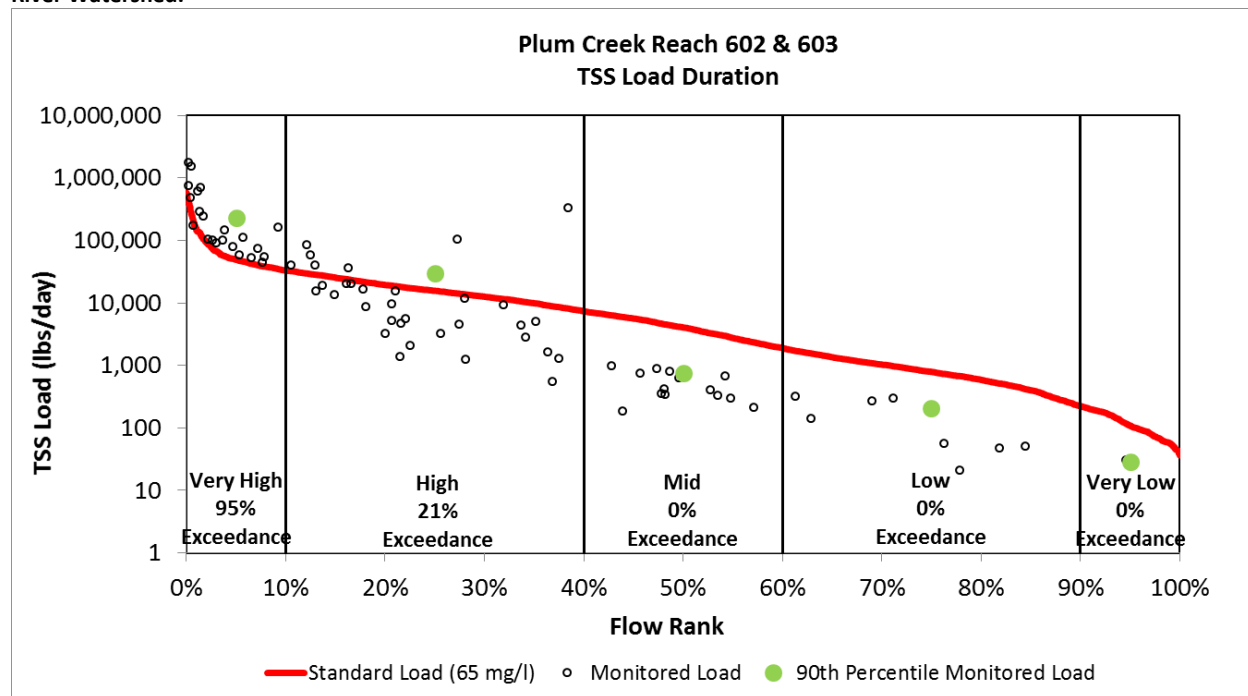


Table 29. TSS TMDL summary for Plum Creek Reach 602 and 603.

Total Suspended Solids		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		TSS load (lbs/day)				
Wasteload	Construction/Industrial SW	73	23	6	1	0.2
	Total WLA	73	23	6	1	0.2
Load	Total LA	46,565	14,829	3,827	747	103
	MOS	2,455	782	202	39	5
Total load		49,093	15,634	4,035	787	108
Existing 90th percentile concentration (mg/L)**		77				
Overall estimated percent reduction**		16%				

* Model simulated flow for HSPF reach 191 (2008-2017) was used to develop the flow zones and LCs for this reach.

** Water quality monitoring station(s) used to estimate reductions: S001-913.

4.3 *E. coli* - Streams

4.3.1 Loading Capacity Methodology

LDCs were used to represent the LC for the *E. coli* impaired reaches (see Figure 2 and Appendix A) covered in this TMDL. The flow component of the LC curve is based on the HSPF-simulated average daily flows from April through October (2008 through 2017), and the concentration component is the *E. coli* concentration standard of 126 cfu/100 mL. *E. coli* LDCs for Cottonwood River Watershed impaired reaches are shown in Section 4.3.6. On these figures the red curve represents the allowable *E. coli* LC of the reach for each daily flow. The median (or midpoint) loads of each flow zone were used to represent the total LC in the TMDL tables. Each reach's LC can be compared to current conditions by plotting the measured load during each individual water quality sampling event (black circles). Each black circle that is above the curve exceeds the 126 cfu/100 mL water quality standard while those below the line are below the water quality standard. It is important to point out that the *E. coli* standard is not applied to

individual sample points, but rather by aggregating the data by month and calculating the geometric mean. That said, plotting the individual sample points helps visualize how the individual data points relate to flow conditions and when elevated bacteria concentrations are more common.

The existing *E. coli* concentration for each impaired reach was calculated as the geometric mean of all monitoring data collected during the months that the standard applies (April through October). The loading capacity was calculated as flow multiplied by the *E. coli* geometric mean standard, 126 org/100 mL. It is assumed that practices that are implemented to meet the geometric mean standard will also address the individual sample standard (1,260 org/100 mL) and that the individual sample standard will also be met. The overall estimated concentration-based percent reduction needed to meet the TMDL was calculated by comparing the highest observed (monitored) monthly geometric mean from the months that the standard applies to the geometric mean standard. Also plotted on the LDC figure are the monitored *E. coli* geometric mean loads for each flow zone (solid green circles). Plotting these individual loads help determine what flow zones and practices should be targeted to achieve the overall reduction goal for each impaired reach.

4.3.2 Wasteload Allocation Methodology

The WLAs for the *E. coli* TMDLs were divided into three categories: NPDES permitted wastewater dischargers, NPDES permitted MS4 stormwater, and NPDES permitted construction and industrial stormwater. This section describes how each of these WLAs were assigned. The NPDES permitted livestock CAFOs are zero discharge facilities and are given a WLA of zero and should not impact water quality in the watershed as a point source. Therefore, it is not necessary to put them in the *E. coli* TMDL table. Straight pipe septic systems are illegal and receive a WLA of zero. Therefore, it is not necessary to put them in the *E. coli* TMDL table.

NPDES Permitted Wastewater Dischargers

There are seven active NPDES permitted surface wastewater dischargers in the Cottonwood River Watershed *E. coli* impaired reach drainage areas (Table 30, Appendix A). WLAs for each facility were calculated by multiplying the facility's wet weather design flow by the *E. coli* standard (126 cfu/100 mL). Discharge monitoring reports (DMRs) were downloaded to assess the typical monthly discharge values and bacteria concentrations at which each facility discharges. It should be noted that NPDES Wastewater Permit limits for bacteria are currently expressed in fecal coliform concentrations, not *E. coli*. However, the fecal coliform permit limit for each wastewater treatment facility (200 organisms/100 mL) is intended to demonstrate that the facility is effectively disinfecting its effluent and therefore does not contribute to *E. coli* standard violations in its receiving waters. No permit modifications are needed at this time for the *E. coli* impairments. The fecal coliform-*E. coli* relationship is documented extensively in the SONAR for the 2007 and 2008 revisions of Minn. R. ch. 7050. Results of DMRs are presented in Appendix B.

The WLA for permitted wastewater dischargers is based on facility design flow. For several of the reaches, however, the WLA exceeds the very low flow zone's daily loading capacity because the facilities in the reach typically discharge less than their design flows. To account for this, the WLA and nonpoint source LA for the very low flow zone are determined by the following formula:

$$\text{Allocation} = (\text{flow contribution from a given source}) \times (\text{E. coli concentration limit or standard})$$

Table 30. *E. coli* allocations for NPDES permitted dischargers in the *E. coli* impaired reach drainage areas.

Impaired Reach	Facility Name and System Type	NPDES ID#	Flow Used for WLA* (MGD)	Chronic Standard (org./100 mL)	Wasteload Allocation (billions of org./day)
502	Balaton WWTP/ Pond	MN0020559	0.816	126	3.89
502	Garvin WWTP/ Pond	MNG580101	0.169	126	0.81
523	Revere WWTP/ Pond	MNG580114	0.150	126	0.71
511	Sleepy Eye WWTP/ Pond	MNG580041	6.420	126	30.62
519	Storden WWTP/ Pond	MNG580106	0.264	126	1.26
523	Walnut Grove WWTP/ Mechanical	MN0021776	0.203	126	0.97
519	Westbrook WWTP/ Pond	MNG580127	1.629	126	7.77

*Average wet weather design flow or maximum daily pond flow in million gallons per day (MGD).

NPDES Permitted MS4 Stormwater

There are no permitted MS4s located in the drainage areas of the *E. coli* impaired reaches covered in this report.

NPDES Permitted Construction and Industrial Stormwater

WLAs for regulated construction stormwater permits (MNR100001) were not developed since *E. coli* is not a typical pollutant from construction sites. Industrial stormwater receives a WLA only if the pollutant is part of benchmark monitoring for an industrial site in the watershed of an impaired water body. There are no bacteria or *E. coli* benchmarks associated with any of the Industrial Stormwater permits (MNR050000) or Nonmetallic Mining & Associated Activities general permits (MNG490000) in the Cottonwood River Watershed *E. coli* impaired reach drainage areas, and therefore no industrial stormwater *E. coli* WLAs were assigned.

4.3.3 Load Allocation Methodology

As stated in the governing TMDL equation, the LA, also referred to as the watershed LA, is comprised of the nonpoint source load that is allocated to an impaired reach after the MOS and WLA are subtracted from the total LC for each flow regime. This residual load is meant to represent the watershed LA that includes all nonregulated sources of *E. coli* upstream of the impaired reach, which are summarized in Section 3.6.

The relationship between bacterial sources and bacterial concentrations found in streams is complex, involving precipitation and flow, temperature, livestock management practices, wildlife activities, survival rates, land use practices, and other environmental factors. Section 3.6 discusses possible

sources of bacteria found in streams and highlighted the observation that *E. coli* populations can be naturalized in the sediment and persist over an extended period of time. Sadowsky et. al. (2015) concluded that approximately 36% of *E. coli* strains were represented by multiple isolates, suggesting persistence of specific *E. coli*. The authors suggested that 36% might be used as a rough indicator of “background” levels of bacteria at this site during the study period. While these results may not be transferable to other locations, they do suggest the presence of background *E. coli* and a fraction of *E. coli* may be present regardless of the control measures taken by traditional implementation strategies.

4.3.4 Margin of Safety

The MOS is a portion of the TMDL that is set aside to account for the uncertainties associated with achieving water quality standards. The MOS can be either implicitly or explicitly defined as a set-aside amount. An explicit MOS was calculated as 5% of the loading capacity for the Cottonwood River Watershed *E. coli* impaired reaches. Five percent was considered an appropriate MOS since the LDC approach minimizes a great deal of uncertainty. The LDC calculations are based on *E. coli* target concentrations and modeled flow data that has been calibrated to long-term monitored flow data. Most of the uncertainty with this calculation is therefore associated with the HSPF modeled flow output for each reach. The Cottonwood River HSPF model was calibrated and validated using 21 years (1996 through 2017) of flow data from five gaging stations (Tetra Tech 2019). Calibration results indicate that the HSPF model is a valid representation of hydrological and chemical conditions in the watershed. See Appendix D of this TMDL for the HSPF model calibration and validation results. The *E. coli* LDCs were developed using HSPF modeled daily flow data from April through October (2008 through 2017). The *E. coli* TMDL applied a MOS to each flow zone along the duration curves by subtracting 5% of the flow zones loading capacity.

4.3.5 Seasonal Variation and Critical Conditions

E. coli monitoring data for the bacteria impaired reaches indicate all reaches had multiple exceedances of the monthly chronic standard (Table 9). Exceedances of the acute standard have also been recorded in each of the impaired reaches covered in this report. Fecal bacteria are most productive at temperatures similar to their origination environment in animal digestive tracts. Thus, these organisms are expected to be at their highest concentrations during warmer summer months when stream flow is low and water temperatures are high. High *E. coli* concentrations in many of the reaches continue into the fall, which may be attributed to constant sources of *E. coli* (such as failing SSTS and animal access to the stream) and less flow for dilution. However, some of the data may be skewed as more samples were collected in the summer months than in early spring and late fall. Seasonal and annual variations are accounted for by setting the TMDL across the entire flow record using the load duration method.

4.3.6 *E. coli* TMDL Summary

The TMDL summary tables (Table 31 through Table 38) for Cottonwood River Watershed *E. coli* impaired reaches present the existing load, the total LC (total load (TMDL) in tables, MOS, WLA (wasteload in tables), and LA (load in tables). Allocations for these TMDLs were established using the 126 cfu/100 mL *E. coli* standard. All LAs are reported in billions of organisms/day and were rounded to one significant figure to prevent zero load values. The last line of each table shows the estimated concentration-based

percent load reductions to meet the TMDL for all flow zones. These reductions were calculated by comparing the highest observed (monitored) monthly geometric mean from the months that the standard applies to the geometric mean standard. At this time, there is not enough information or data available to estimate or calculate the existing (current conditions) load contribution from each of the WLA and LA sources presented in the TMDL tables. Thus, the estimated load reduction for each flow zone applies to the water body as a whole. *E. coli* LDCs (Figure 18 through– Figure 25) for reaches in the Cottonwood River Watershed generally show *E. coli* load exceedances during all flow conditions for which there is data. This suggests a variety of sources contribute to the impairments. For example, during high flow conditions, watershed runoff is likely the primary source of *E. coli* to the river reaches. During low flow conditions, other sources such as noncompliant SSTS and livestock in streams increase in relative importance. See Section 8 of this TMDL and the WRAPS report for further information on which sources and geographical locations within the impaired reach watershed should be targeted for bacteria BMPs and restoration strategies.

Figure 18. Cottonwood River Reach 502 *E. coli* load duration curve and monitored loads and exceedances.

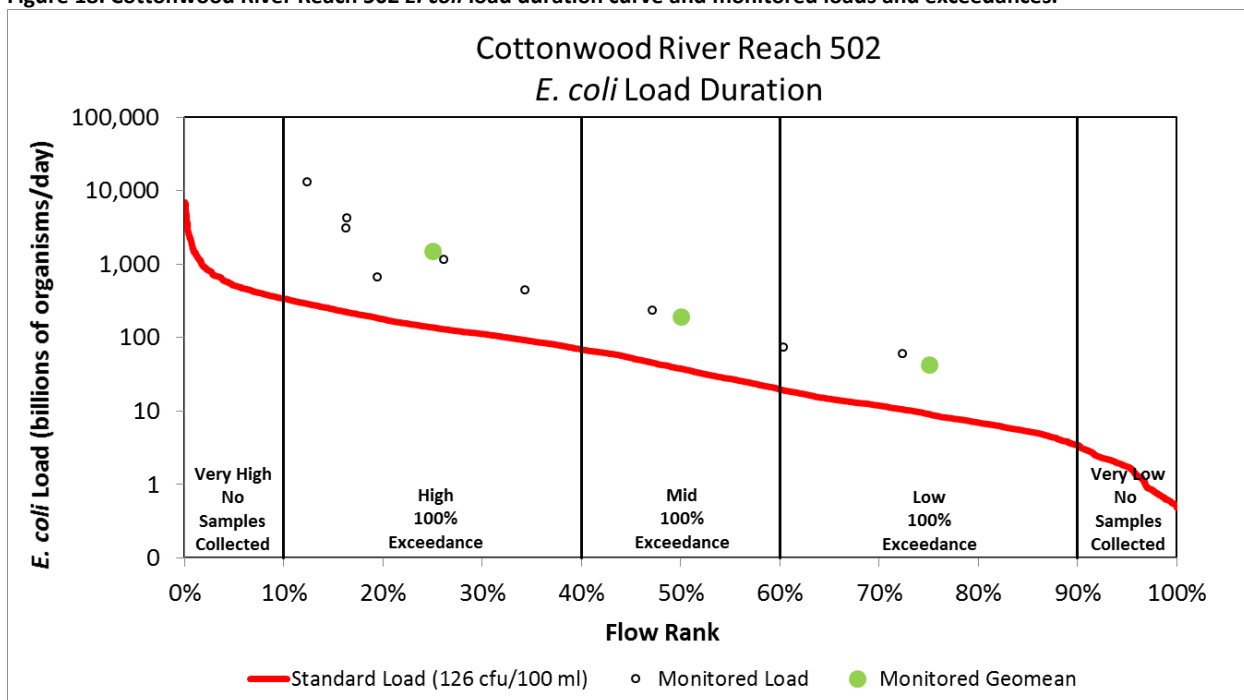


Table 31. *E. coli* TMDL summary for Cottonwood River Reach 502.

<i>E. coli</i>		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		<i>E. coli</i> load (billions of orgs/day)				
Wasteload	Balaton WWTP	4	4	4	4	**
	Garvin WWTP	0.8	0.8	0.8	0.8	**
	Total WLA	5	5	5	5	**
Load	Total LA	743	197	51	9	**
	MOS	39	11	3	0.7	0.1
Total load		787	213	59	15	3
Existing Concentration, Apr-Oct (org/100 mL)***		1,063				
Maximum Monthly Geometric Mean (org/100mL)***		1,859				
Overall Estimated Percent Reduction***		93%				

* Model simulated flow for HSPF reach 90 from April-October (2008-2017) was used to develop the flow zones and LCs for this reach.

** The permitted wastewater design flows exceed the stream flow in the indicated flow zone(s). The allocations are expressed as an equation rather than an absolute number: allocation = (flow contribution from a given source) x (126 org per 100 mL) x conversion factors.

*** Water quality monitoring station(s) used to estimate reductions: S009-440; the maximum monthly geometric mean of 1,859 is from a month with fewer than 5 samples.

Figure 19. Judicial Ditch 30 Reach 511 *E. coli* load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

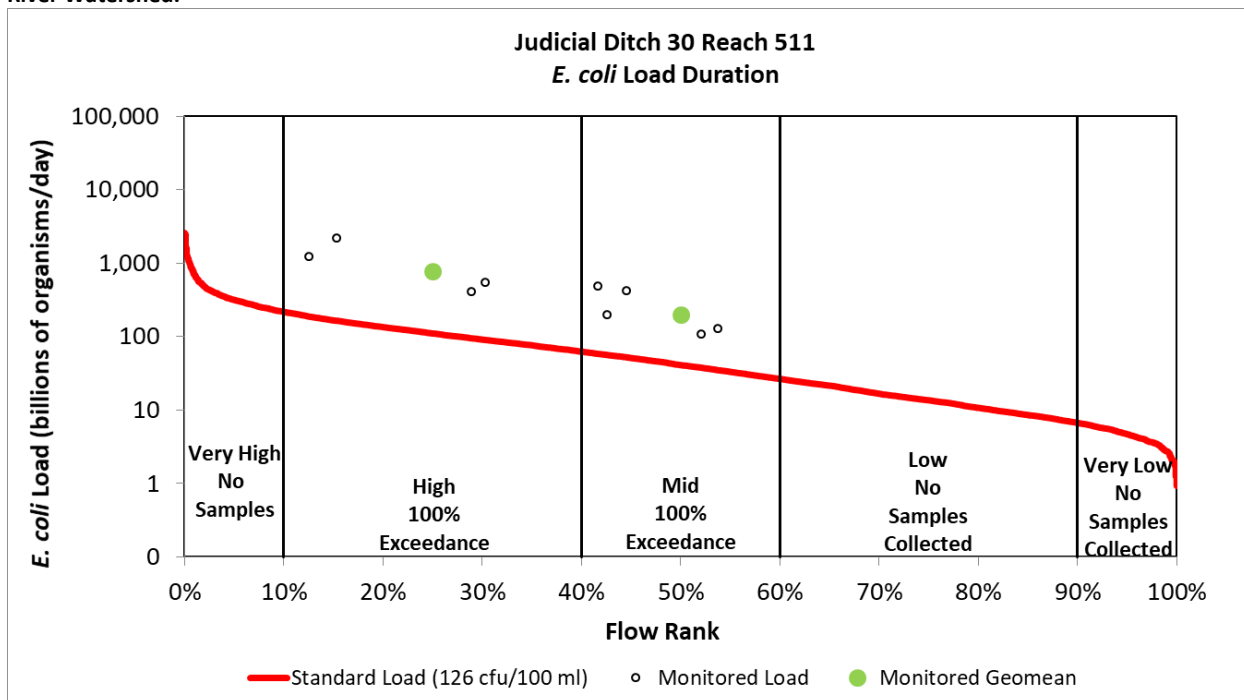


Table 32. *E. coli* TMDL summary for Judicial Ditch 30 Reach 511.

<i>E. coli</i>		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		<i>E. coli</i> load (billions of orgs/day)				
Wasteload	Sleepy Eye WWTP	31	31	31	**	**
	Total WLA	31	31	31	**	**
Load	Total LA	451	149	30	**	**
	MOS	25	10	3	1	0.3
Total load		507	190	64	20	7
Existing Concentration, Apr-Oct (org/100 mL)**		710				
Maximum Monthly Geometric Mean (org/100mL)**		921				
Overall Estimated Percent Reduction***		86%				

* Model simulated flow for HSPF reach 435 from April-October (2008-2017) was used to develop the flow zones and LCs for this reach.

** The permitted wastewater design flows exceed the stream flow in the indicated flow zone(s). The allocations are expressed as an equation rather than an absolute number: allocation = (flow contribution from a given source) x (126 org per 100 mL) x conversion factors.

*** Water quality monitoring station(s) used to estimate reductions: S009-438; the maximum monthly geometric mean of 921 is from a month with fewer than 5 samples.

Figure 20. Highwater Creek Reach 519 *E. coli* load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

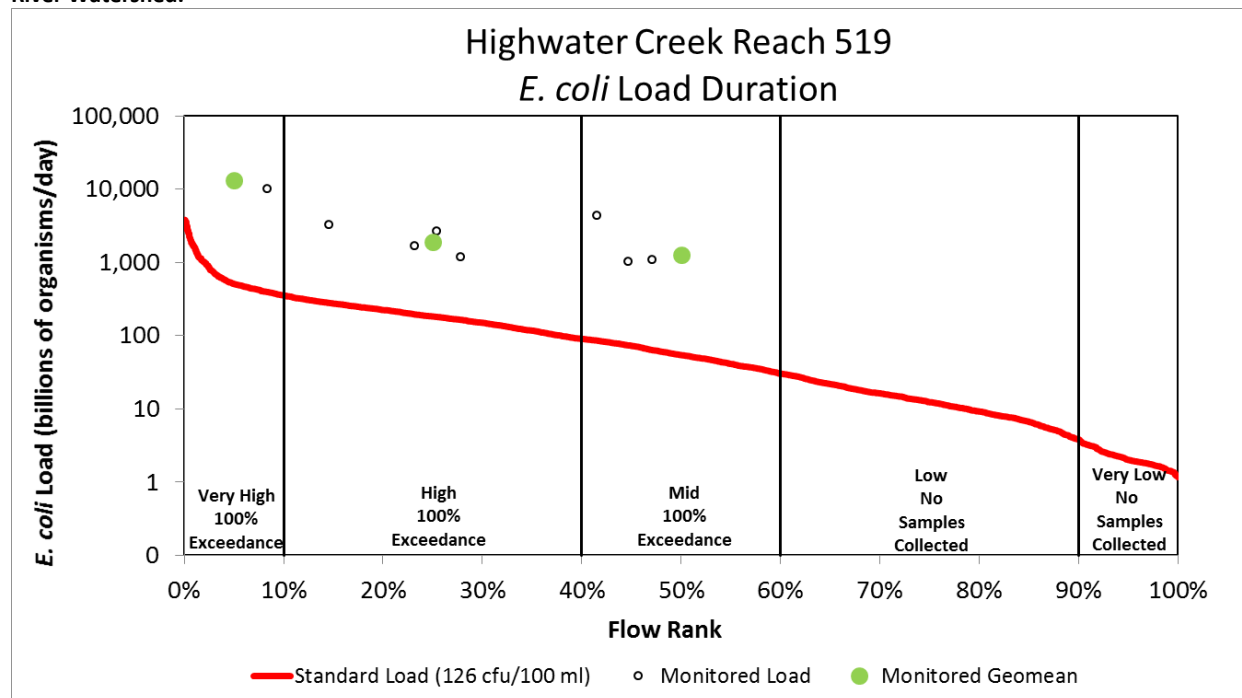


Table 33. *E. coli* TMDL summary for Highwater Creek Reach 519.

<i>E. coli</i>		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		<i>E. coli</i> load (billions of orgs/day)				
Wasteload	Storden WWTP	1	1	1	1	**
	Westbrook WWTP	8	8	8	8	**
	Total WLA	9	9	9	9	**
Load	Total LA	735	259	71	9	**
	MOS	39	14	4	1	0.2
Total load		783	282	84	19	3
Existing Concentration, Apr-Oct (org/100 mL)***		1,897				
Maximum Monthly Geometric Mean (org/100mL)***		2,729				
Overall Estimated Percent Reduction***		95%				

* Model simulated flow for HSPF reach 279 from April-October (2008-2017) was used to develop the flow zones and LCs for this reach.

** The permitted wastewater design flows exceed the stream flow in the indicated flow zone(s). The allocations are expressed as an equation rather than an absolute number: allocation = (flow contribution from a given source) x (126 org per 100 mL) x conversion factors.

*** Water quality monitoring station(s) used to estimate reductions: S009-443; the maximum monthly geometric mean of 2,729 is from a month with fewer than 5 samples.

Figure 21. Dry Creek Reach 520 *E. coli* load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

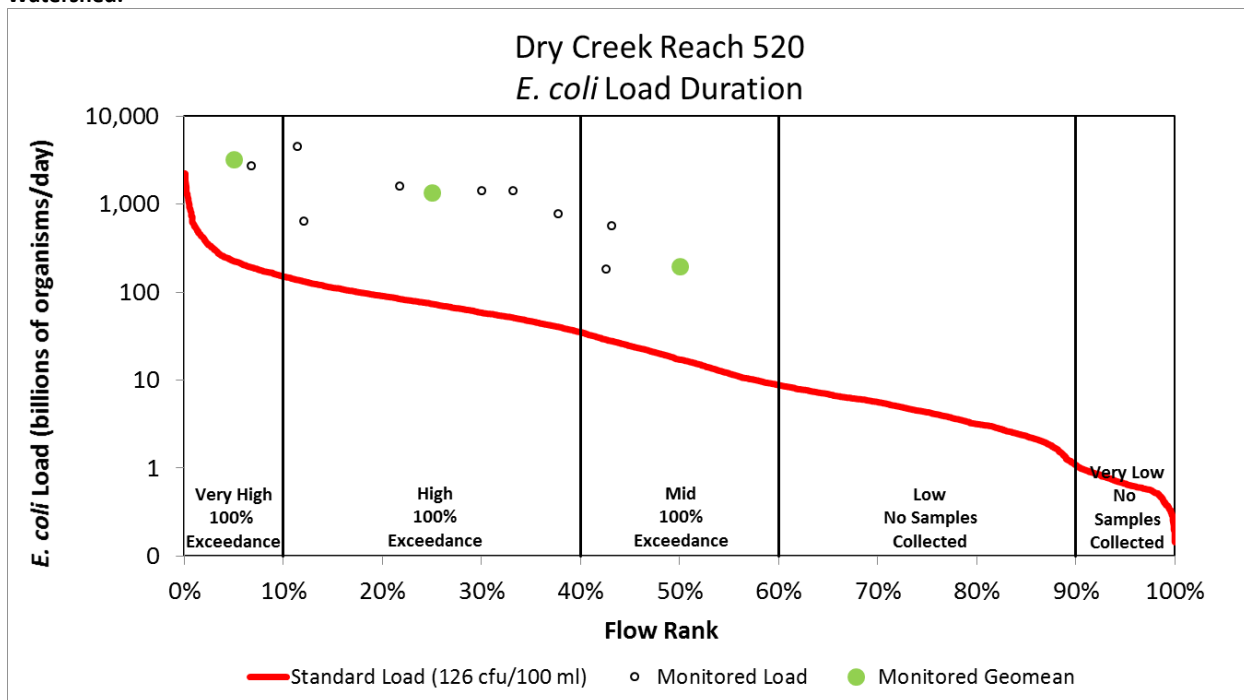


Table 34. *E. coli* TMDL summary for Dry Creek Reach 520.

<i>E. coli</i>		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		<i>E. coli</i> load (billions of orgs/day)				
Load	Total LA	329	108	25	6	1
	MOS	17	6	1	0.3	0.1
	Total load	346	114	26	6	1
	Existing Concentration, Apr-Oct (org/100 mL)**	2,033				
	Maximum Monthly Geometric Mean (org/100mL)**	3,248				
	Overall Estimated Percent Reduction**	96%				

* Model simulated flow for HSPF reach 291 from April-October (2008-2017) was used to develop the flow zones and LCs for this reach.

** Water quality monitoring station(s) used to estimate reductions: S009-442; the maximum monthly geometric mean of 3,248 is from a month with fewer than 5 samples.

Figure 22. Mound Creek Reach 521 *E. coli* load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

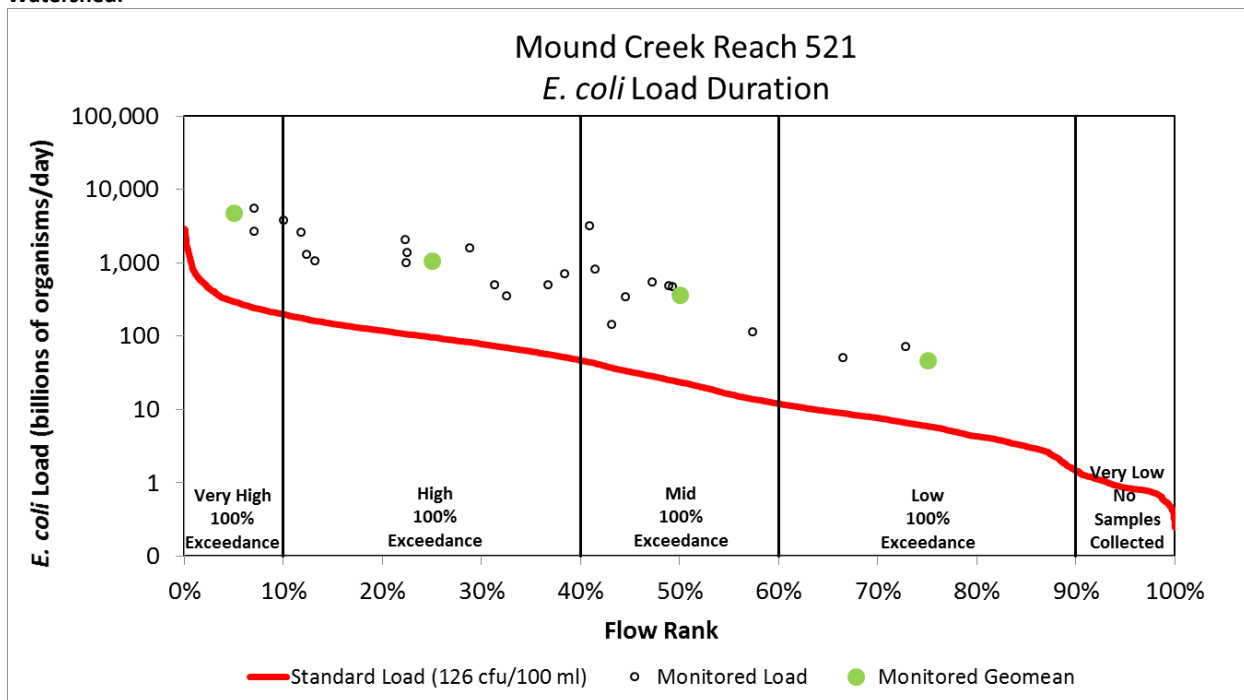


Table 35. *E. coli* TMDL summary for Mound Creek Reach 521.

<i>E. coli</i>		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		<i>E. coli</i> load (billions of orgs/day)				
Load	Total LA	433	142	35	9	1
	MOS	23	7	2	0.5	0.1
	Total load	456	149	37	10	1
	Existing Concentration, Apr-Oct (org/100 mL)**	1,553				
	Maximum Monthly Geometric Mean (org/100mL)**	1,709				
	Overall Estimated Percent Reduction**	93%				

* Model simulated flow for HSPF reach 311 from April-October (2008-2017) was used to develop the flow zones and LCs for this reach.

** Water quality monitoring station(s) used to estimate reductions: S005-690.

Figure 23. Pell Creek Reach 523 *E. coli* load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

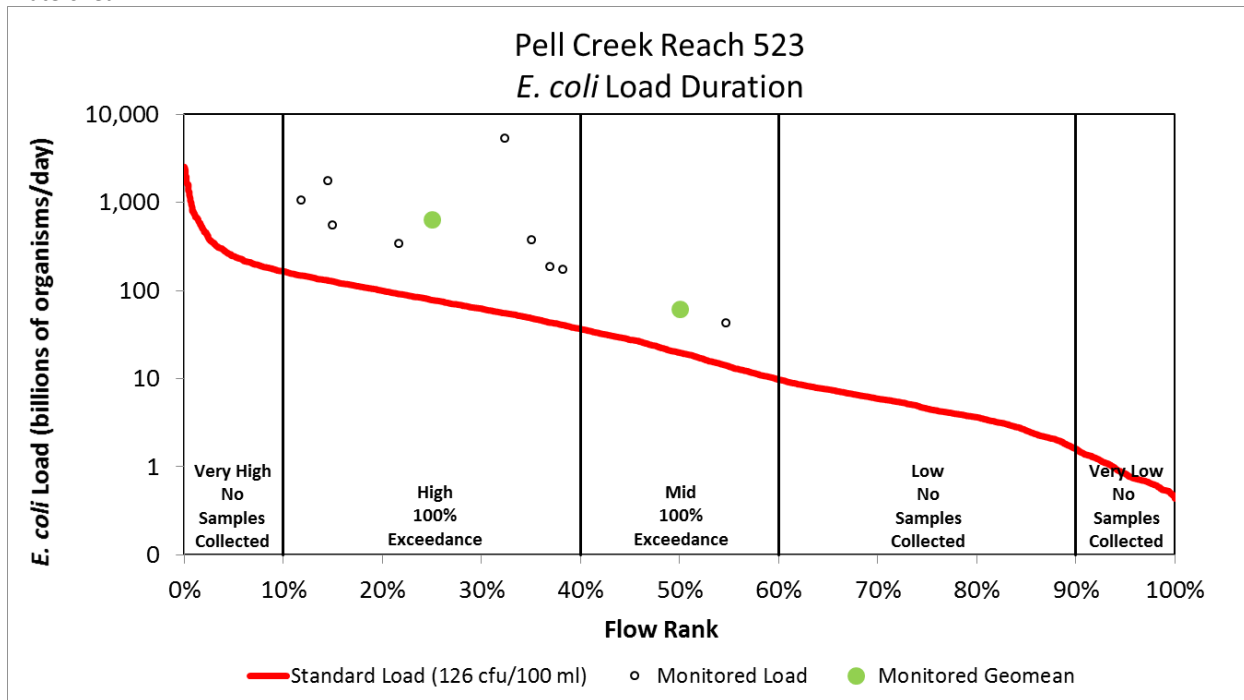


Table 36. *E. coli* TMDL summary for Pell Creek Reach 523.

<i>E. coli</i>		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		<i>E. coli</i> load (billions of orgs/day)				
Wasteload	Walnut Grove WWTP	1	1	1	1	**
	Revere WWTP	0.7	0.7	0.7	0.7	**
	Total WLA	2	2	2	2	**
Load	Total LA	358	113	27	5	**
	MOS	19	6	2	0.4	0.1
Total load		379	121	31	7	1
Existing Concentration, Apr-Oct (org/100 mL)**		937				
Maximum Monthly Geometric Mean (org/100mL)**		2,005				
Overall Estimated Percent Reduction**		94%				

* Model simulated flow for HSPF reach 215 from April-October (2008-2017) was used to develop the flow zones and LCs for this reach.

** The permitted wastewater design flows exceed the stream flow in the indicated flow zone(s). The allocations are expressed as an equation rather than an absolute number: allocation = (flow contribution from a given source) x (126 org per 100 mL) x conversion factors.

*** Water quality monitoring station(s) used to estimate reductions: S009-444; the maximum monthly geometric mean of 2,005 is from a month with fewer than 5 samples.

Figure 24. Coal Mine Creek Reach 604 *E. coli* load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

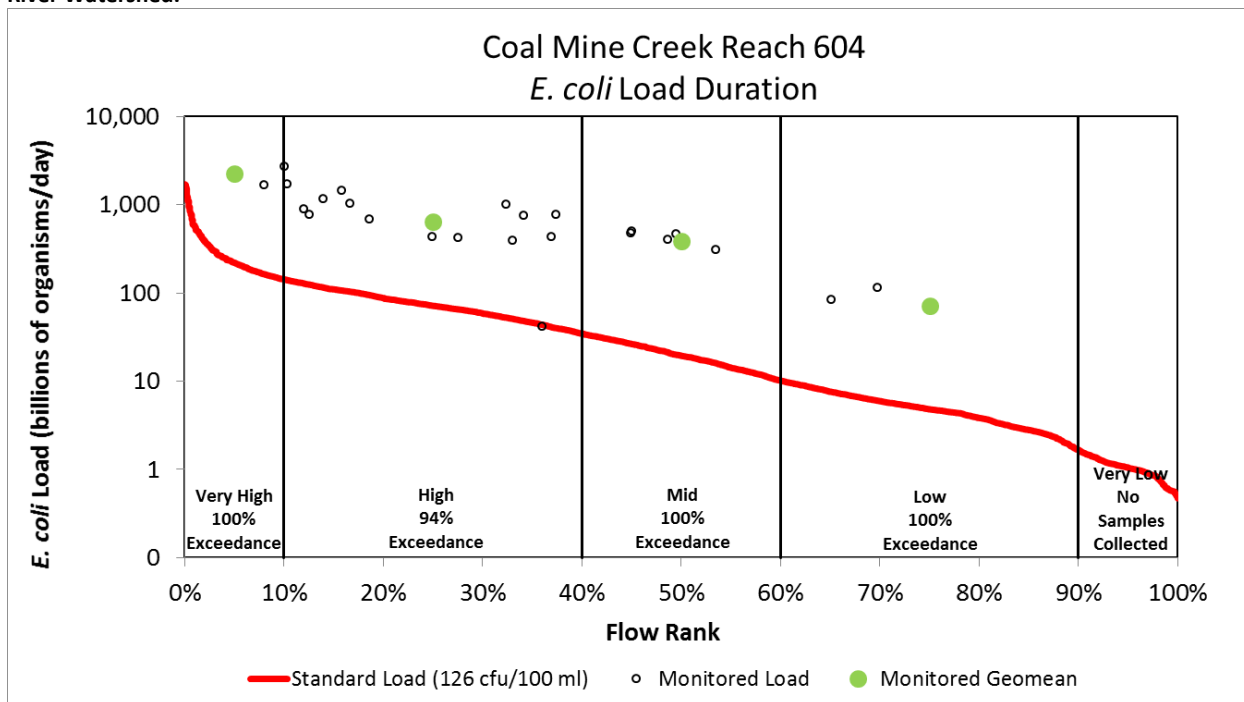


Table 37. *E. coli* TMDL summary for Coal Mine Creek Reach 604.

<i>E. coli</i>		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		<i>E. coli</i> load (billions of orgs/day)				
Load	Total LA	321	105	29	7	2
	MOS	17	6	2	0.4	0.1
	Total load	338	111	31	7	2
	Existing Concentration, Apr-Oct (org/100 mL)**	1,401				
	Maximum Monthly Geometric Mean (org/100mL)**	1,740				
	Overall Estimated Percent Reduction**	93%				

* Model simulated flow for HSPF reach 335 from April-October (2008-2017) was used to develop the flow zones and LCs for this reach.

** Water quality monitoring station(s) used to estimate reductions: S005-691 and S009-439.

Figure 25. Judicial Ditch 30 Reach 609 *E. coli* load duration curve and monitored loads and exceedances in the Cottonwood River Watershed.

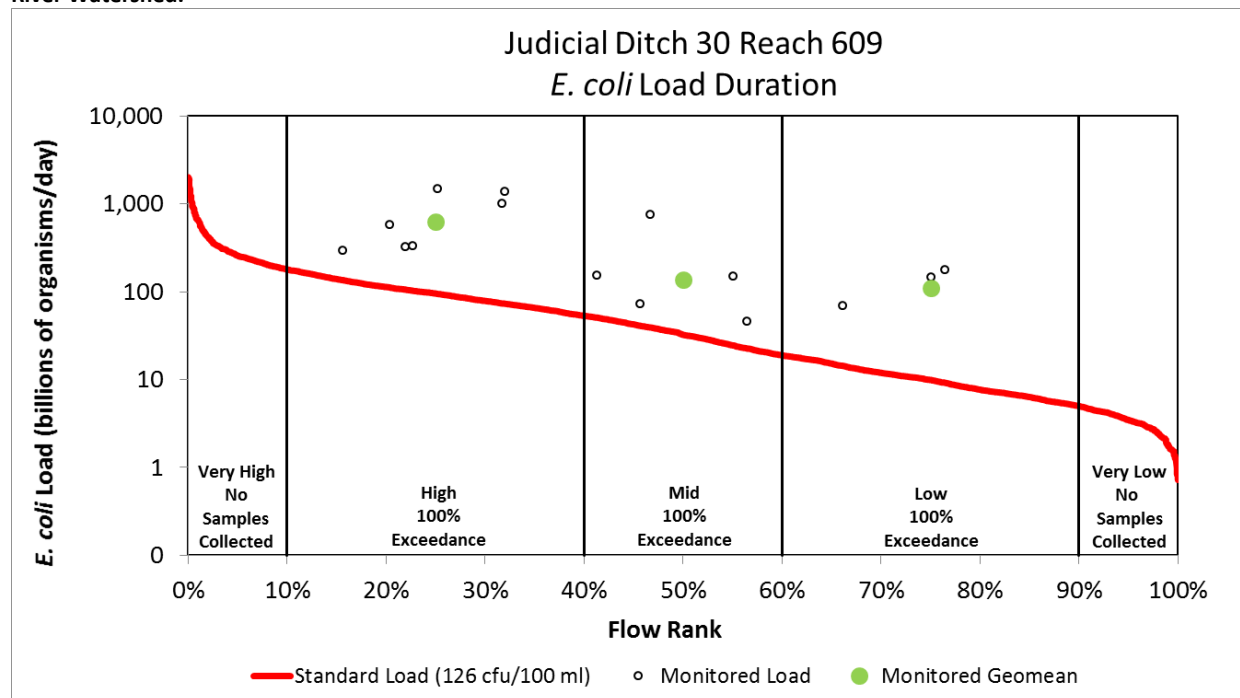


Table 38. *E. coli* TMDL summary for Judicial Ditch 30 Reach 609.

<i>E. coli</i>		Flow zones*				
		Very high	High	Mid-range	Low	Very low
Sources		<i>E. coli</i> load (billions of orgs/day)				
Load	Total LA	378	140	48	15	5
	MOS	20	7	3	0.8	0.3
	Total load	398	147	51	16	5
	Existing Concentration, Apr-Oct (org/100 mL)**	787				
	Maximum Monthly Geometric Mean (org/100mL)**	2,064				
	Overall Estimated Percent Reduction**	94%				

* Model simulated flow for HSPF reach 435 from April-October (2008-2017) was used to develop the flow zones and LCs for this reach.

** Water quality monitoring station(s) used to estimate reductions: S005-688.

4.4 Phosphorus - Lakes

4.4.1 Loading Capacity Methodology

TP LCs for each impaired lake in the Cottonwood River Watershed (see Figure 2 and Appendix A) were developed using the Canfield-Bachmann Lake Response Model. Phosphorus loading from the atmosphere, SSTs, watershed, upstream impaired lakes and internal load were the primary sources evaluated and incorporated into the Canfield-Bachmann Lake Response Models. Section 3.6.3 of this TMDL provides a detailed discussion of the phosphorus source assessment and lake response model methodology. Once each of the lake response models were calibrated, the resulting relationship between phosphorus load and in-lake water quality were used to determine the assimilative capacity.

To set the LC for each impaired lake, the nutrient inputs partitioned between sources in the lake response models were systematically reduced until the model predicted that each lake met their ecoregion TP standard. This process is discussed in more detail in Section 4.4.6.

4.4.2 Wasteload Allocation Methodology

The WLAs were divided into three primary categories: NPDES permitted wastewater dischargers, NPDES permitted MS4 stormwater, and NPDES-permitted construction and industrial stormwater. The NPDES permitted livestock CAFOs are zero discharge facilities and are given a WLA of zero and should not impact water quality in each lake's drainage area as a point source. Therefore, it is not necessary to put them in the lake phosphorus TMDL tables. Also, straight pipe septic systems are illegal and receive a WLA of zero. Therefore, it is not necessary to put them in the lake phosphorus TMDL tables.

NPDES Permitted Wastewater Dischargers

There are currently no permitted wastewater dischargers located in the impaired lake watersheds covered in this TMDL.

NPDES Permitted MS4 Stormwater

There are no permitted MS4s located in the watersheds draining to the impaired lakes covered in this TMDL.

NPDES Permitted Construction and Industrial Stormwater

Construction and industrial stormwater WLAs were established based on estimated percentage of land in the Cottonwood River Watershed currently under construction or permitted for industrial use. A 2018 permit review across the watershed (see Section 4.2.2) showed minimal construction and industrial activities (~0.15% of the watershed).

4.4.3 Load Allocation Methodology

The LA, also referred to as the watershed LA, includes all nonpermitted and nonpoint sources, including: natural background, atmospheric deposition, SSTs, discharge from upstream lakes, watershed loading from nonregulated areas, and internal loading.

The LA is the portion of the total loading capacity assigned to nonpoint and natural background sources of nutrient loading. These sources include atmospheric loading and nearly all of the loading from watershed runoff. The only portion of the watershed runoff not included in the LA is the small loading set aside for regulated stormwater runoff from construction and industrial sites. The LA includes nonpoint sources that are not subject to NPDES Permit requirements, as well as natural background sources. These include phosphorus sources such as soil erosion or nutrient leaching from cropland, runoff from feedlots not operating under a NPDES or SDS permit, phosphorus-laden runoff from urban areas not covered by MS4 Permits, and streambed and streambank erosion resulting from human-induced hydrologic changes and disturbance of stream channels and riparian areas. In addition, some phosphorus may leach into the lake or its upstream tributaries from failing SSTs.

Natural background sources of phosphorus include atmospheric deposition, as well as the relatively low levels of soil erosion from both stream channels and upland areas that would occur under natural conditions. Aside from atmospheric deposition, this TMDL does not attempt to quantify the natural

background load as a separate component of the LA for the impaired lakes. Natural background load is likely a very small part of the LA for lakes in the Cottonwood River Watershed. Studies indicate runoff load of nutrients and other pollutants from urban, agricultural and other developed or disturbed lands is generally at least an order of magnitude greater than runoff loads from natural landscapes (Barr Engineering 2004). Any estimate of natural background as a separate component of the LA would be very difficult to derive and would have a large potential for error without expensive, special studies such as paleolimnological analysis of sediment cores. Given the highly altered landscape in which the Cottonwood River Watershed impaired lakes are located, it is unlikely natural background is a major component of phosphorus loading.

4.4.4 Margin of Safety

An explicit MOS was used for each of the impaired lake TMDLs in this TMDL. The purpose of the MOS is to account for uncertainty that the allocations will result in attainment of water quality standards. Section 303(d) of the CWA and EPA's regulations in 40 CFR § 130.7 require that: TMDLs shall be established at levels necessary to attain and maintain the applicable narrative and numeric water quality standards with seasonal variations and a MOS, which takes into account any lack of knowledge concerning the relationship between effluent limitations and water quality. The MOS can either be implicitly incorporated into conservative assumptions used to develop the TMDL or be added as a separate explicit component of the TMDL (EPA 1991). Ten percent of the load was set aside in the TMDL for each impaired lake to account for uncertainty in the phosphorus source assessment and the lake response models. The use of an explicit MOS accounts for environmental variability in pollutant loading, variability in water quality monitoring data, calibration and validation processes of modeling efforts, uncertainty in modeling outputs, conservative assumptions made during the modeling efforts, and limitations associated with the drainage area-ratio method used to extrapolate flow data. This MOS is considered to be sufficient given the robust datasets used and high quality of modeling, as described below.

The Cottonwood River Basin HSPF model was calibrated and validated using 21 years (1996 through 2017) of flow data from five gaging stations. Calibration results indicate that the HSPF model is a valid representation of hydrological and chemical conditions in the watershed. The BATHTUB models used to develop the lake TMDLs show generally good agreement between the observed lake water quality and the water quality predicted by the lake response models. See Appendix D of this TMDL for the HSPF model calibration and validation results.

4.4.5 Seasonal Variation and Critical Conditions

Seasonal variation is accounted for through the use of annual loads and developing targets for the summer period, where the frequency and severity of nuisance algal growth will be the greatest. Although the critical period is the summer, lakes are not sensitive to short term changes in water quality, rather lakes respond to long-term changes such as changes in the annual load. Therefore, seasonal variation is accounted for in the annual loads. By setting the TMDL to meet targets established for the most critical period (summer), the TMDL will inherently be protective of water quality during the other seasons.

4.4.6 Phosphorus Reduction Methodology

This section provides an explanation of the steps used in the lake response models to calculate lake nutrient reductions to meet the TMDLs. The following items were taken into account: atmospheric sources, upstream lakes, SSTS loading, watershed conditions, and internal load. A uniform methodology was established to assign load reductions to the various sources to meet TMDL goals. The steps for nutrient reductions are discussed below:

- No reductions to atmospheric load were assigned since these loads were generally a small portion of the total load to the lake and the sources are extremely difficult to define and control.
- Phosphorus loading from ITPHS SSTSs and SSTSs that fail to protect groundwater (FTPGW) were reduced to levels expected from properly functioning SSTSs. See Section 3.6.4 for more discussion on the methods used to estimate SSTS contributions and Reasonable Assurance SSTS Section 6.1.5.
- All upstream impaired lakes are expected to meet water quality standards, and the resultant reductions are applied to the lake being evaluated. If these reductions result in the lake meeting water quality standards, then the TMDL allocations are done. If more reductions are required, then the internal and external loads are evaluated simultaneously.
- Watershed loading will ideally be reduced until the lake response model indicates the lake is meeting lake water quality standards. Watershed loading was incrementally reduced until watershed TP concentrations met the river/stream eutrophication standard for the Southern River Nutrient Region (150 µg/L). If the lake model did not meet water quality standards after watershed phosphorus concentrations were set to the river/stream eutrophication standard, the remaining phosphorus reduction was taken from internal loading.
- For many of the lakes in the Cottonwood River Watershed, internal load is a significant source of phosphorus and in-lake efforts may be needed to achieve water quality standards. The general approach to internal load reductions is based on review of the potential internal loading sources (see discussion in Sections 3.6.4 and 8.3.5), the monitored/modeled sediment RRs and lake morphometry. This is accomplished by comparing the existing monitored/modeled RRs to literature values of “healthy lakes” (~1 mg/m²/day) (Nürnberg 1997; Wenck 2011). If the estimated RR is high, then the rate is reduced systematically until either a minimum of 1 mg/m²/day is reached or the lake meets TMDL requirements.

4.4.7 Phosphorus TMDL Summary

The allowable TP load (TMDL) for each lake was divided among the WLA, LA, and the MOS as described in the preceding sections. The following tables summarize the existing and allowable TP loads (Total Load in tables), the TMDL allocations (Wasteload and Load in tables), and required reductions for each lake. In these tables the total load reduction is the sum of the required WLA reductions plus the required LA reductions; this is not the same as the net difference between the existing and allowable total loads, however, because the WLA and LA reductions must accommodate the MOS.

The following rounding conventions were used in the TMDL tables:

- Values ≥1.0 reported in lbs/yr have been rounded to the nearest lb.

- Values <1.0 reported in lbs/yr have been rounded to one significant digit so that the value is greater than zero and a number is displayed in the table.
- While some of the numbers in the tables show multiple digits, they are not intended to imply great precision; this is done primarily to make the arithmetic accurate.

Table 39 through Table 46 present the allocations for the impaired lakes in the Cottonwood River Watershed and Figure 26 through Figure 32 show the estimated phosphorus sources for each of the lakes. Internal phosphorus load and watershed phosphorus load are the dominant sources for the lakes in this TMDL report. A focus on reducing internal phosphorus loads will be required to return these lakes to a nonimpaired state, however, long-term improvement to the lakes' trophic status will also require reductions from external load sources. See the [Minnesota State and Regional Government Review of Internal Phosphorus Load Control](#) (MPCA 2020d) for more information on internal phosphorus load control planning and practices.

Table 39. Rock Lake (42-0052-00) phosphorus TMDL in the Cottonwood River Watershed.

Phosphorus		Existing TP load*		Allowable TP load		Estimated load reduction	
Sources		lbs/year	lbs/day	lbs/year	lbs/day	lbs/year**	%
Wasteload	Construction/Industrial SW	3	0.01	3	0.01	0	0%
	Total WLA	3	0.01	3	0.01	0	0%
Load	Watershed runoff	1,699	4.65	841	2.30	858	50%
	SSTS	15	0.04	9	0.03	6	39%
	Atmospheric deposition	91	0.25	91	0.25	0	0%
	Internal load	3,722	10.19	496	1.36	3,226	87%
	Total LA	5,527	15.13	1,437	3.94	4,090	74%
MOS				160	0.44		
Total load		5,530	15.14	1,600	4.39	4,090	71%

* Model calibration year(s): 2002, 2007 & 2017. ** Net reduction from current load to TMDL is 3,930 lbs/yr; but the gross load reduction from all sources must accommodate the MOS as well, and hence is 3,930 + 160 = 4,090 lbs/yr.

Figure 26. Rock Lake phosphorus source reductions to meet TMDL in the Cottonwood River Watershed.

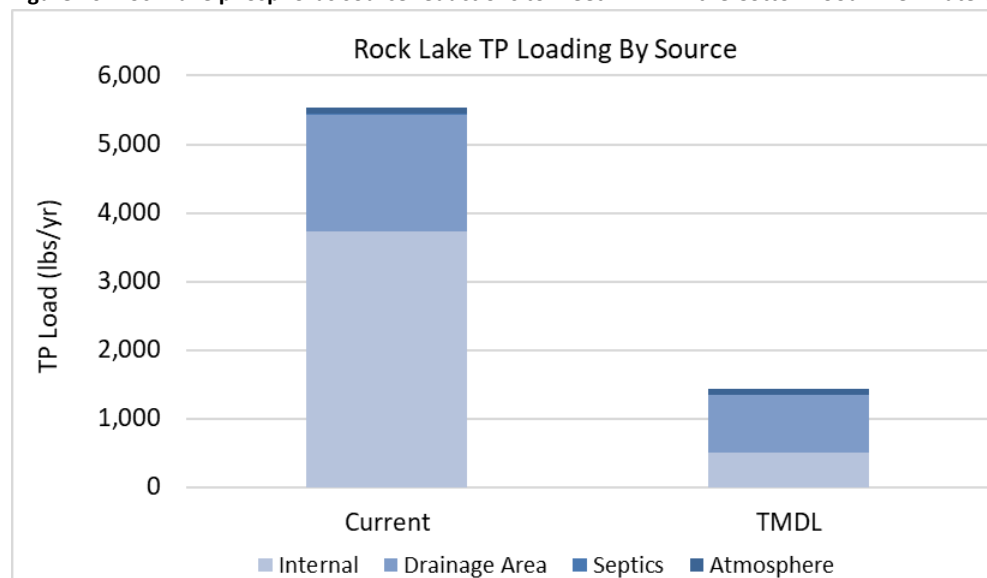


Table 40. Bean Lake (08-0011-00) phosphorus TMDL in the Cottonwood River Watershed.

Phosphorus		Existing TP load*		Allowable TP load		Estimated load reduction	
Sources		lbs/year	lbs/day	lbs/year	lbs/day	lbs/year**	%
Wasteload	Construction/Industrial SW	0.5	0.001	0.5	0.001	0.0	0%
	Total WLA	0.5	0.001	0.5	0.001	0.0	0%
Load	Watershed runoff	326.0	0.893	211.6	0.579	114.4	35%
	SSTS	2.5	0.007	1.2	0.003	1.3	54%
	Atmospheric deposition	39.2	0.107	39.2	0.107	0.0	0%
	Internal load	1,191.8	3.263	591.2	1.619	600.6	50%
	Total LA	1,559.5	4.270	843.2	2.308	716.3	46%
MOS				93.7	0.257		
Total load		1,560.0	4.271	937.4	2.566	716.3	40%

* Model calibration year(s): 2007, 2008 & 2017.

** Net reduction from current load to TMDL is 622.6 lbs/yr; but the gross load reduction from all sources must accommodate the MOS as well, and hence is 622.6 + 93.7 = 716.3 lbs/yr.

Figure 27. Bean Lake phosphorus source reductions to meet TMDL in the Cottonwood River Watershed.

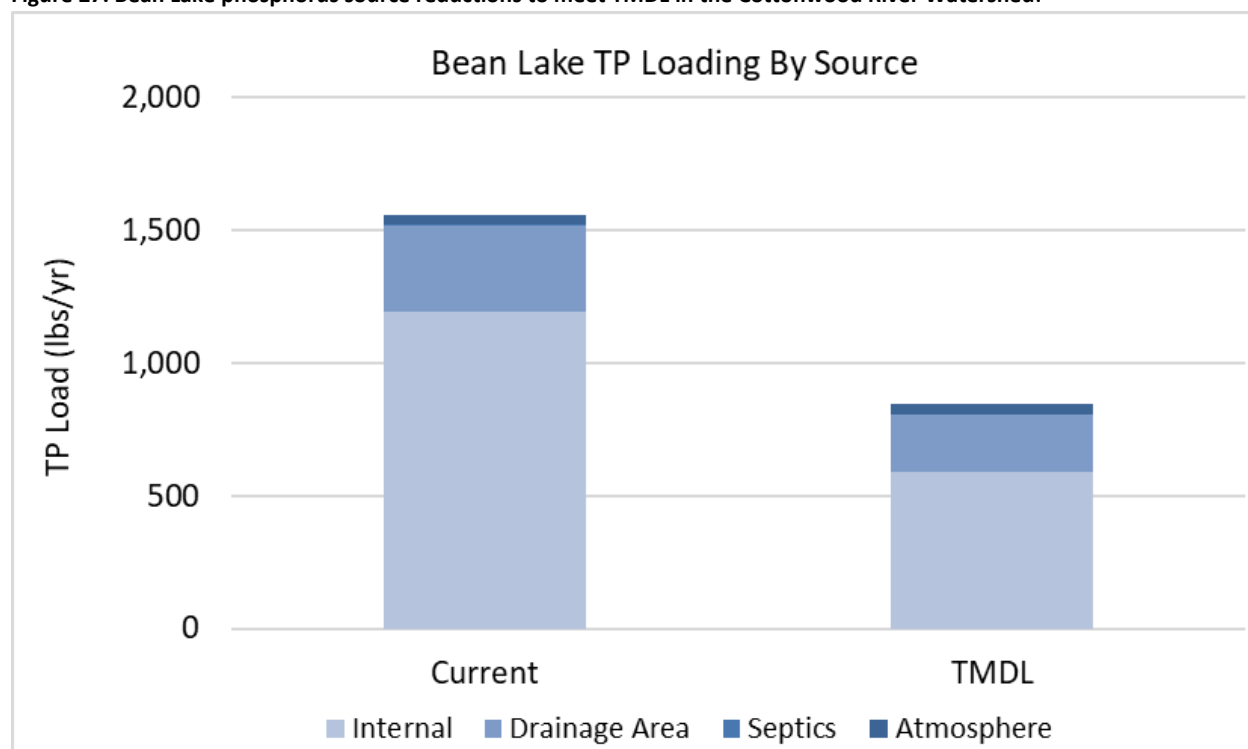


Table 41. Double (North Portion) Lake (17-0056-01) phosphorus TMDL in the Cottonwood River Watershed.

Phosphorus		Existing TP load*		Allowable TP load		Estimated load reduction	
Sources		lbs/year	lbs/day	lbs/year	lbs/day	lbs/year**	%
Wasteload	Construction/Industrial SW	0.5	0.001	0.5	0.001	0.0	0%
	Total WLA	0.5	0.001	0.5	0.001	0.0	0%
Load	Watershed runoff	365.2	1.000	103.8	0.284	261.4	72%
	SSTS	10.9	0.030	5.2	0.014	5.7	52%
	Upstream lake (Bean)	145.8	0.399	97.8	0.268	48.0	33%
	Atmospheric deposition	32.5	0.089	32.5	0.089	0.0	0%
	Internal load	468.2	1.282	329.0	0.901	139.2	30%
	Total LA	1,022.6	2.800	568.3	1.556	454.3	44%
MOS				63.2	0.173		
Total load		1,023.1	2.801	632.0	1.730	454.3	38%

* Model calibration year(s): 2007, 2008, 2017 and 2018.

** Net reduction from current load to TMDL is 391.1 lbs/yr; but the gross load reduction from all sources must accommodate the MOS as well, and hence is 391.1 + 63.2 = 454.3 lbs/yr.

Figure 28. Double (North Portion) Lake phosphorus source reductions to meet TMDL in the Cottonwood River Watershed.

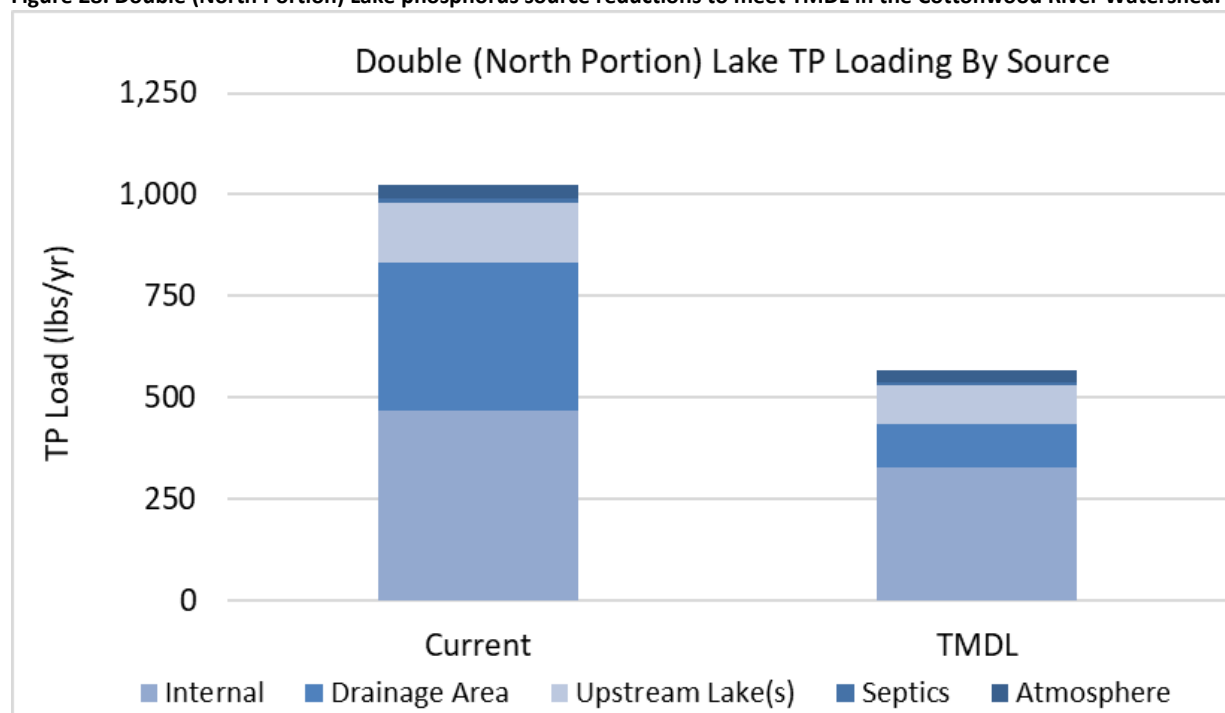


Table 42. Clear Lake (08-0011-00) phosphorus TMDL in the Cottonwood River Watershed.

Phosphorus		Existing TP load*		Allowable TP load		Estimated load reduction	
Sources		lbs/year	lbs/day	lbs/year	lbs/day	lbs/year**	%
Wasteload	Construction/Industrial SW	1.6	0.004	1.6	0.004	0.0	0%
	Total WLA	1.6	0.004	1.6	0.004	0.0	0%
Load	Watershed Runoff	1,055.8	2.891	605.3	1.657	450.5	43%
	SSTS	16.3	0.045	7.6	0.021	8.7	53%
	Atmospheric deposition	66.2	0.181	66.2	0.181	0.0	0%
	Internal load	1,289.0	3.529	344.6	0.943	944.4	73%
	Total LA	2,427.3	6.646	1,023.7	2.802	1,403.6	58%
MOS				113.9	0.312		
Total load		2,428.9	6.650	1,139.2	3.118	1,403.6	53%

* Model calibration year(s): 2009, 2010 and 2017.

** Net reduction from current load to TMDL is 1,289.7 lbs/yr; but the gross load reduction from all sources must accommodate the MOS as well, and hence is 1,289.7 + 113.9 = 1,403.6 lbs/yr.

Figure 29. Clear Lake phosphorus source reductions to meet TMDL in the Cottonwood River Watershed.

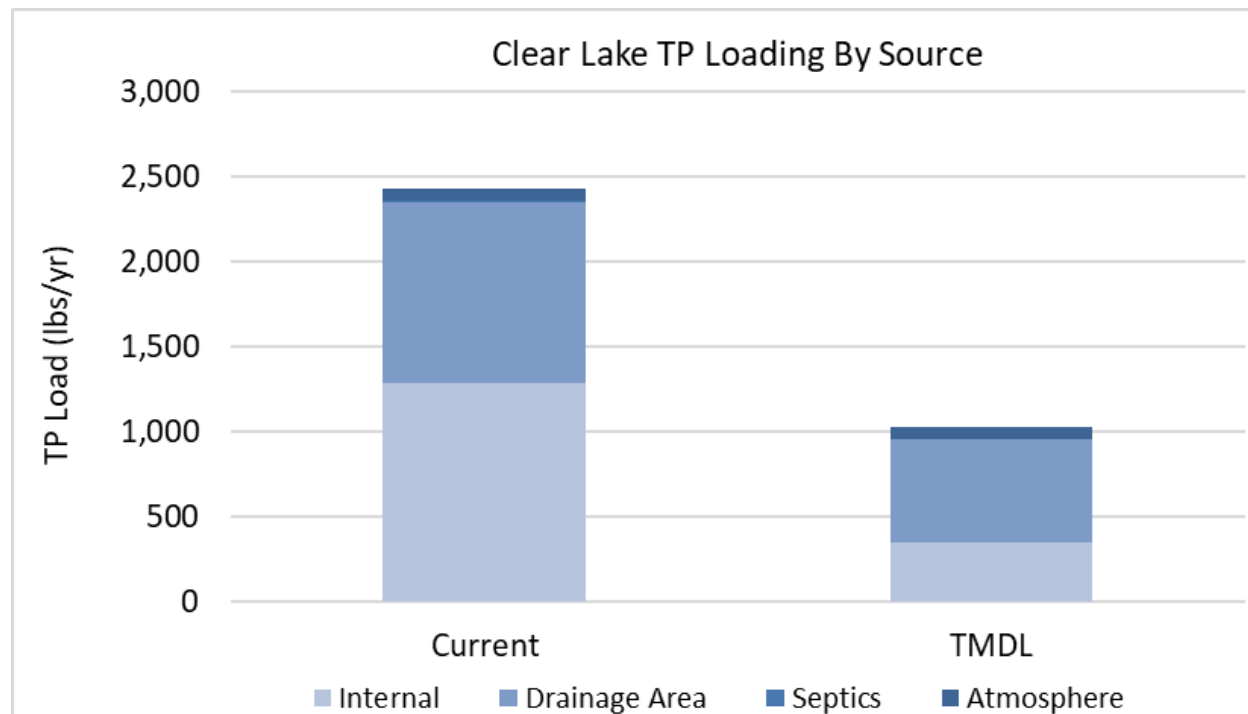


Table 43. Altermatt Lake (08-0054-00) phosphorus TMDL in the Cottonwood River Watershed.

Phosphorus		Existing TP load*		Allowable TP load		Estimated load reduction	
Sources		lbs/year	lbs/day	lbs/year	lbs/day	lbs/year**	%
Wasteload	Construction/Industrial SW	1	0.004	1	0.004	0	0%
	Total WLA	1	0.004	1	0.004	0	0%
Load	Watershed runoff	978	2.679	374	1.025	604	62%
	SSTS	9	0.026	4	0.012	5	54%
	Atmospheric deposition	29	0.080	29	0.080	0	0%
	Internal load	3,169	8.677	50	0.136	3,119	98%
	Total LA	4,185	11.462	457	1.253	3,728	89%
MOS				51	0.140		
Total load		4,186	11.466	509	1.397	3,728	88%

* Model calibration year(s): 2009 and 2010.

** Net reduction from current load to TMDL is 3,677 lbs/yr; but the gross load reduction from all sources must accommodate the MOS as well, and hence is 3,677 + 51 = 3,728 lbs/yr.

Figure 30. Altermatt Lake phosphorus source reductions to meet TMDL in the Cottonwood River Watershed.

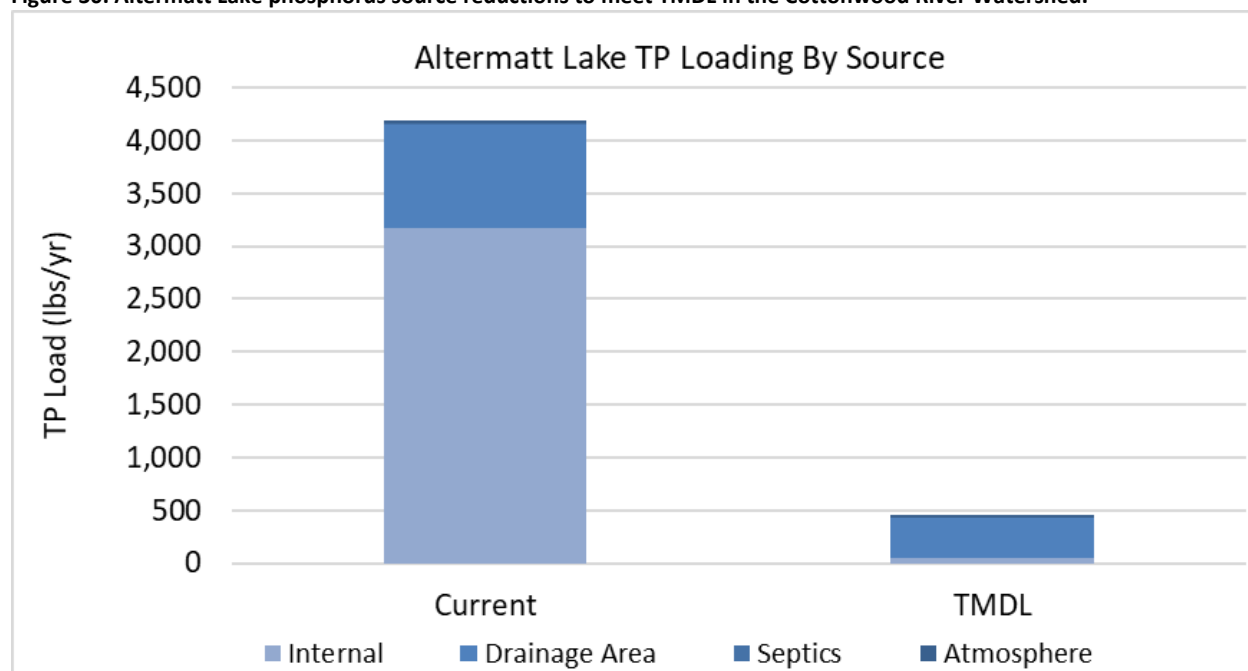


Table 44. Boise Lake (08-0096-00) phosphorus TMDL in the Cottonwood River Watershed.

Phosphorus		Existing TP load*		Allowable TP load		Estimated load reduction	
Sources		lbs/year	lbs/day	lbs/year	lbs/day	lbs/year**	%
Wasteload	Construction/Industrial SW	1	0.003	1	0.003	0	0%
	Total WLA	1	0.003	1	0.003	0	0%
Load	Watershed runoff	804	2.202	258	0.706	546	68%
	SSTS	8	0.023	4	0.010	4	50%
	Atmospheric deposition	42	0.114	42	0.114	0	0%
	Internal load	1,333	3.649	96	0.264	1,237	93%
	Total LA	2,187	5.988	400	1.094	1,787	82%
MOS				44	0.122		
Total load		2,188	5.991	445	1.219	1,787	80%

* Model calibration year(s): 2011 and 2012.

** Net reduction from current load to TMDL is 1,743 lbs/yr; but the gross load reduction from all sources must accommodate the MOS as well, and hence is 1,743 + 44 = 1,787 lbs/yr.

Figure 31. Boise Lake phosphorus source reductions to meet TMDL in the Cottonwood River Watershed.

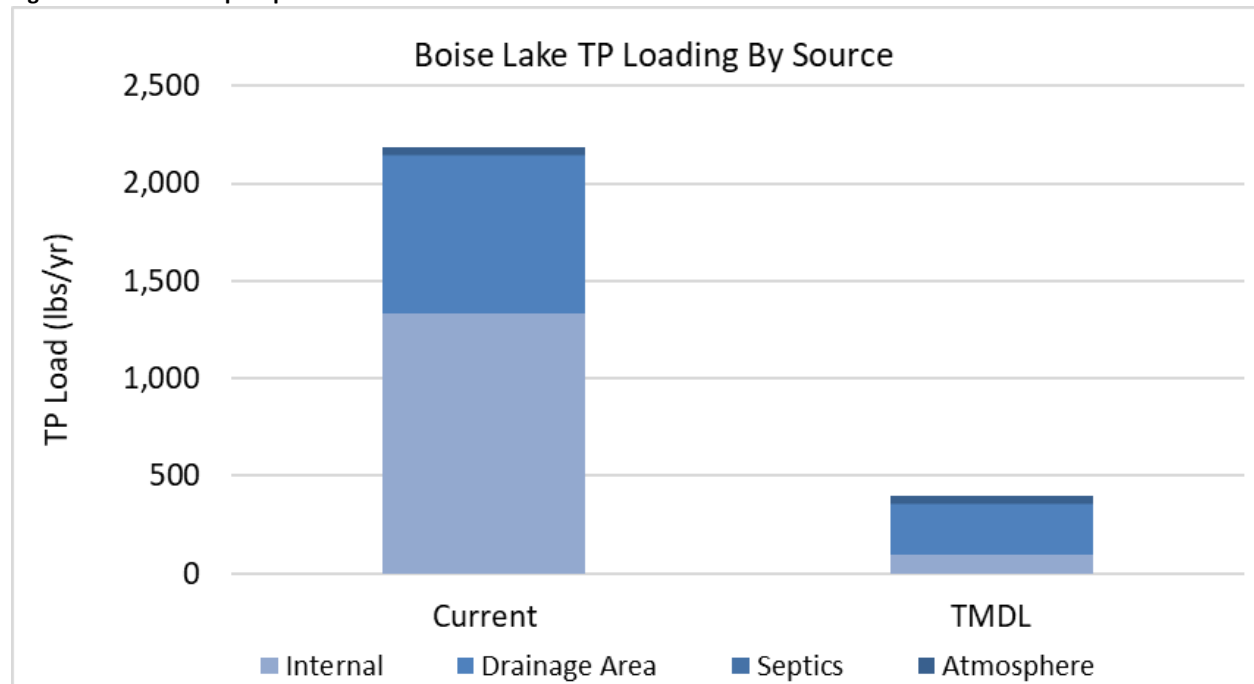


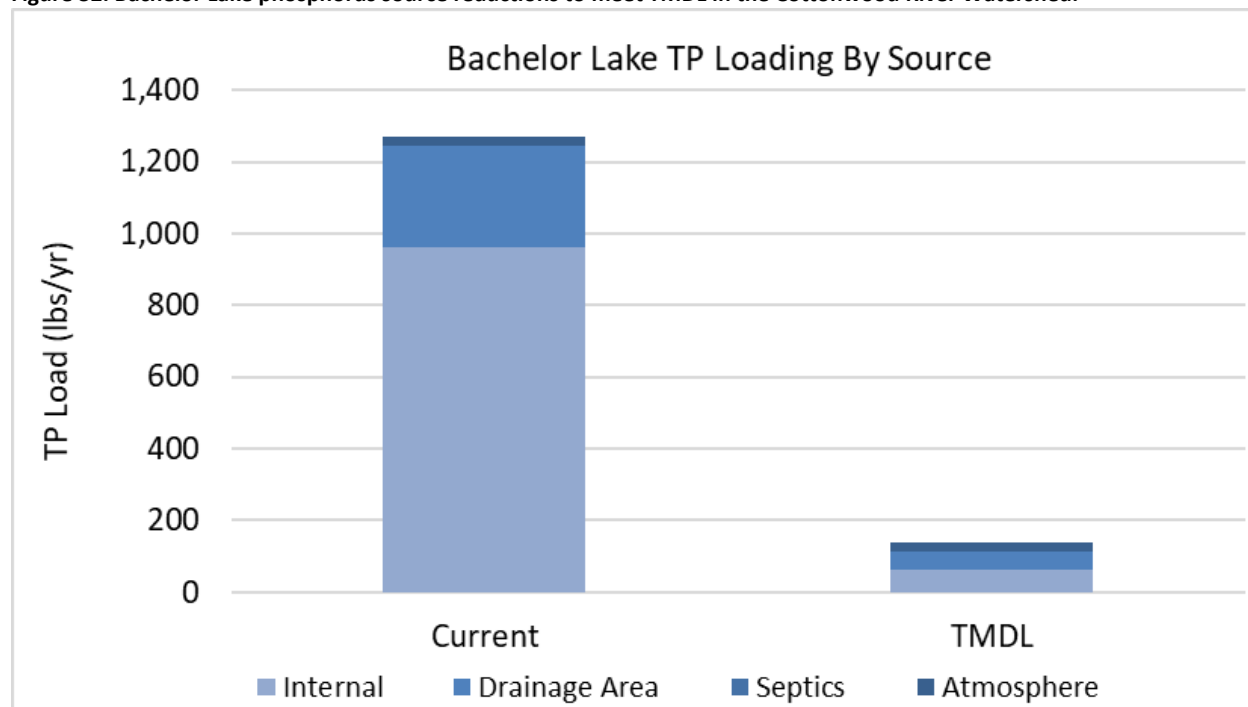
Table 45. Bachelor Lake (08-0029-00) phosphorus TMDL in the Cottonwood River Watershed.

Phosphorus		Existing TP load*		Allowable TP load		Estimated load reduction	
Sources		lbs/year	lbs/day	lbs/year	lbs/day	lbs/year**	%
Wasteload	Construction/Industrial SW	0.4	0.001	0.4	0.001	0.0	0%
	Total WLA	0.4	0.001	0.4	0.001	0.0	0%
Load	Watershed runoff	282.2	0.773	50.5	0.138	231.7	82%
	SSTS	0.6	0.002	0.4	0.001	0.2	33%
	Atmospheric deposition	23.3	0.064	23.3	0.064	0.0	0%
	Internal load	962.8	2.636	63.6	0.174	899.2	93%
	Total LA	1,268.9	3.475	137.8	0.377	1,131.1	89%
MOS				15.4	0.042		
Total load		1,269.3	3.476	153.6	0.420	1,131.1	88%

* Model calibration year(s): 2011 and 2012.

** Net reduction from current load to TMDL is 1,115.7 lbs/yr; but the gross load reduction from all sources must accommodate the MOS as well, and hence is 1,115.7 + 15.4 = 1,131.1 lbs/yr.

Figure 32. Bachelor Lake phosphorus source reductions to meet TMDL in the Cottonwood River Watershed.



5. Future Growth Considerations

According to the Minnesota State Demographic Center (Minnesota Department of Administration 2015) from 2015 to 2035, the populations of all five counties in the Cottonwood River Watershed are projected to decrease by 3% (Lyon County) to as much as 18% (Redwood County). The overall projection for all five counties is negative 8%. The MPCA does not anticipate significant population growth within the Cottonwood River Watershed.

5.1 New or Expanding Permitted MS4 WLA Transfer Process

Future transfer of watershed runoff loads in this TMDL may be necessary if any of the following scenarios occur within the project watershed boundaries.

1. New development occurs within a regulated MS4. Newly developed areas that are not already included in the WLA must be transferred from the LA to the WLA to account for the growth.
2. One regulated MS4 acquires land from another regulated MS4. Examples include annexation or highway expansions. In these cases, the transfer is WLA to WLA.
3. One or more nonregulated MS4s become regulated. If this has not been accounted for in the WLA, then a transfer must occur from the LA.
4. Expansion of a U.S. Census Bureau Urban Area encompasses new regulated areas for existing permittees. An example is existing state highways that were outside an urban area at the time the TMDL was completed, but are now inside a newly expanded urban area. This will require either a WLA to WLA transfer or a LA to WLA transfer.
5. A new MS4 or other stormwater-related point source is identified and is covered under a NPDES Permit. In this situation, a transfer must occur from the LA.

Load transfers will be based on methods consistent with those used in setting the allocations in this TMDL. In cases where WLA is transferred from or to a regulated MS4, the permittees will be notified of the transfer and have an opportunity to comment.

5.2 New or Expanding Wastewater (TSS and *E. coli* TMDLs only)

The MPCA, in coordination with the EPA Region 5, has developed a streamlined process for setting or revising WLAs for new or expanding wastewater discharges to water bodies with an EPA approved TMDL (MPCA 2012). This procedure will be used to update WLAs in approved TMDLs for new or expanding wastewater dischargers whose permitted effluent limits are at or below the instream target and will ensure that the effluent concentrations will not exceed applicable water quality standards or surrogate measures. The process for modifying any and all WLAs will be handled by the MPCA, with input and involvement by the EPA, once a permit request or reissuance is submitted. The overall process will use the permitting public notice process to allow for the public and EPA to comment on the permit changes based on the proposed WLA modification(s). Once any comments or concerns are addressed, and the MPCA determines that the new or expanded wastewater discharge is consistent with the applicable water quality standards, the permit will be issued and any updates to the TMDL WLA(s) will be made.

For more information on the overall process, visit the MPCA's [TMDL Policy and Guidance](#) webpage.

6. Reasonable Assurance

A TMDL needs to provide reasonable assurance that water quality targets will be achieved through the specified combination of point and nonpoint source reductions reflected in the LAs and WLAs. According to EPA guidance (EPA 2002a), “When a TMDL is developed for waters impaired by both point and nonpoint sources, and the WLA is based on an assumption that nonpoint-source load reductions will occur... the TMDL should provide reasonable assurances that nonpoint-source control measures will achieve expected load reductions in order for the TMDL to be approvable. This information is necessary for the EPA to determine that the TMDL, including the LA and WLAs, has been established at a level necessary to achieve water quality standards”. In the Cottonwood River Watershed considerable reductions in nonpoint sources are required.

The MPCA will:

- Evaluate existing programmatic, funding, and technical capacity to implement basin and watershed strategies.
- Identify gaps in current programs, funding, and local capacity to achieve the needed controls.
- Build program capacity for short-term and long-term goals. Demonstrate increased implementation and/or pollutant reductions.
- Commit to track/monitor/assess and report progress at set regular times.

6.1 Regulatory

6.1.1 Construction Stormwater

Regulated construction stormwater was given a categorical WLA in this study. Construction activities disturbing one acre or more are required to obtain NPDES permit coverage through the MPCA. Compliance with TMDL requirements are assumed when a construction site owner/operator meets the conditions of the Construction General Permit and properly selects, installs, and maintains all BMPs required under the permit, including any applicable additional BMPs required in Section 23 of the Construction General Permit for discharges to impaired waters, or compliance with local construction stormwater requirements if they are more restrictive than those in the State General Permit.

6.1.2 Industrial Stormwater

Industrial stormwater was given a categorical WLA in this study. Industrial activities require permit coverage under the state's NPDES/SDS Industrial Stormwater Multi-Sector General Permit (MNR050000) or NPDES/SDS Nonmetallic Mining/Associated Activities General Permit (MNG490000). If a facility owner/operator obtains stormwater coverage under the appropriate NPDES/SDS permit and properly selects, installs, and maintains BMPs sufficient to meet the benchmark values in the permit, the stormwater discharges would be expected to be consistent with the WLA in this TMDL report.

6.1.3 MS4 Permits

The MPCA is responsible for applying federal and state regulations to protect and enhance water quality in Minnesota. The MPCA oversees stormwater management accounting activities for all MS4 entities listed in this TMDL report. The MS4 General Permit requires regulated municipalities to implement

BMPs that reduce pollutants in stormwater to the maximum extent practicable. A critical component of permit compliance is the requirement for the owners or operators of a permitted MS4 conveyance to develop a SWPPP. The SWPPP addresses all permit requirements, including the following six measures:

- Public education and outreach
- Public participation
- Illicit discharge detection and elimination program
- Construction site runoff controls
- Post-construction runoff controls
- Pollution prevention and municipal good housekeeping measures

A SWPPP is a management plan that describes the MS4 permittee's activities for managing stormwater within their regulated area. In the event of a completed TMDL study, MS4 permittees must document the WLA in their future NPDES/SDS permit application and provide an outline of the BMPs to be implemented that address needed reductions. The MPCA requires MS4 owners or operators to submit their application and corresponding SWPPP document to the MPCA for review. Once the application and SWPPP are deemed adequate by the MPCA, all application materials are placed on 30-day public notice, allowing the public an opportunity to review and comment on the prospective program. Once NPDES/SDS permit coverage is granted, permittees must implement the activities described within their SWPPP and submit an annual report to the MPCA documenting the implementation activities completed within the previous year, along with an estimate of the cumulative pollutant reduction achieved by those activities.

The MS4 General Permit requires permittees to develop compliance schedules for EPA approved TMDL WLAs not already being met at the time of permit application. A compliance schedule includes BMPs that will be implemented over the permit term, a timeline for their implementation, and a long-term strategy for continuing progress towards assigned WLAs. For WLAs being met at the time of permit application, the same level of treatment must be maintained in the future. This TMDL report assigns TSS WLAs to the City of Marshall, a permitted MS4. However, as there is an assessed unimpaired reach between the City's outfall and the TSS impaired reaches, no reductions are required for the city's MS4. Regardless of WLA attainment or required reductions, all permitted MS4s are still required to reduce pollutant loadings to the maximum extent practicable.

The MPCA's stormwater program and its NPDES permit program are regulatory activities providing reasonable assurance that implementation activities are initiated, maintained, and consistent with WLAs assigned in this study.

6.1.4 Wastewater NPDES and SDS Permits

The MPCA issues permits for WWTPs or industrial facilities that discharge into waters of the state. The permits have site specific limits on TSS and other parameters that are based on water quality standards. Permits regulate discharges with the goals of 1) protecting public health and aquatic life, and 2) assuring that every facility treats wastewater. In addition, NPDES and SDS Permits set limits and establish controls for land application of waste and byproducts. Permits issued under the NPDES program are required to have effluent limits consistent with the assumptions and requirements of the WLAs in this

TMDL. Compliance with the WLAs, as developed and presented in this TMDL, is assumed to ensure meeting the water quality standards for all TSS 303(d) listings.

Bacteria, TSS, and Lake Phosphorus

WWTPs discharging to the TSS and *E. coli* impaired reaches did not require any changes to their discharge permit limits due to the WLAs calculated in this TMDL report. No WWTPs discharge to the impaired lakes addressed in this TMDL report.

6.1.5 SSTS Program

SSTS, commonly known as septic systems, are regulated by Minn. Stat. §§ 115.55 and 115.56. Counties and other Local Government Unit (LGUs) that regulate SSTS must meet the requirements for local SSTS programs in Minn. R. ch. 7082. Counties and other LGUs must adopt and implement SSTS ordinances in compliance with Minn. R. chs. 7080 - 7083.

These regulations detail:

- Minimum technical standards for individual and mid-size SSTS;
- A framework for LGUs to administer SSTS programs and;
- Statewide licensing and certification of SSTS professionals, SSTS product review and registration, and establishment of the SSTS Advisory Committee.

Counties and other LGUs enforce Minn. R. chs. 7080 through 7083 through their local SSTS ordinance and issue permits for systems designed with flows up to 10,000 gallons per day. There are approximately 200 LGUs across Minnesota, and depending on the location an LGU may be a county, city, township, or sewer district. LGU SSTS ordinances vary across the state. Some require SSTS compliance inspections prior to property transfer, require permits for SSTS repair and septic tank maintenance, and may have other requirements which are stricter than the state regulations.

Compliance inspections by Counties and other LGUs are required by Minnesota Rule for all new construction and for existing systems if the LGU issues a permit for the addition of a bedroom. In order to increase the number of compliance inspections, the MPCA has developed and administers funds to LGUs for various ordinances, and specific actions. Additional funding dollars are awarded to counties that have provisions in their ordinance above the minimum program requirements. The MPCA has worked with counties through the SSTS Implementation and Enforcement Task Force (SIETF) to identify the most beneficial ways to use these funds to accelerate SSTS compliance statewide:

- Compliance inspection for property transfer;
- Compliance inspection for any (all) permit-countywide;
- Plan to improve compliance, such as records catalog or inventory (past, ongoing or future); and
- Plan to address unsewered areas.

The MPCA staff keep a statewide database of known ITPHS systems that include “straight pipe systems”. These straight pipe systems are reported to the counties or the MPCA by the public. Upon confirmation of a straight pipe system, the county sends out a notification of noncompliance, which starts a 10-month deadline to fix the system and bring it into compliance. From 2006 through 2017, 742 straight pipes

have been tracked by the MPCA. Seven hundred-one of those were abandoned, fixed, or were found not to be a straight pipe system as defined in Minn. Stat. 115.55, subd. 1. There have been 17 Administrative Penalty Orders issued and docketed in court. The remaining straight pipe systems received a notification of noncompliance and are currently within the 10-month deadline.

Since 1996, the MPCA southwest wastewater staff have helped small communities build wastewater soil treatment systems throughout the region. The unsewered communities within the Cottonwood River Watershed are all addressing their wastewater treatment through SSTS upgrades regulated by county ordinances and funded by various sources, such as the Clean Water Fund (CWF) and Clean Water Partnership (CWP) State Revolving Fund (SRF) Loan Program.

6.1.6 Feedlot Program

All feedlots in Minnesota are regulated by Minn. R. ch. 7020. The MPCA has regulatory authority of feedlots but counties may choose to participate in a delegation of the feedlot regulatory authority to the local unit of government. Delegated counties are then able to enforce Minn. R. ch. 7020 (along with any other local rules and regulations) within their respective counties for facilities that are under the CAFO threshold. In the Cottonwood River Watershed, the counties of Lyon, Murray, Cottonwood, and Brown are the delegated feedlot regulatory authority. The only nondelegated county in the Cottonwood River Watershed is Redwood County. The Counties and MPCA will continue to implement the feedlot program and work with producers on MMPs.

The MPCA regulates the collection, transportation, storage, processing, and disposal of animal manure and other livestock operation waste. The MPCA Feedlot Program implements rules governing these activities and provides assistance to counties and the livestock industry. The feedlot rules apply to most aspects of livestock waste management including the location, design, construction, operation, and management of feedlots and manure handling facilities.

There are two primary concerns about feedlots in protecting water:

- Ensuring that manure on a feedlot or manure storage area does not run into water.
- Ensuring that manure is applied to cropland at a rate, time and method that prevents bacteria and other possible contaminants from entering streams, lakes and ground water.

6.1.7 Buffers and Shoreland

Minnesota's buffer law requires perennial vegetative buffers along public ditches, lakes, rivers, and streams. Buffers along lakes, rivers, and streams are to be 50 feet in width, and buffers along public ditches are to be 16.5 feet wide or more. These buffers help filter out phosphorus, nitrogen, and sediment. Buffers are critical to protecting and restoring water quality and healthy aquatic life, natural stream functions, and aquatic habitat due to their immediate proximity to the water. The law provides some flexibility for landowners to install alternative practices if they provide equal or better water quality benefits. An example of an alternative practice could be a narrower buffer if the land slopes away from the water body. This is not uncommon with some ditches, rivers, and streams. Alternative practices must be approved by the local governmental unit that implements the buffer law.

Most of the private lands in the Cottonwood River Watershed contain well vegetated buffers along ditches, lakes, and streams. Reported rates of compliance for all four counties in the Cottonwood River Watershed are between 95% and 100% (Board of Water and Soil Resources; [BWSR website](#)).

Other nonpoint source statutes/rules include:

- Protecting highly erodible land within the 300-foot shoreland district (Minn. Stat. § 103F.201)
- Excessive soil loss statute (Minn. Stat. § 103F.415)
- Nuisance nonpoint source pollution (Minn. R. 7050.0210, subp. 2)

6.2 Nonregulatory

6.2.1 Pollutant Load Reduction

Reliable means of reducing nonpoint source pollutant loads are fully addressed in the WRAPS report (MPCA 2022), a document that is written to be a companion to this TMDL. In order for the impaired waters to meet water quality standards, the majority of pollutant reductions in the Cottonwood River Watershed will need to come from nonpoint sources. Agricultural drainage and surface runoff are major contributors of nutrients, bacteria, sediment, and increased flows throughout the watershed. As described in the WRAPS report, the BMPs identified for restoration have all been demonstrated to be effective in reducing transport of pollutants to surface water. The combinations of BMPs discussed throughout the WRAPS process were derived from Minnesota's Nutrient Reduction Strategy (NRS) (MPCA 2015a) and related tools. As such, they were vetted by a statewide engagement process prior to being applied in the Cottonwood River Watershed.

Selection of sites for BMPs will be led by LGUs, including SWCDs, watershed management organizations, and county planning and zoning, through the One Watershed, One Plan (1W1P) process, which was awarded planning funding for this watershed in August 2022, with support from state and federal agencies. These BMPs are supported by programs administered by the SWCDs and the Natural Resources Conservation Service (NRCS). Local resource managers are well-trained in promoting, placing, and installing these BMPs. Some counties within the basin have shown significant levels of adoption of these practices. State and local agencies will need to work with landowners to identify priority areas for BMPs and practices that will help reduce nutrient runoff, as well as streambank and overland erosion. Agencies, organizations, LGUs, and citizens alike need to recognize that allowing waters to be in an impaired condition is not acceptable. Throughout the course of the WRAPS and TMDL meetings, local stakeholders endorsed the BMPs selected in the WRAPS report. These BMPs reduce pollutant loads from runoff (i.e., phosphorus, sediment and pathogens) and loads delivered through drainage tiles or groundwater flow (e.g., nitrates).

To help achieve nonpoint source reductions, a large emphasis has been placed on public participation, where the citizens and urban communities that hold the power to improve water quality conditions are involved in discussions and decision-making. The watershed's citizens and urban communities will need to voluntarily adopt the practices at the necessary scale and rates to achieve the 10-year targets presented in Implementation Table 14- through Table 22 of the WRAPS report and the [Minnesota Stormwater Manual](#). The WRAPS also presents the pollutant/stressor reduction goals and targets and the estimated years to meet the goal developed by the WRAPS Local Work Group (LWG). The strategies

identified and relative adoption rates developed by the WRAPS LWG were used to calculate the adoption rates needed to meet the pollutant/stressor 10-year targets. In addition to public participation, several government programs are in place to support a political and social infrastructure that aims to increase the adoption of strategies that will improve watershed conditions and reduce loading from nonpoint sources.

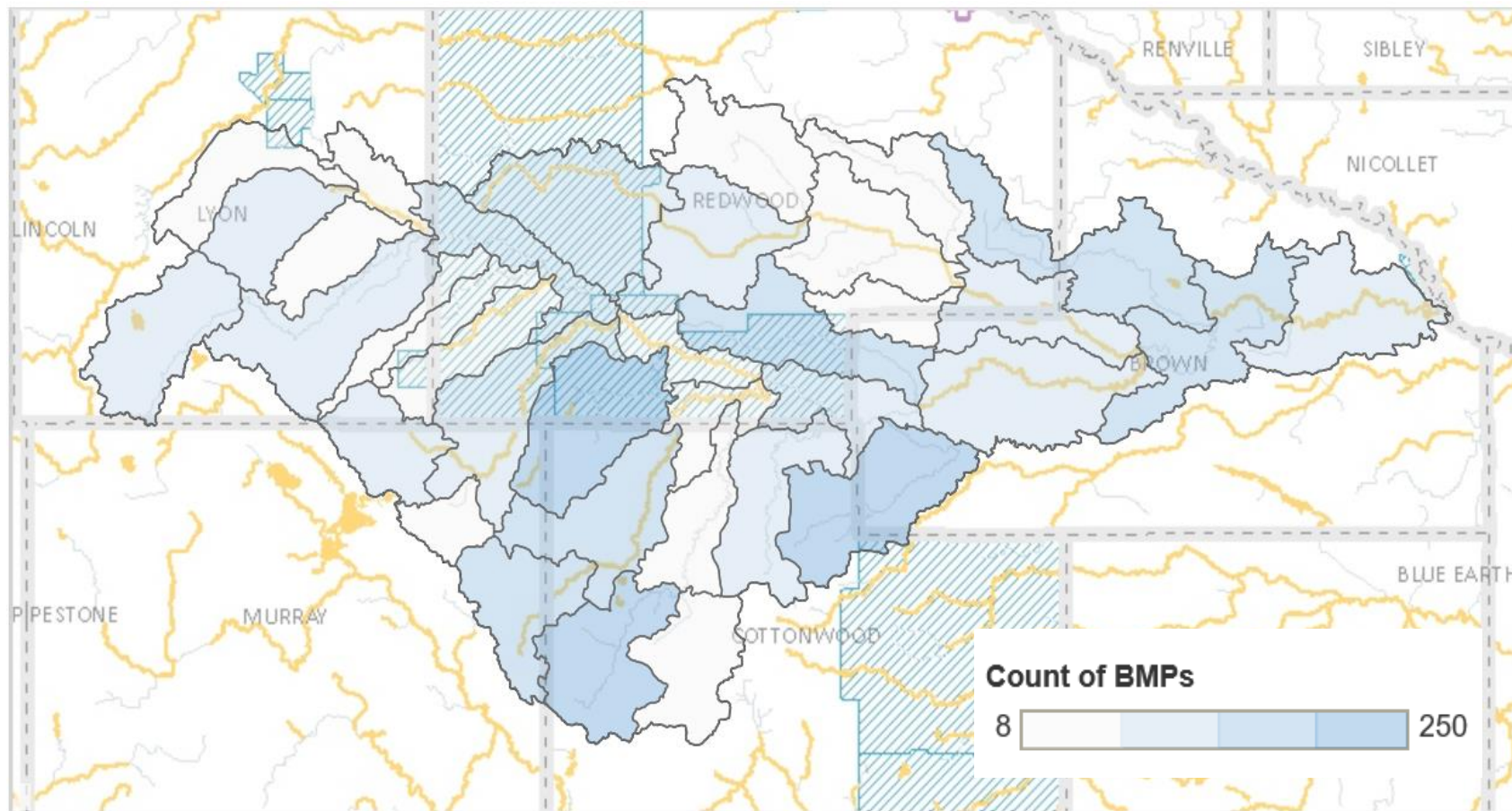
Several nonpermitted reduction programs exist to support implementation of nonpoint source reduction BMPs in the Cottonwood River Watershed. These programs identify BMPs, provide means of focusing BMPs, and support their implementation via state initiatives, ordinances, and/or dedicated funding.

From 2004 to 2019, over 3,500 BMPs were installed in the Cottonwood River Watershed by local partners. Table 46 summarizes the major types of BMPs that have been implemented throughout the watershed, while Figure 33 depicts the number of BMPs per subwatershed in the Cottonwood River Watershed. Additional information about the BMPs may be found on the [MPCA’s Healthier Watershed website](#).

Table 46. Reported BMPs in the Cottonwood River Watershed by BMP type (2004-2021).

BMP Type	Total BMPs
Tile Inlet Improvements	266
Tillage/residue Management	480
Nutrient Management (Cropland)	430
Septic System Improvements	48
Designed Erosion Control	271
Converting Land to Perennials	157
Buffers and Filters	59
Living Cover to Crops in Fall/Spring	135
Stream Banks, Bluffs, and Ravines	101
Pasture Management	63
Tile Drainage Treatment/Storage	11
Habitat and Stream Connectivity	9
Crop Rotation	19

Figure 33. Numbers of BMPs installed in the Cottonwood River Watershed by subwatershed.



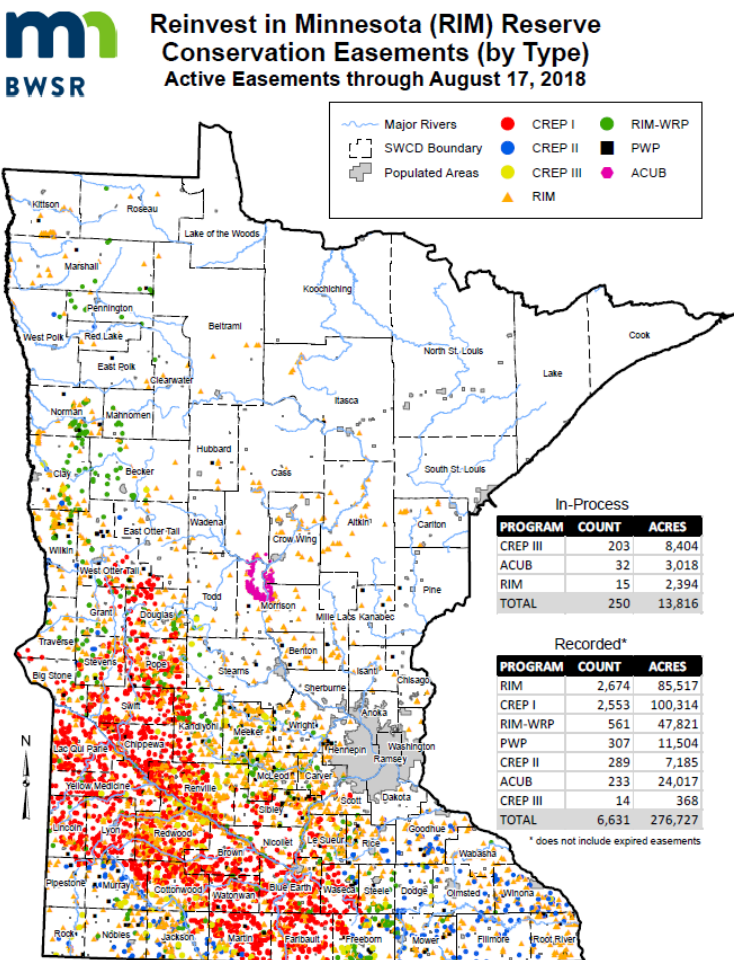
Further, two Minnesota Department of Agriculture (MDA) led initiatives - [The Nutrient Management Initiative Program](#) (NMI) and [The Agricultural Water Quality Certification Program](#) (MAWQCP) – have engaged farmers and increased agricultural BMP adoption in the Cottonwood River Watershed. The NMI Program has provided financial incentives for participants to conduct on-farm trials comparing related to nitrogen fertilizer rate management. A total of 31 nutrient trials took place in the Cottonwood and Redwood River Watersheds between 2006 and 2019. MAWQCP is a voluntary opportunity for farmers and agricultural landowners to take the lead in implementing conservation practices that protect water quality. Those who implement and maintain approved farm management practices are certified and in turn obtain regulatory certainty for a period of 10 years. In the Cottonwood River Watershed, there are 16 MAWQCP-certified producers that cover 12,239 acres. BMPs implemented to-date through this program include:

- 84 alternative/closed tile intakes
- 231 acres of pest management
- 19 sediment basins
- 4 acres of filter strips
- 1,431 acres of residue management
- 887 acres of nutrient management
- 946 acres nitrogen BMPs
- 313 acres cover crops
- 2,000 ft grassed waterway

Conservation Easements

Conservation easements are a critical component of the state’s efforts to improve water quality by reducing soil erosion, phosphorus, and nitrogen loading, and improving wildlife habitat and flood attenuation on private lands. Easements protect the state’s water and soil resources by permanently restoring wetlands, adjacent native grassland wildlife habitat complexes, and permanent riparian buffers. In cooperation with county SWCDs and the USDA NRCS, BWSR’s programs compensate landowners for granting conservation easements and establishing native vegetation habitat on economically marginal, flood-prone, environmentally sensitive, or highly erodible lands. These easements vary in length of time from 10 years to permanent/perpetual easements. Types of conservation easements in Minnesota include: Conservation Reserve Program (CRP); Conservation Reserve Enhancement Program (CREP); Reinvest in Minnesota (RIM); and the Wetland Reserve Program (WRP) or Permanent Wetland Preserve (PWP) (Figure 34).

Figure 34. Conservation easements in Minnesota.



6.2.2 Prioritization

[Water Quality Trends for Minnesota Rivers and Streams at Milestone Sites](#) notes that sites across Minnesota, including the Cottonwood River, show long-term reductions in TSS, ammonia, and biochemical oxygen demand (MPCA 2014). [The Minnesota NRS](#) documented a 33% reduction of the phosphorus load leaving the state via the Mississippi River from the pre-2000 baseline to current (MPCA 2015). These reports generally agree that while further reductions are needed, municipal and industrial phosphorus loads as well as loads of runoff-driven pollutants (i.e., TSS) are decreasing; a conclusion that lends assurance that the Cottonwood River WRAPS and TMDL goals and strategies are reasonable and that long-term, enduring efforts to decrease erosion and nutrient loading to surface waters have the potential to reduce pollutant loads.

The WRAPS report details several tools that provide means for identifying priority pollutant sources and implementation work in the watershed. Further, LGUs in the Cottonwood River Watershed often employ their own local analyses for determining priorities.

The State of Minnesota has provided tools to further the buffer initiative; they are being used in the implementation planning process to examine riparian land use in the Cottonwood River Watershed, and prioritize potential buffer installation. The Buffer Initiative was signed into law by Governor Dayton in June 2015 (amended by the Legislature and signed into law by Governor Dayton on April 25, 2016). It

provides clarification regarding which waters need buffers, a timeline for implementing them, and tools for LGUs to use in tracking and reporting compliance (<http://www.bwsr.state.mn.us/buffers/>).

Light Detection and Ranging (LiDAR) data and hydro-conditioned DEMs are available for the entire Cottonwood River Watershed. These data are being increasingly used by LGUs to examine landscapes, understand watershed hydrology, and prioritize BMP targeting.

6.2.3 Funding

On November 4, 2008, Minnesota voters approved the Clean Water, Land, and Legacy Amendment to the State constitution to:

- protect drinking water sources;
- protect, enhance, and restore wetlands, prairies, forests, and fish, game, and wildlife habitat;
- preserve arts and cultural heritage;
- support parks and trails; and
- protect, enhance, and restore lakes, rivers, streams, and groundwater.

This is a secure funding mechanism with the explicit purpose of supporting water quality improvement projects.

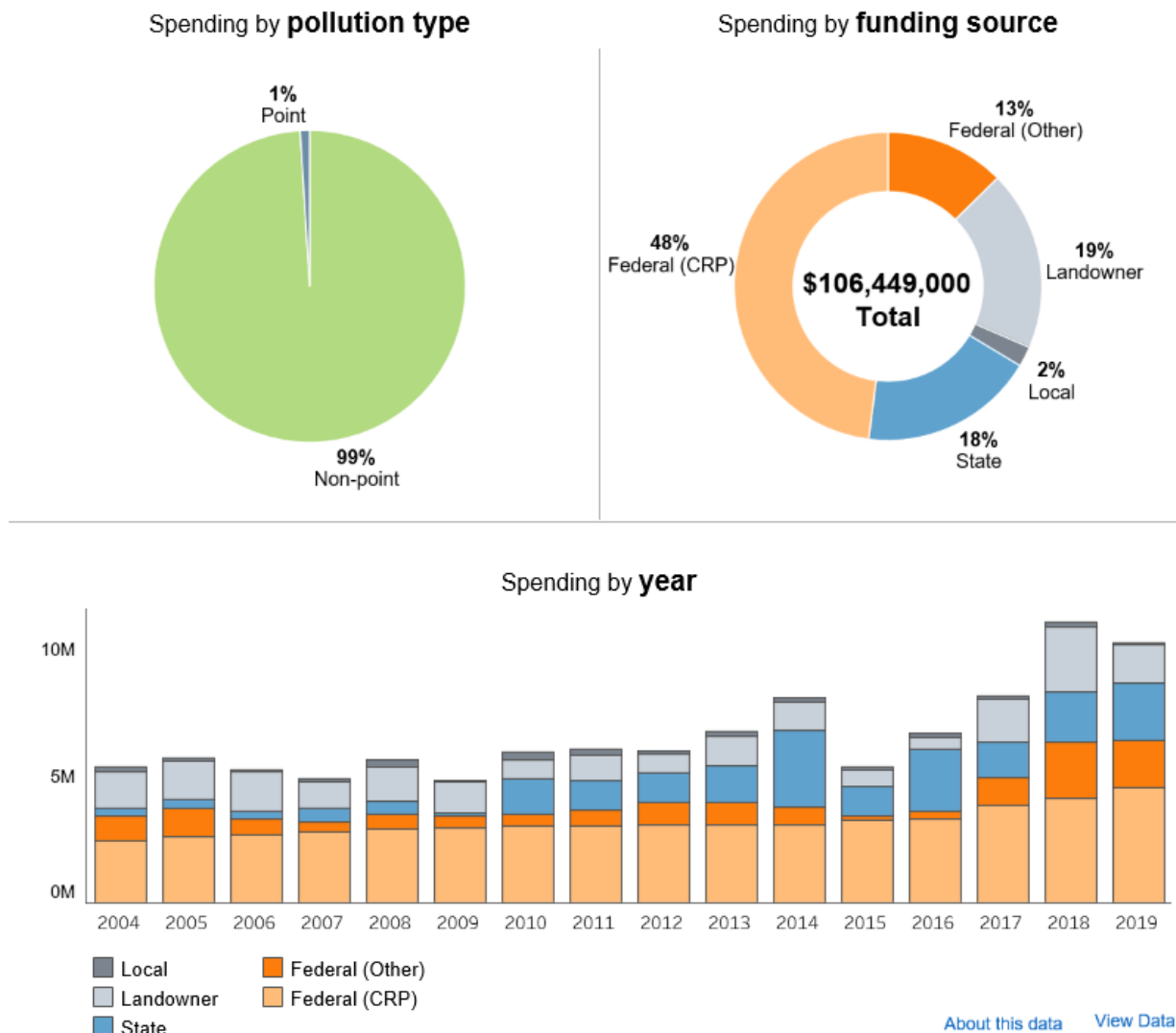
Additionally, there are many other funding sources for nonpoint pollutant reduction work; they include but are not limited to Clean Water Act Section 319 grant programs, BWSR state CWF implementation funding, and NRCS incentive programs. Programs and activities are also occurring at the local government level, where county staff, commissioners, and residents work together to address water quality issues. In the past, several state CWP and federal Section 319 grants have been utilized to implement nonpoint source BMPs.

Minnesota was awarded \$500 million to implement the CREP that when fully implemented will convert approximately 60,000 acres of land to perennial cover (perpetual easements). Riparian areas and marginal agricultural land are a focus of the program. This aligns precisely with statewide and Cottonwood River Watershed strategies focused on converting marginal lands to perennials to reduce pollutant loading to surface and groundwater.

Since 2004, over \$106 million have been spent addressing water quality issues in the Cottonwood River Watershed (Figure 35). Additional information about funding may be found on the [MPCA's Healthier Watersheds](#) website.

Figure 35. Spending addressing water quality issues in the Cottonwood River Watershed.

Cottonwood River watershed within all counties



6.2.4 Planning and Implementation

The WRAPS, TMDLs, and all the supporting documents provide a foundation for planning and implementation. Subsequent planning, including imminent development of a 1W1P comprehensive watershed management plan for the Cottonwood River Watershed awarded planning funding in August 2022, will draw on the goals, technical information, and tools to describe in detail strategies and actions for implementation. For the purposes of reasonable assurance, the WRAPS document is sufficient in that it provides strategies for achieving pollutant reduction goals. However, many of the goals outlined in this TMDL are very similar to objectives outlined in the individual county water plans. All counties in the Cottonwood River Watershed currently have approved, up-to-date water management plans. Some general goals and themes in the individual county water plans are consistent such as:

- Protect, manage and improve surface waters;

- Target landscapes and sites for increased conservation practices and reduction in feedlot and septic pollutants;
- Reduce flooding, erosion, sediment, and nutrient loading;
- Identify, design, and improve drainage management, water retention, and concentrated flow;
- Protect groundwater resources.

These county plans have the same goal of removing streams and lakes from the 303(d) Impaired Waters List. These plans provide watershed specific strategies for addressing water quality and quantity issues. In addition, the commitment and support from the local governmental units will ensure that this TMDL project is carried successfully through implementation. The 1W1P that will be developed for the watershed will be a cohesive, watershed-wide plan across all LGUs. TMDL and WRAPS goals will be incorporated in the process.

6.2.5 Tracking Progress

Water monitoring efforts within the Cottonwood River Watershed are diverse and constitute a sufficient means for tracking progress and supporting adaptive management. See Chapter 7 for more information on monitoring efforts and programs in the Cottonwood River Watershed. The MPCA’s Healthier Watersheds web application tracks implementation efforts and funding for the watershed.

6.2.6 Reasonable Assurance Summary

In summary, significant time and resources have been devoted to identifying the best BMPs and supporting their implementation via state initiatives and dedicated funding in southwest Minnesota and in the Cottonwood River Watershed.

The WRAPS and TMDL process engaged partners to arrive at reasonable examples of BMP combinations that achieve pollutant reduction goals. Minnesota is a leader in watershed planning, monitoring, and tracking progress toward water quality goals. Finally, examples cited herein confirm that BMPs and restoration projects have proven to be effective over time and as stated in A15-1622 MCEA vs MPCA & MCEA (Minnesota Court of Appeals 2016):

“We conclude that substantial evidence exists to conclude that voluntary reductions from nonpoint sources have occurred in the past and can be reasonably expected to occur in the future. The Nutrient Reduction Strategy (NRS) [...] provides substantial evidence of existing state programs designed to achieve reductions in nonpoint source pollution as evidence that reductions in nonpoint pollution have been achieved and can reasonably be expected to continue to occur.”

7. Monitoring Plan

Several types of monitoring are necessary to track progress toward achieving the load reductions required for the TMDLs and the achievement of water quality standards. Water monitoring combined with tracking implementation of BMPs on the ground is critical in the adaptive management approach to implementing TMDLs. The LGUs will track the implementation of BMPs annually through BWSR's e-LINK system. This, and other data (e.g. USDA data) are readily available via the MPCA's Healthier Watersheds web application. Monitoring results will identify progress toward obtainable benchmark goals as well as shape the next course of action for implementation through adaptive management. Data from water quality monitoring programs enables water quality condition assessment and creates a long-term data set to track progress toward water quality goals. These programs will continue to collect and analyze data in the Cottonwood River Watershed as part of [Minnesota's Water Quality Monitoring Strategy](#) (MPCA 2021). Data needs are considered by each program and additional monitoring is implemented when deemed necessary and feasible. These monitoring programs are summarized as follows:

- [Intensive Watershed Monitoring](#) collects water quality and biological data for 2 years at established stream and lake monitoring stations across the Cottonwood River Watershed every 10 years. The MPCA, with assistance from LGUs, will re-visit and re-assess these monitoring stations, as well as have capacity to visit new sites in areas with BMP implementation activity, beginning in 2027. It is anticipated that funding for monitoring and analysis will be available through the MPCA.
- [Watershed Pollutant Load Monitoring Network](#) data provides a continuous and long-term record of water quality conditions at the major watershed and subwatershed scale. This program collects pollutant samples and flow data to calculate continuous daily flow, sediment, and nutrient loads. There are three sites in the Cottonwood River Watershed with data that vary by site.
- [Volunteer Stream and Lake Monitoring Program](#) data provide a continuous record of water body transparency throughout much of the basin. This program relies on a network of volunteers who make monthly stream and lake measurements annually. There is currently a limited number of volunteers doing monitoring within the Cottonwood River Watershed. The MPCA will seek more volunteer monitors to track trends of water quality transparency for impaired waters within the watershed.
- [RCRCA](#) has a long history of water quality monitoring in the Cottonwood River Watershed with a special focus on sediment and nutrient contributions from tributaries of the Cottonwood River. Water quality monitoring efforts have been based on a three-tier system. Primary, secondary, and tertiary monitoring stations have been developed to assess areas of the watershed delivering the greatest amount of sediment and nutrients to the Cottonwood River. This information has been used to select priority management areas and measure progress toward watershed goals.
- [MDA's pesticide monitoring program](#) goal is to determine the presence and concentration of pesticides in Minnesota waters, and present long-term trend analysis based on information collected over the past 30 years. Trend analysis requires long-term investments in monitoring

within the MDA's established networks. The MDA releases an annual water quality monitoring report that includes all pesticide water quality data and long-term trends available on MDA's website. The MDA will continue to conduct statewide pesticide monitoring in the future and will provide additional information related to the occurrence of pesticides in Minnesota waters.

The MDA completed 14 pesticide water quality sample collection events from seven lakes within the Cottonwood and Redwood River watersheds from 2012 through 2019. Double Lake was added to the 2020 303(d) Impaired Waters List for the insecticide chlorpyrifos due to one detection each in 2017 and 2018. No other lakes sampled in the Cottonwood River Watershed were above an applicable pesticide water quality reference value. The MDA will continue to monitor Double Lake until it can be delisted from the Impaired Waters List.

The MDA completed 517 pesticide and/or nutrient water quality sample collection events from 10 river and stream locations within the Cottonwood and Redwood River watersheds from 1992 through 2019. Sleepy Eye Creek at Cobden and the Cottonwood River at New Ulm were sampled within the Cottonwood River Watershed. Sleepy Eye Creek was designated on the 2018 Impaired Waters List for the insecticide chlorpyrifos due to detection in 2015 and 2016. No other river and stream pesticide impairments have been identified in the Cottonwood River Watershed. The MDA will continue to monitor the Cottonwood River and Sleepy Eye Creek into the future to allow for analysis of pesticide detections over time.

Finally, the MDA completed 10 pesticide water quality sample collection events from 5 wetlands within the Cottonwood and Redwood River watersheds in 2014. No pesticide detections in the wetlands in either watershed were above the applicable water quality reference values.

8. Implementation Strategy Summary

8.1 Implementation Framework

The strategies described in this section will be used in the 1W1P process to determine prioritized and targeted actions to reduce TSS, *E. coli*, and nutrient loads (TP) in the Cottonwood River Watershed. These actions are further developed in a separate, more detailed WRAPS report.

8.2 Permitted Sources

8.2.1 Construction Stormwater

The WLA for stormwater discharges from sites where there is construction activity reflects the number of construction sites greater than one acre expected to be active in the watershed at any one time, and the BMPs and other stormwater control measures that should be implemented at the sites to limit the discharge of pollutants of concern. The BMPs and other stormwater control measures that should be implemented at construction sites are defined in Minnesota's NPDES/SDS General Stormwater Permit for Construction Activity (MNR100001). If a construction site owner/operator obtains coverage under the NPDES/SDS General Stormwater Permit and properly selects, installs, and maintains all BMPs required under the permit, including those related to impaired waters discharges and any applicable additional requirements found in Section 23 of the Construction Stormwater General Permit, the stormwater discharges would be expected to be consistent with the WLA in this TMDL. Construction activity must also meet all local government construction stormwater requirements.

8.2.2 Industrial Stormwater

The WLA for stormwater discharges from sites where there is industrial activity reflects the number of sites in the watershed for which NPDES Industrial Stormwater Permit coverage is required, and the BMPs and other stormwater control measures that should be implemented at the sites to limit the discharge of pollutants of concern. Minnesota's NPDES/SDS Industrial Stormwater Multi-Sector General Permit (MNR050000) and NPDES/SDS Nonmetallic Mining/Associated Activities General Permit (MNG490000) establish benchmark concentrations for pollutants in industrial stormwater discharges. If a facility owner/operator obtains stormwater coverage under the appropriate NPDES/SDS Permit and properly selects, installs, and maintains BMPs sufficient to meet the benchmark values in the permit, the stormwater discharges would be expected to be consistent with the WLA in this TMDL report. Industrial activity must also meet all local government stormwater requirements.

8.2.3 MS4 Stormwater

The City of Marshall should continue to treat its stormwater to the maximum extent practicable, even though no reductions are required to meet the assigned TSS WLAs. Information on stormwater BMPs can be found in the [Minnesota Stormwater Manual](#). This resource includes links to specific urban BMP strategies, studies, calculators, special considerations for Minnesota, as well as links regarding industrial and stormwater programs. LGUs participated in the Cottonwood River WRAPS development and identified strategies that could be implemented.

For the purposes of this TMDL, the baseline year for implementation will be the mid-range year of the data years used for the lake response modeling (Table 46) and development of the TSS and *E. coli* LDCs. Since the TSS and *E. coli* LDCs were developed using the watershed HSPF models, the baseline year will coincide with the mid-range year of the HSPF model simulations. The rationale for developing a baseline year is that projects undertaken recently may take a few years to influence water quality. Any wasteload-reducing BMP implemented since the baseline year will be eligible to “count” toward an MS4’s load reductions. If a BMP was implemented during or just prior to the baseline year, the MPCA is open to presentation of evidence by the MS4 Permit holder to demonstrate that it should be considered as a credit. The WRAPS report for the Cottonwood River Watershed was developed with input from the stakeholders to determine the appropriate BMPs and implementation strategies to meet the MS4 goals for all the TMDLs presented in this report.

Table 47. Implementation baseline years in the Cottonwood River Watershed.

Impairment	Data Years Used for TMDL Development	Baseline Year
TSS Impairments (HSPF)	2008 through 2017	2012
<i>E. coli</i> Impairments (HSPF)	2008 through 2017	2012
Rock Lake	2002, 2007, 2017	2007
Bean Lake	2007, 2008, 2017	2008
Double Lake	2007, 2008, 2017, 2018	2017
Clear Lake	2009, 2010, 2017	2010
Altermatt Lake	2009, 2010	2010
Boise Lake	2011, 2012	2012
Bachelor Lake	2011, 2012	2012

8.2.4 Wastewater

The MPCA issues permits for WWTPs that discharge into waters of the state. The permits have site specific limits that are based on water quality standards. Permits regulate discharges with the goals of protecting public health and aquatic life and assuring that every facility treats wastewater. In addition, SDS Permits set limits and establish controls for land application of sewage. For TSS and *E. coli*, WWTPs discharging into impaired reaches did not require any changes to their discharge permit limits due to the WLAs calculated in this TMDL. No WWTPs discharge to the impaired lakes addressed in this TMDL report.

8.3 Nonpermitted Sources

Implementation of the Cottonwood River Watershed TMDL will require BMPs that address the numerous pollutants in the watershed. This section provides an overview of example BMPs that may be used for implementation. The BMPs included in this section are not exhaustive, and the list may be amended after the development of future watershed plans and studies. Other reports and studies have evaluated implementation strategies in the Cottonwood River Watershed, such as the Cottonwood River Fecal Coliform TMDL (RCRCA 2013), and the draft Cottonwood River Watershed SID Report (MPCA, available upon request).

Agricultural sources such as livestock and runoff from cropland, human wastewater sources such as ITPHS septic systems, near-channel sources of sediment, and internal lake phosphorus loading were

identified as high priority pollutant sources. Though developed areas within the Cottonwood River Watershed are small, urban stormwater runoff can contribute to localized pollutant loading. Urban runoff is a high priority pollutant source.

8.3.1 Agricultural Sources

Several different agricultural BMPs can be used to target priority sources and their associated pollutants. Table 47 provides a summary of agricultural BMPs, their NRCS code, and their targeted pollutants. Descriptions of each BMP are provided below. More information on agricultural BMPs in the state of Minnesota can be found in the Agricultural BMP Handbook for Minnesota (Lenhart et al. 2017).

Table 48. Summary of agricultural BMPs for agricultural sources and their primary targeted pollutants.

BMP (NRCS standard)	Targeted pollutant(s)		
	Phosphorus	TSS	<i>E. coli</i>
Conservation cover (327)	X	X	
Conservation/reduced tillage (329 & 345)	X	X	
Cover crops (340)	X	X	
Filter strips (636)	X	X	X
Riparian buffers (390)	X	X	X
Clean water diversion (362)	X		X
Access control/fencing (472 & 382)	X	X	X
Waste storage facilities (313) and nutrient management (590)	X		X
Drainage water management (554)	X	X	
Alternative tile intakes (606)	X	X	X
Grassed waterways (412)	X	X	
Water and sediment control basins (638)	X	X	
Wetland restorations (657)	X	X	X

Conservation Cover (327), Conservation/Reduced Tillage (329 and 345), and Cover Crops (340)

Conservation cover, conservation/reduced tillage, and cover crops are all on-field agricultural BMPs that aim to reduce erosion and nutrient loss by increasing and/or maintaining vegetative cover and root structure. Conservation cover is the process of converting previously row crop agricultural fields to permanent perennial vegetation. Conservation or reduced tillage can mean any tillage practice that leaves additional residue on the soil surface; 30% or more cover is typically considered conservation tillage. In addition to reducing erosion, conservation tillage preserves soil moisture. Cover crops refer to “the use of grasses, legumes, and forbs planted with annual cash crops to provide seasonal soil cover on cropland when the soil would otherwise be bare” (Lenhart et al. 2017).

Filter Strips (636) and Riparian Buffers (390)

Feedlot/wastewater filter strips are defined as “a strip or area of vegetation that receive and reduce sediment, nutrients, and pathogens in discharge from a settling basin or the feedlot itself.” (Lenhart et al. 2017). Riparian buffers are composed of a mix of grasses, forbs, sedges, and other vegetation that serve as an intermediate zone between upland and aquatic environments (Lenhart et al. 2017). The vegetation is tolerant of intermittent flooding and/or saturated soils that are prone to occur in intermediate zones.

Riparian buffers and filter strips that include perennial vegetation and trees can filter runoff from adjacent cropland, provide shade and habitat for wildlife, and reinforce streambanks to minimize erosion. The root structure of the vegetation uses enhanced infiltration of runoff and subsequent trapping of pollutants. Both, however, are only effective in this manner when the runoff enters the BMP as a slow moving, shallow “sheet”; concentrated flow in a ditch or gully will quickly pass through the vegetation offering minimal opportunity for retention and uptake of pollutants. Similarly, tile lines can often allow water to bypass a buffer or filter strip, thus reducing their effectiveness.

Clean Water Diversions (362)

Clean runoff water diversion “involves a channel constructed across the slope to prevent rainwater from entering the feedlot area or the farmstead to reduce water pollution” (Lenhart et al. 2017). Clean water diversions can take many forms including roof runoff management, grading, earthen berms, and other barriers that direct uncontaminated runoff from areas that may contain high levels of *E. coli* and nutrients.

Access Control/Fencing (472 and 382)

Fencing can be used with controlled stream crossings to allow livestock to cross a stream while minimizing disturbance to the stream channel and streambanks. Providing alternative water supplies for livestock allows animals to access drinking water away from the stream, thereby minimizing the impacts to the stream and riparian corridor. Some researchers have studied the impacts of providing alternative watering sites without structural exclusions and found that cattle spend 90% less time in the stream when alternative drinking water is furnished (EPA 2003).

Waste Storage Facilities (313) and Nutrient Management (590)

Manure management strategies depend on a variety of factors. A pasture or open lot system with a relatively low density of animals (one to two head of cattle per acre [EPA 2003]) may not produce manure in quantities that require management for the protection of water quality. For mid-size and large facilities, additional waste storage is needed. A waste storage facility is “an impoundment created by excavating earth or a structure constructed to hold and provide treatment to agricultural waste” (Lenhart et al. 2017). Waste storage facilities hold and treat waste directly from animal operations, process wastewater, or contaminated runoff.

Confined swine operations typically use liquid manure storage areas that are located under the confinement barn. Wash water used to clean the floors and remove manure buildup combines with the solid manure to form a liquid or slurry in the pit. The mixture is usually land applied in the spring and fall by injection/incorporation into the soil or transported offsite. Some facilities may have “open-air” liquid manure storage areas, which can pose a runoff risk if improperly managed.

Nonpermitted large dairies in the Cottonwood River Watershed mainly store and handle manure in liquid form to be land-applied at a later date. Other potential sources of wastewater include process wastewater such as parlor wash down water, milk-house wastewater, silage leachate, and runoff from outdoor silage feed storage areas. There are potential runoff problems associated with these wastewater sources if not properly managed. In addition, many small dairy operations have limited to no manure storage. Most poultry manure is handled as a dry solid in the state; liquid poultry manure handling and storage is rare. Improperly stockpiled poultry manure or improper land application can

pose runoff issues. Final disposal of waste usually involves land application on the farm or transportation to another site.

The MDA recommends that inorganic and organic (manure) fertilizer application follow the “4Rs” of nutrient management by optimizing application rate (Right rate), application timing (Right timing), source of nutrient (Right source), and placement of the application (Right placement). Manure is typically applied to the land once or twice per year. To maximize the amount of nutrients and organic material retained in the soil, application should not occur on frozen ground or when precipitation is forecast during the next several days.

Drainage water management (554)

Drainage water management, or controlled drainage, is a BMP in which a water control structure such as stop logs or floating mechanisms are placed at or near the outlet of a drainage system to manage the water table beneath an agricultural field. Storing excess water through the use of a controlled drainage system reduces the volume of agricultural drainage flow to surface water and the nutrients and sediment it carries.

Alternative tile intakes (606)

This BMP replaces open intakes that are flush with the ground surface that provide a direct conduit for sediment and nutrients to enter the tile system. Alternative options include perforated riser pipes, gravel/rock inlets, dense pattern tile and vegetated buffers surrounding the inlet. These alternatives increase sediment trapping efficiency and reduce the velocity of flow into the inlet.

Grassed Waterways (412) and Water and Sediment Control Basins (638)

Grassed waterways and water and sediment control basins (WASCOBs) are both agricultural BMPs that aim to slow water flow off agricultural fields. Grassed waterways are areas of vegetative cover that are placed in line with high flow areas on a field. WASCOBs are vegetative embankments that are placed perpendicular to water’s flow path to pool and slowly release water. Both practices reduce erosion and sediment and phosphorus loss from agricultural fields.

Wetland Restoration (657)

Wetland restoration refers to the restoration of former or degraded wetlands to the hydrological, vegetative, and soil conditions that existed before modification from activities such as farming or draining. Wetlands are natural storage features that slow and filter water, reducing downstream flooding events. Wetland restoration can reduce fecal bacteria, nutrient, and sediment loading to nearby waterways in addition to providing habitat for plants and wildlife (Lenhart et al. 2017).

8.3.2 Stormwater Runoff

Implementation strategies to address urban stormwater management are detailed in the [Minnesota Stormwater Manual](#). Practices can be construction-related, post-construction, pre-treatment, nonstructural, and structural. Implementation in the more urban areas will likely require retrofits, while practices in the more rural residential areas can target open areas and runoff from lawns and impervious surfaces associated with development.

8.3.3 Subsurface Sewage Treatment Systems

SSTS Assessments

State-sponsored funding programs are available for community-wide septic system assessments. The Public Facilities Authority (PFA) administers the Small Community Wastewater Treatment Program, which provides grants of up to \$60,000 to LGUs to “conduct preliminary site evaluations and prepare feasibility reports, provide advice on possible SSTS alternatives, and help develop the technical, managerial, and financial capacity to build, operate, and maintain SSTS systems” ([PFA website](#)). These studies assess current SSTS compliance status as well as potential future individual and/or community SSTS solutions.

Also, BWSR has provided grant funds in the past to local governments for large-scale SSTS compliance inspection projects. These projects typically involve riparian communities on impaired water bodies.

SSTS Upgrades/Replacement

When a straight pipe system or other ITPHS location is confirmed, the local SSTS LGU will send a Notice of Noncompliance to the owner that includes a replacement or repair timeline. State rules mandate a 10-month deadline for the system to be brought into compliance, but an LGU can choose to set a more restrictive timeline. The reductions in loading resulting from upgrading or replacing failing systems in the watershed depend on the level of failure present in the watershed.

An SSTS doesn't need to be a straight pipe or other ITPHS to be a threat to surface water quality. Leaking tanks or a drainfield without adequate separation from groundwater can result in the transport of pathogens or excess nutrients to nearby surface waters through the groundwater. This is of particular concern for water-front properties. Shoreland rules in every county require proof of a compliant SSTS prior to issuance of a building permit for dwelling additions or rebuilds, and most County-level SSTS LGU also require proof of a compliant SSTS for property transfers.

Many counties and SWCDs offer low interest loan programs for SSTS upgrades or replacement. The PFA Small Community Wastewater Program offers grant and loan packages of up to \$2,000,000 for the construction of publicly owned community SSTS.

SSTS Maintenance

The most cost-effective BMP for managing loads from SSTSs is regular maintenance. The EPA recommends that septic tanks be pumped every three to five years depending on the tank size and number of residents in the household (EPA 2002b). When not maintained properly, SSTSs can cause the release of pathogens and excess nutrients into surface water. Annual inspections, in addition to regular maintenance, ensure that systems function properly. Compliance with state and county code is essential to reducing *E. coli* and phosphorus loading from SSTSs. SSTSs are regulated under Minn. Stat. §§ 115.55 and 115.56. Counties must enforce ordinances in Minn. R. ch. 7080 to 7083.

Public Education

Education is another crucial component of reducing pollutant loading from SSTSs. Education can occur through public meetings, routine SSTS service provider home visits, mass mailings, and radio and television advertisements. An inspection program can also help with public education because inspectors can educate owners about proper operation and maintenance during inspections.

8.3.4 Near Channel Sources of Sediment

It is expected that implementation of the Sediment Reduction Strategy (MPCA 2015) for the Minnesota River Basin will reduce sediment in the Cottonwood River Watershed. Both direct and indirect controls for reducing near-channel sediment can be used in the Cottonwood River Watershed.

Direct Sediment Controls

Direct controls for near channel sediment sources include practices such as limiting ravine erosion with a drop structure or energy dissipater, or controlling streambank or bluff erosion through streambank stabilization and restoration. Streambank stabilization and restoration should be implemented to address eroding banks and areas of instability in stream channels. Activities should be focused in priority areas as defined by the LGUs.

The natural vegetation along stream corridors should be preserved. Buffers can mitigate pollutant loading associated with human disturbances and help to stabilize streambanks and improve infiltration. Minnesota's buffer law requires establishment of up to 50 feet of perennial vegetation along many rivers, streams, and ditches. Additional value could be added by working with landowners and residents to also install fencing or stream crossings to limit access to streams and ensuring enforcement of Minnesota's Shoreland Management Act.

Indirect Controls

Indirect controls for sediment loss typically involve land management practices and structural practices designed to temporarily store water or shift runoff patterns by increasing evapotranspiration at critical times of the year. The temporary storage of water and a shift in runoff patterns are needed to reduce peak flows and extend the length of storm hydrographs, which in turn will reduce the erosive power of streamflow on streambanks and bluffs.

8.3.5 Internal Loading in Lakes

Implementation strategies for internal TP load reduction include water level drawdown, sediment phosphorus immobilization or chemical treatment (e.g., alum), management of aquatic vegetation, and biomanipulation (e.g., carp management).

Sequencing of in-lake management strategies both relative to each other as well as relative to external load reduction is important to evaluate and consider. In general, external loading, if moderate to high, should be the initial priority for reduction efforts. Biomanipulation may also be an early priority. However, it is generally believed that further in-lake management efforts involving chemical treatment (e.g., alum) should follow after substantial progress has been made toward achieving external load reduction goals. The success of alum treatments depends on several factors including lake morphometry, water residence time, alum dose used, and presence/abundance of benthic-feeding fish (Huser et al. 2016).

The MPCA recommends feasibility studies for any lakes in which water level drawdown or chemical treatment is considered. [The Minnesota State and Regional Government Review of Internal Phosphorus Load Control](#) (MPCA 2020d) paper provides more information on internal phosphorus load BMPs and considerations.

8.4 Education

Education is a crucial component of reducing pollutant sources in the Cottonwood River Watershed and is important to increasing public buy-in of residents, businesses, and organizations. Education can occur through public meetings, mass mailings, radio and television advertisements, and other media.

8.5 Cost

TMDL reports are required to include an overall approximation of implementation costs (Minn. Stat. 2007, § 114D.25). It is estimated that the costs to implement the activities outlined in the strategy document are approximately \$207 million dollars over the next 20 years. This value is considered a rough estimate at this time, as there is a level of uncertainty in the generalized cost estimate numbers used here as well as in the source assessment and TMDL allocations presented in this report. The individual cost estimate exercises include: BMPs commonly implemented to address upland TSS and TP sources, livestock BMPs, ITPHS system repairs/replacements, and lake internal load projects. Required buffer installation, replacement of FTPGW systems, and SSTS maintenance are not included in the cost estimate at this time. Below is a general discussion of cost considerations for the three pollutants (TSS, bacteria, and phosphorus (lakes)) covered in this TMDL.

TSS

Utilizing estimates developed by an interagency work group (BWSR, USDA, MPCA, Minnesota Association of SWCDs, Minnesota Association of Watershed Districts, NRCS) who assessed restoration costs for several TMDLs, it was determined that implementing the Cottonwood River Watershed TSS TMDLs will cost approximately \$154 million over 20 years. This was based on total area of the watershed (1,314 square miles) multiplied by the cost estimate of \$117,000/square mile for a watershed-based treatment approach.

E. coli

The cost estimate for bacteria load reduction is based on unit costs for the two major sources of bacteria: livestock and ITPHS SSTSs. The unit cost for bringing AUs under MMPs and feedlot lot runoff controls is \$350/AU. This value is based on USDA EQIP payment history and includes buffers, livestock access control, MMPs, waste storage structures, and clean water diversions. Repair or replacement of ITPHS systems was estimated at \$20,000/system (Wenck, personal communication 2020). Multiplying those unit costs by an estimated 165 ITPHS systems and 168,537 AUs in the Cottonwood River Watershed provides a total cost of approximately \$62 million. However, the MPCA staff calculates that approximately 75% of these AUs currently have controls or management plans in place, thus reducing this estimate to approximately \$18 million.

Lake nutrients (phosphorus)

A detailed analysis of the cost to implement the nutrient TMDLs was not conducted. However, as a rough approximation one can use some general results from BMP cost studies across the United States. For example, an EPA summary of several studies showed a median life cycle cost of approximately \$2,200 per lb TP removed for watershed BMPs (Foraste et al. 2012). Another recent review (Macbeth et al. 2018) of lake restoration projects performed throughout the State of Minnesota suggests a median life cycle cost of approximately \$500 per lb of TP removed for internal load BMPs such as aluminum

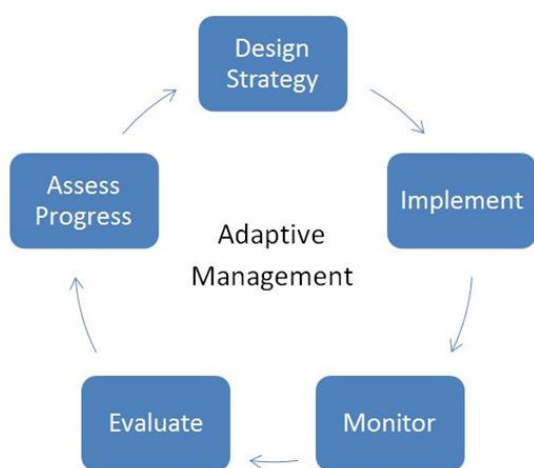
sulfate. Multiplying these rates by the needed watershed (3,196 lbs per year) and internal (10,165 lbs per year) TP reductions needed for the five lake basins included in this TMDL provides a total cost of approximately \$12 million. This cost estimate assumes a 20-year life cycle for watershed and internal load BMPs.

8.6 Adaptive Management

Adaptive management is an iterative implementation process that makes progress toward achieving water quality goals while using new data and information to reduce uncertainty and adjust implementation activities. The State of Minnesota has a unique opportunity to adaptively manage water resource plans and implementation activities every 10 years. This opportunity resulted from a voter-approved tax increase to improve state waters. The resulting interagency coordination effort is referred to as the Minnesota Water Quality Framework, which works to monitor and assess Minnesota’s major watersheds every 10 years. This Framework supports ongoing implementation and adaptive management of conservation activities and watershed-based local planning efforts, utilizing regulatory and nonregulatory means to achieve water quality standards.

Implementation of TMDL-related activities can take many years, and water quality benefits associated with these activities can also take many years. As the pollutant source dynamics within the watershed are better understood, implementation strategies and activities will be adjusted and refined to efficiently meet the TMDL and lay the groundwork for de-listing the impaired reaches and lakes. The water monitoring program outlined in Section 7 will be integral to the adaptive management approach, providing assurance that implementation measures are succeeding in achieving water quality standards. Adaptive management does not include changes to water quality standards or loading capacity. Any changes to water quality standards or loading capacity must be preceded by appropriate administrative processes, including public notice and an opportunity for public review and comment.

Figure 36. Adaptive management.



A list of implementation strategies in the WRAPS report prepared in conjunction with this TMDL focuses on adaptive management (Figure 36). Continued monitoring and “course corrections” responding to monitoring results are the most appropriate strategy for achieving the water quality goals established in this TMDL. Management activities will be changed or refined to efficiently meet the TMDLs and lay the groundwork for de-listing the impaired water bodies.

9. Public Participation

A stakeholder participation process was undertaken for this TMDL to obtain input from, review results with, and take comments from the general public and a LWG that consisted of staff from county environmental services departments, SWCDs, RCRCA, MPCA, DNR, BWSR, MDA, Minnesota Department of Health (MDH) and other interested and affected agencies. The LWG, led by RCRCA and MPCA staff, convened multiple times to discuss and review TMDL results and provide input and feedback on the development of the Cottonwood River WRAPS. The entire public stakeholder process involved meetings and other forms of communication as described in Table 48.

Table 49. Summary of stakeholder meetings/events held during the development of the Cottonwood TMDL/WRAPS.

Date	Description
4/19/2017	Local Work Group Meeting at Wabasso, MN
6/8/2017	Local Work Group Meeting at Marshall, MN
8/10/2017	Local Work Group Meeting at Marshall, MN
11/7/2017	Local Work Group Meeting at Marshall, MN
1/18/2018	Local Work Group Meeting at Marshall, MN
2/15/2018	Local Work Group Meeting at Marshall, MN
3/19/2018	Elected Officials Meeting at Lamberton, MN
4/19/2018	Local Work Group Meeting at Marshall, MN
6/28/2018	Local Work Group Meeting at Sleepy Eye, MN
7/19/2018	Public Informational Meeting at Sleepy Eye, MN
7/24/2018	Public Informational Meeting at Lake Benton, MN
7/25/2018	Public Informational Meeting at Marshall, MN
7/26/2018	Public Informational Meeting at Redwood Falls, MN
8/16/2018	Local Work Group Meeting at Lamberton, MN
9/20/2008	Local Work Group Meeting at Redwood Falls, MN
11/15/2018	Local Work Group Meeting at Marshall, MN
1/16/2019	Local Work Group Meeting at Marshall, MN
3/21/2019	Local Work Group Meeting at Wabasso, MN
5/16/2019	Local Work Group Meeting at Marshall, MN
7/18/2019	Local Work Group Meeting at Redwood Falls, MN
9/19/2019	Local Work Group Meeting at Wabasso, MN
12/19/2019	Local Work Group Meeting at Redwood Falls, MN
2/25/2020	Local Work Group Meeting at Redwood Falls, MN
5/21/2020	Local Work Group Meeting via WebEx
6/18/2020	Local Work Group Meeting via WebEx
8/27/2020	Local Work Group Meeting via WebEx
9/17/2020	Local Work Group Meeting via WebEx
12/10/2020	Local Work Group Meeting via WebEx
1/21/2021	Local Work Group Meeting via WebEx
3/18/2021	Local Work Group Meeting via WebEx
5/13/2021	Local Work Group Meeting via WebEx

Public notice

An opportunity for public comment on the draft TMDL was provided via a public notice in the State Register from October 10, 2022 through November 9, 2022. There were no comments received as a result of the public comment period.

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Supporting Items for Cottonwood River TSS and *E. coli* Impaired Reach (07020008-502)

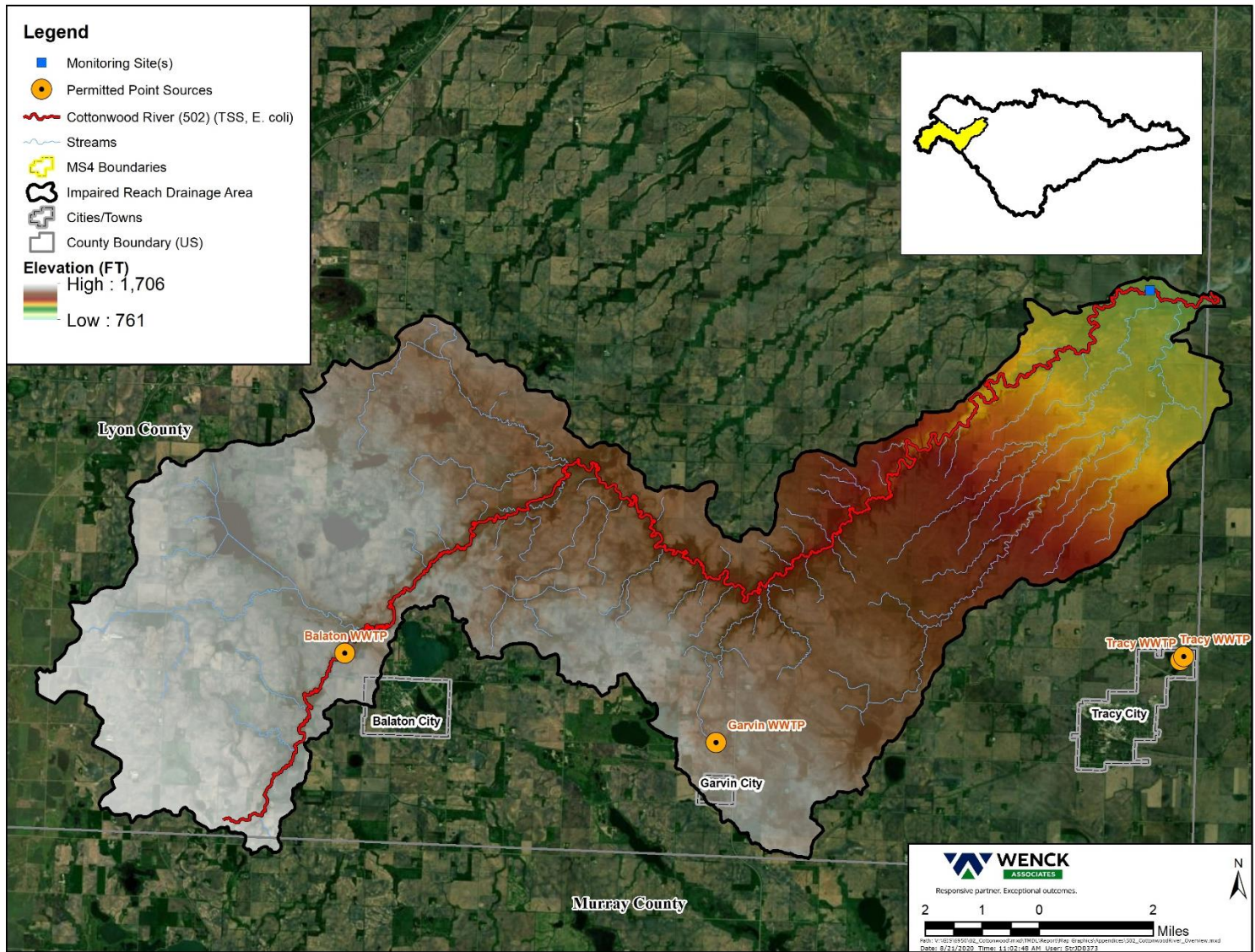


Figure A-1. Cottonwood River Reach 502 Overview.

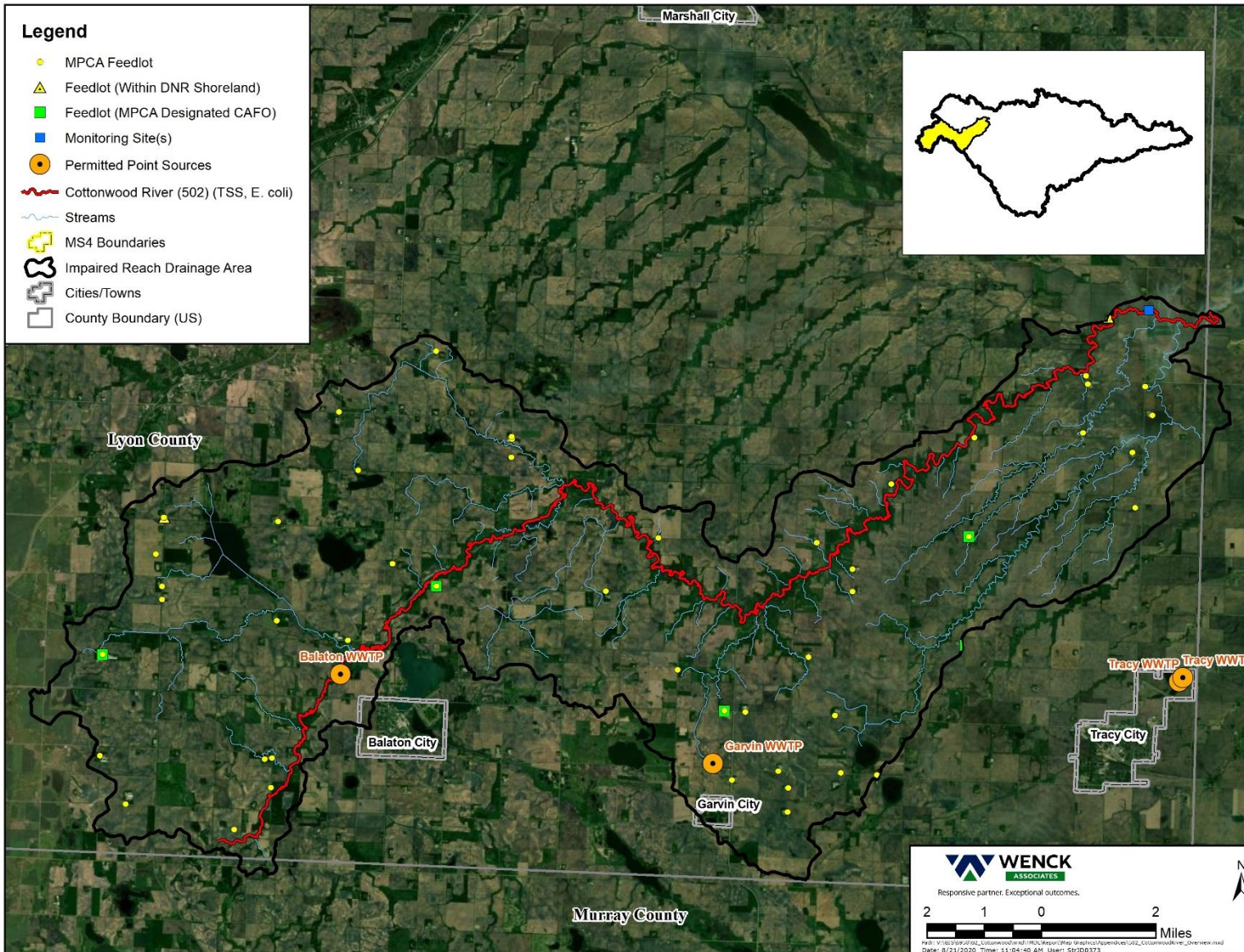


Figure A-2. Cottonwood River Reach 502 Feedlots.

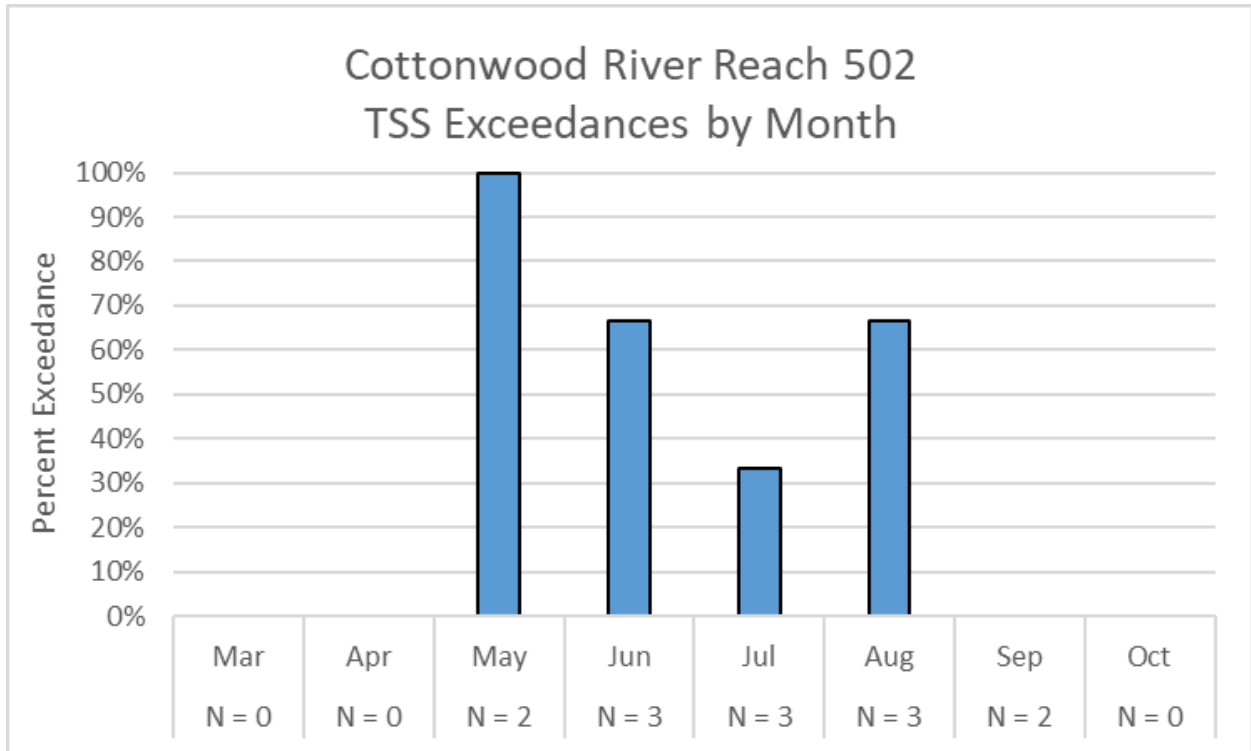


Figure A-3. Cottonwood River Reach 502 TSS Exceedances by Month.

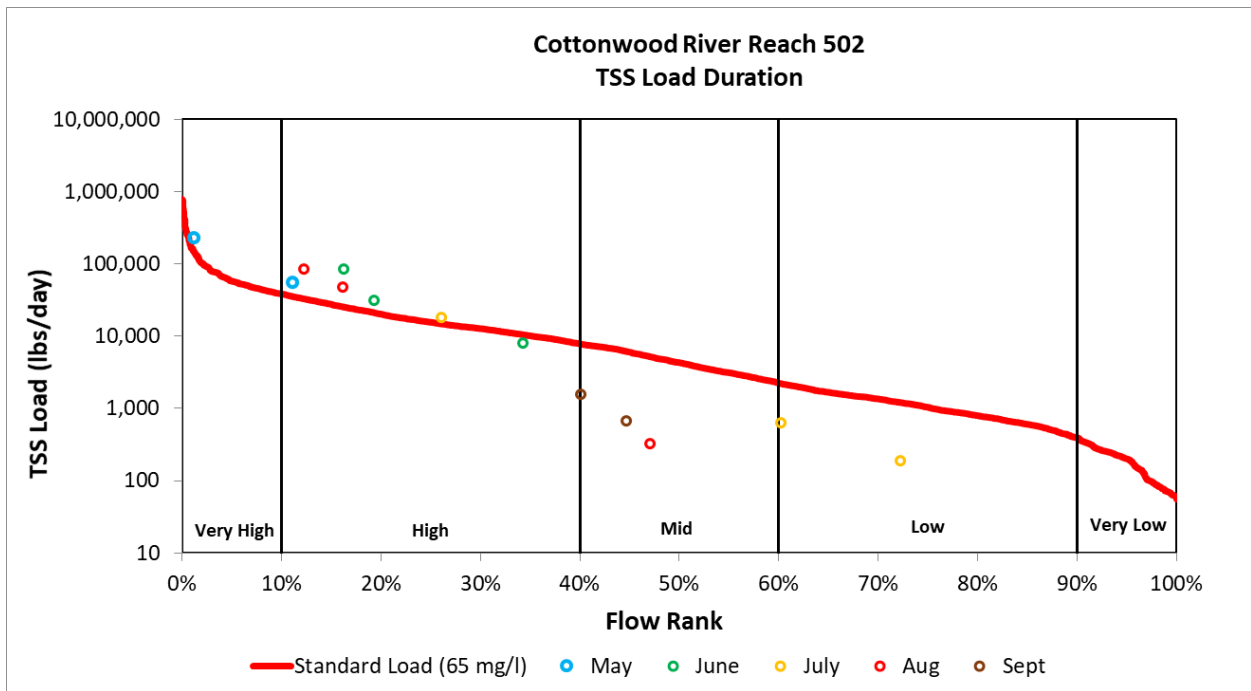


Figure A-4. Cottonwood River Reach 502 TSS Load Duration Curve (by month).

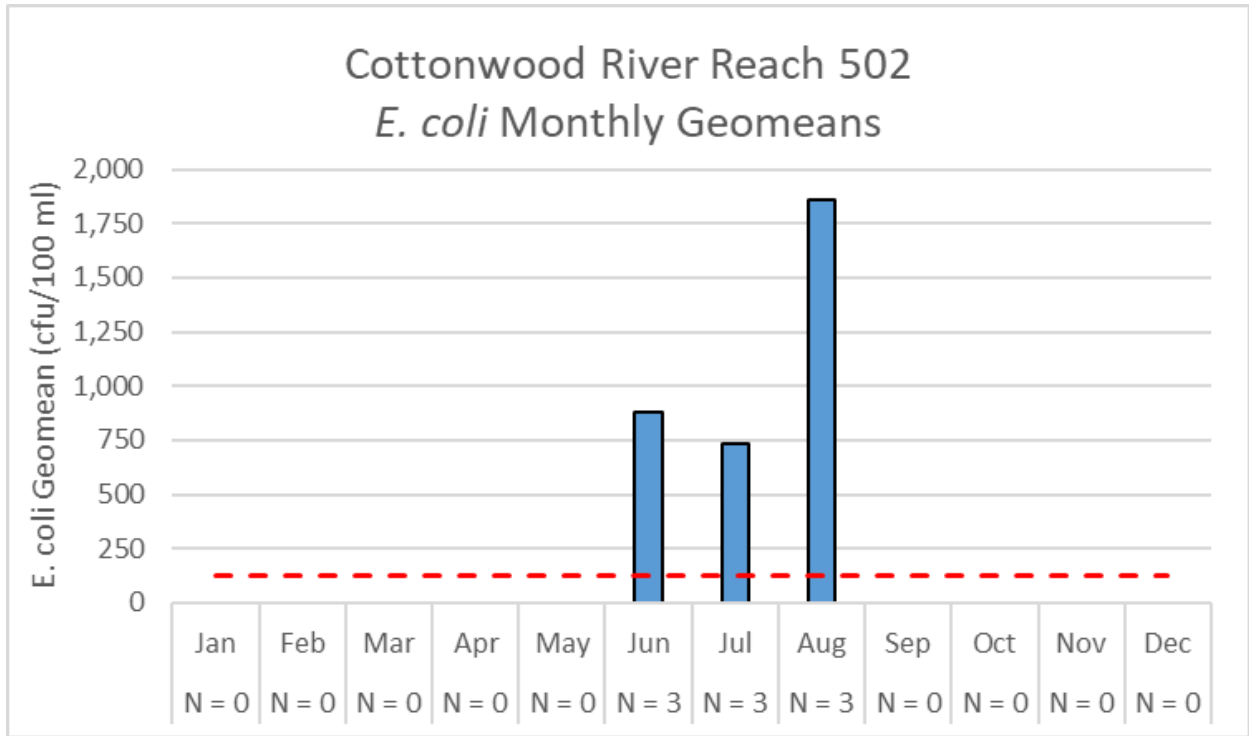


Figure A-5. Cottonwood River Reach 502 *E. coli* Monthly Geomeans.

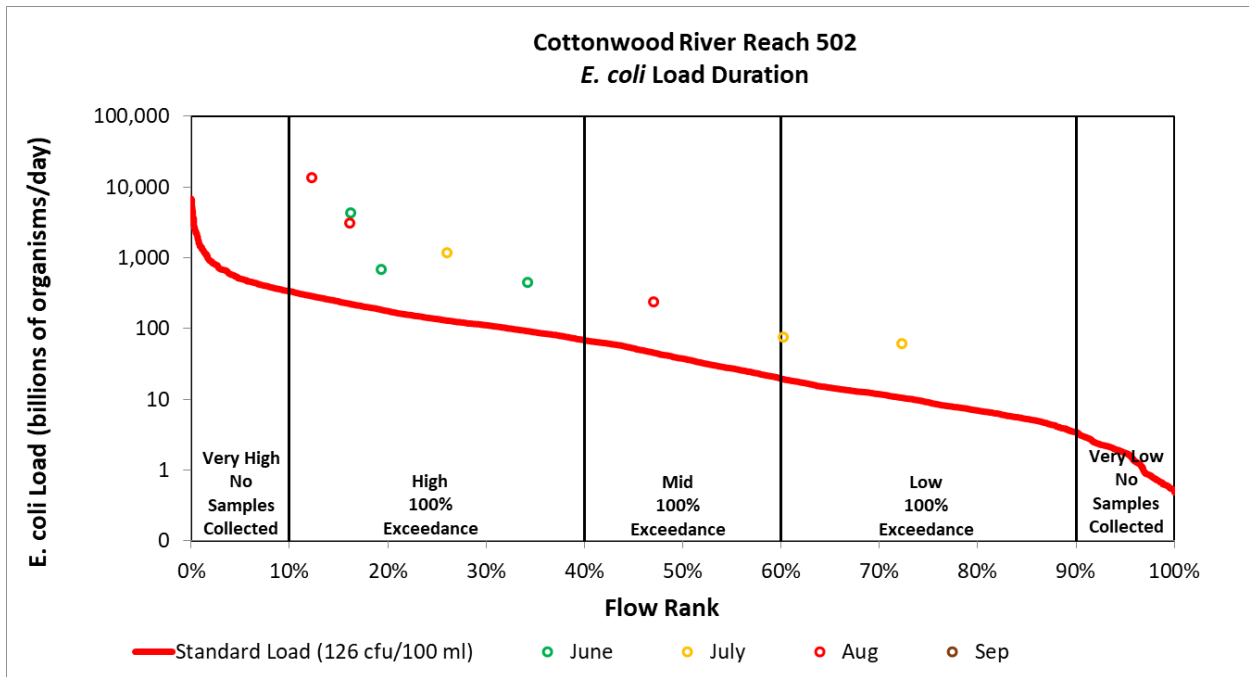


Figure A-6. Cottonwood River Reach 502 *E. coli* Load Duration Curve (by month).

Table A-1. Cottonwood River Reach 502 Bacteria Production Exercise.

Major Category	Source	Animal Units* or Individuals in Subwatershed	Fecal Bacteria Organisms Produced Per Unit Per Day	Total Fecal Bacteria Produced Per Day	Total Fecal Bacteria Produced Per Day by Major Category	Percent by Category
			[Billions of Org.] ⁸	[Billions of Org.]	[Billions of Org.]	
Livestock (Surface Applied Manure) ¹	Horse*	-	-	-	857,147	99.85%
	Swine*	10,045	32.7	328,462		
	Bovine*	8,949	58.2	520,849		
	Poultry*	243.0	20.5	4,982		
	Other Livestock*, ⁹	87	32.7	2,855		
Wildlife	Deer ³	502	0.5	251	854	0.10%
	Waterfowl ⁴	1,506	0.4	603		
Human	Failing Septic Systems ⁵	9	5.7	53	53	0.01%
	WWTP effluent ⁶	2	0.1	0		
Domestic Animals ²	Improperly Managed Pet Waste ⁷	735	0.6	413	413	0.05%

* Values reported as Animal Units.

¹ Livestock animal units estimated based on MPCA registered feedlot database with animal units converted based on MN Dept. of Ag conversion units (<http://www.mda.state.mn.us/animals/feedlots/feedlot-dmt/feedlot-dmt-animal-units.aspx>).

² # of households in watershed multiplied by 0.58 dogs/ household and 0.73 cates/household according to the SE MN Regional TMDL (MPCA, 2002)

³ Assumes average deer density of .0078 deer/acre from Monitoring Population Trends of White-tailed Deer in Minnesota (Minnesota DNR, 2013)

⁴ Estimated from the MN DNR and US Fish & Wildlife Service 2018 Waterfowl Breeding Population Survey (Minnesota DNR, 2018)

⁵ based on county SSTS inventory failure rates reported to MPCA (MPCA personal communication, 2018) and rural population estimates (3 persons/ septic) based on 2010 Census blocks.

⁶ Reported as # of facilities with production based on WWTP effluent data from facility discharge monitoring reports (DMRs)

⁷ Estimated that 35% of the bacteria produced per month attributed to pet waste is improperly managed and available for runoff (CWP, 1999)

⁸ Derived from literature rates in Metcalf and Eddy (1991), Horsley and Witten (1996), Alderisio and De Luca (1999), ASAE Standards (1998) and the Southeast Minnesota Regional TMDL (MPCA, 2002). Values have been reported to two significant digits.

⁹ Other cattle include llama, goat, and sheep.

Supporting Items for Cottonwood River TSS Impaired Reach (07020008-504)

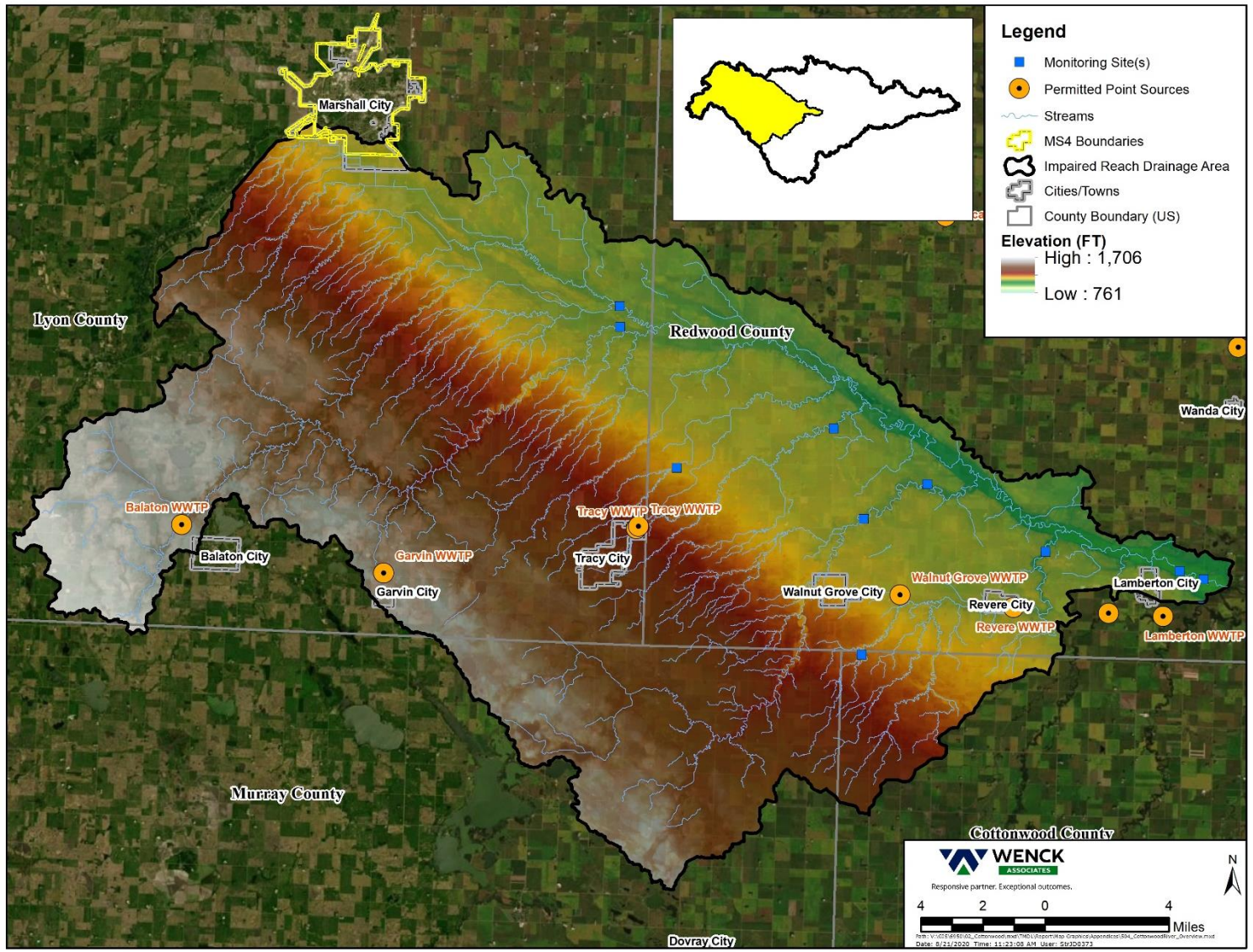


Figure A-7. Cottonwood River Reach 504 Overview.

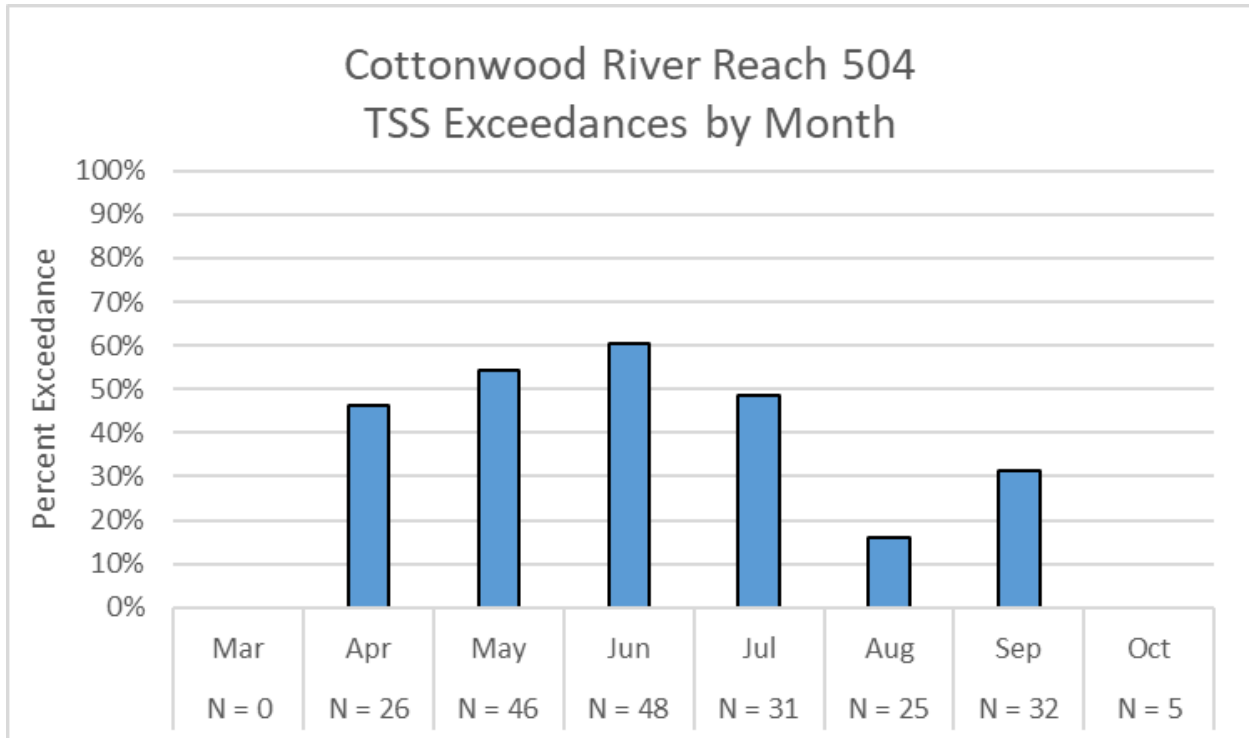


Figure A-8. Cottonwood River Reach 504 TSS Exceedances by Month.

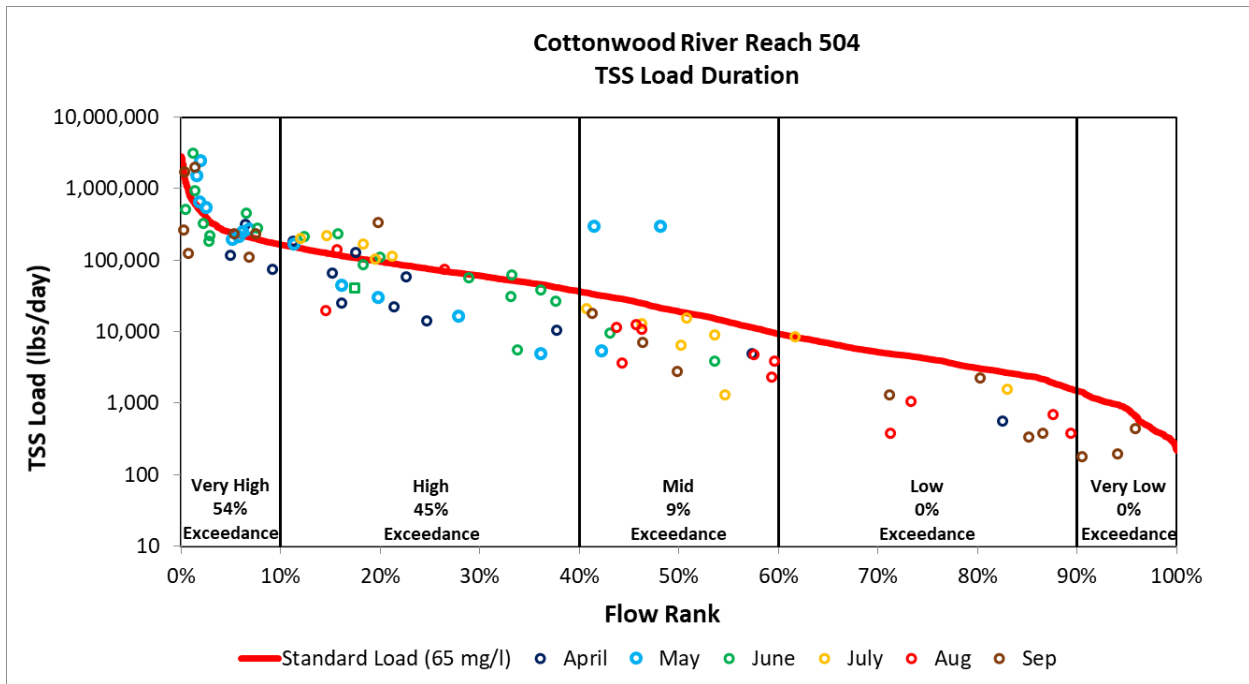


Figure A-9. Cottonwood River Reach 504 TSS Load Duration Curve (by month).

Supporting Items for Cottonwood River TSS Impaired Reach (07020008-508)

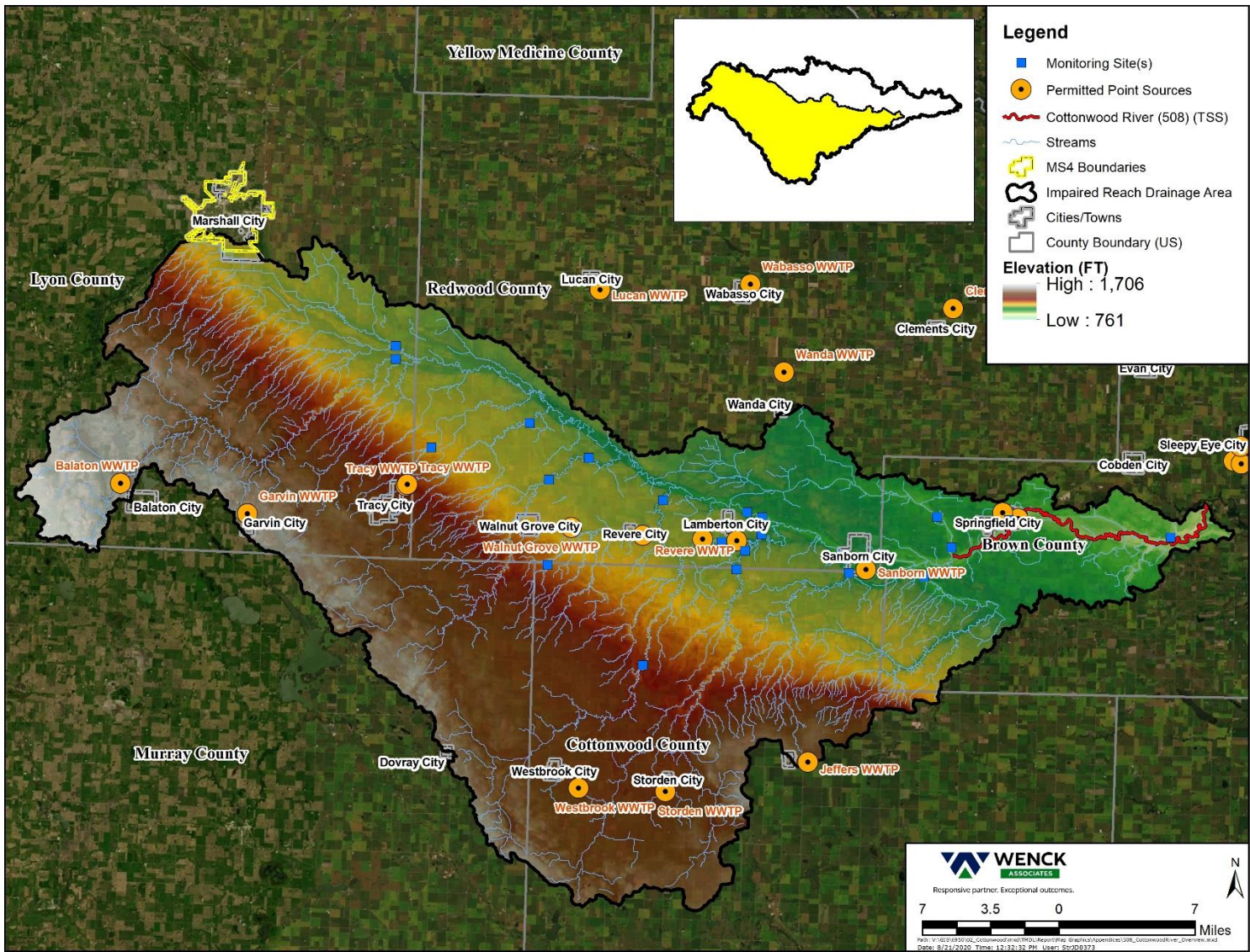


Figure A-10. Cottonwood River Reach 508 Overview.

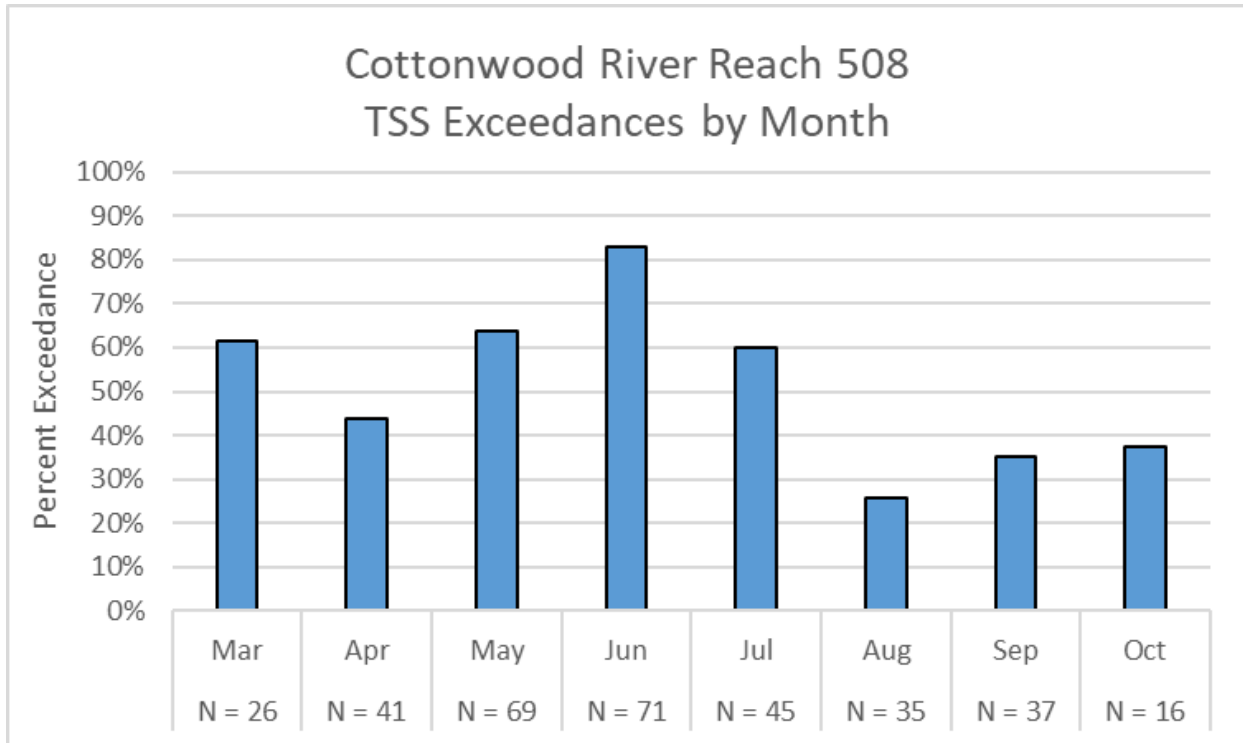


Figure A-11. Cottonwood River Reach 508 TSS Exceedances by Month.

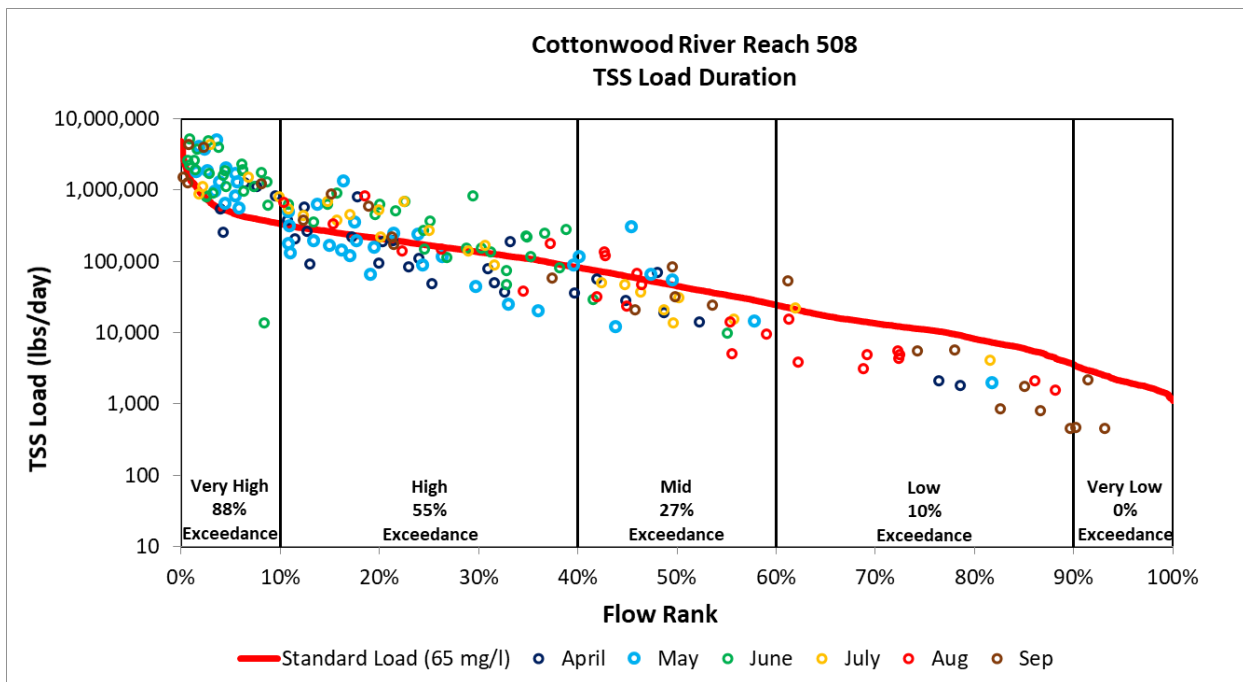


Figure A-12. Cottonwood River Reach 508 TSS Load Duration Curve (by month).

Supporting Items for Cottonwood River TSS Impaired Reach (07020008-509)

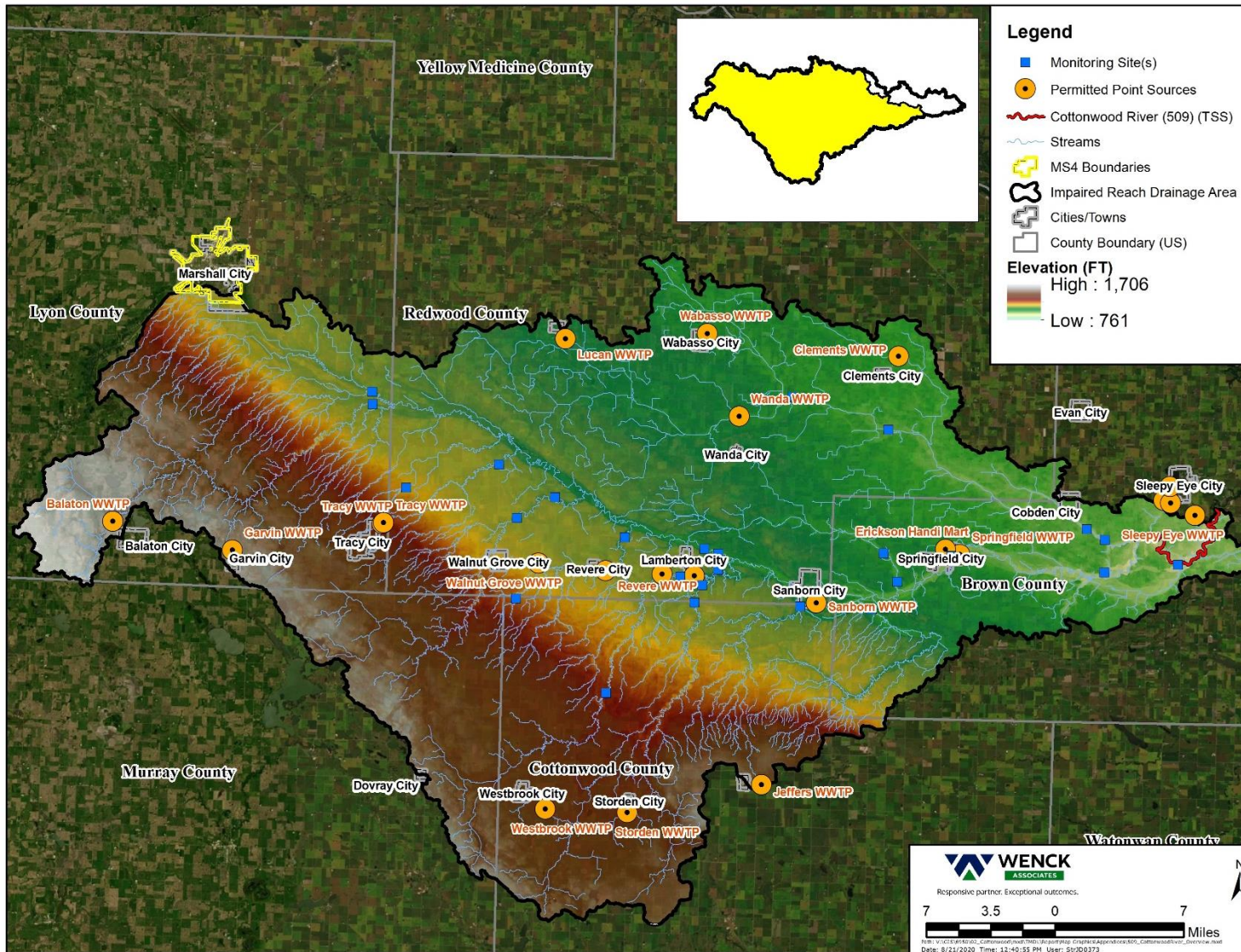


Figure A-13. Cottonwood River Reach 509 Overview.

Cottonwood River Reach 509 S-Tube Exceedances by Month

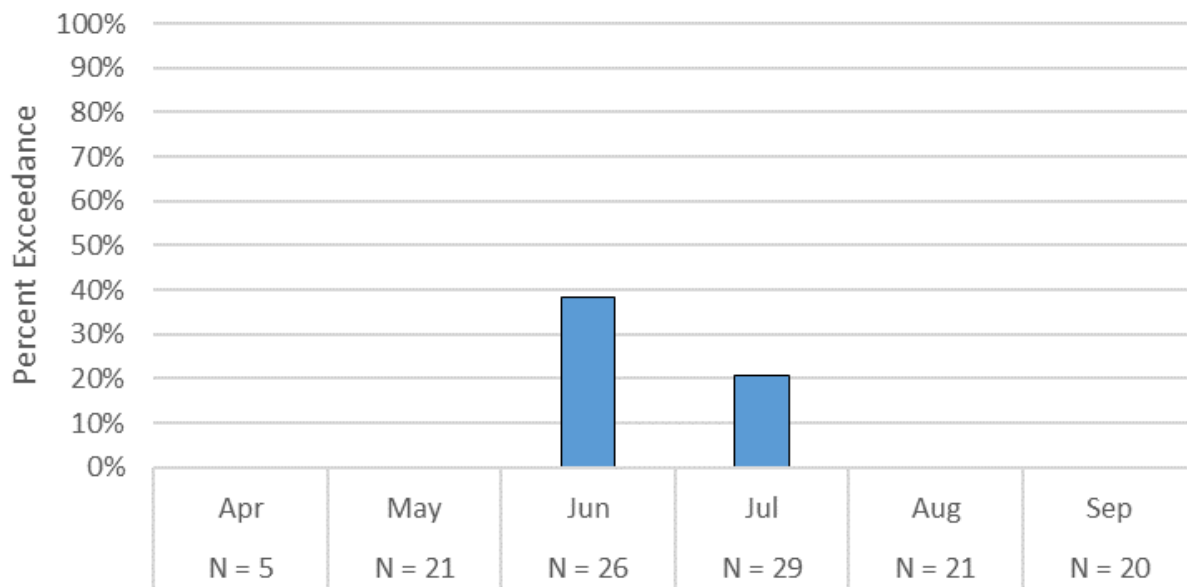


Figure A-14. Cottonwood River Reach 509 S-tube Exceedances by Month.

Note: No TSS data has been collected for this reach

Supporting Items for Judicial Ditch 30 Bacteria Impaired Reach (07020008-511)

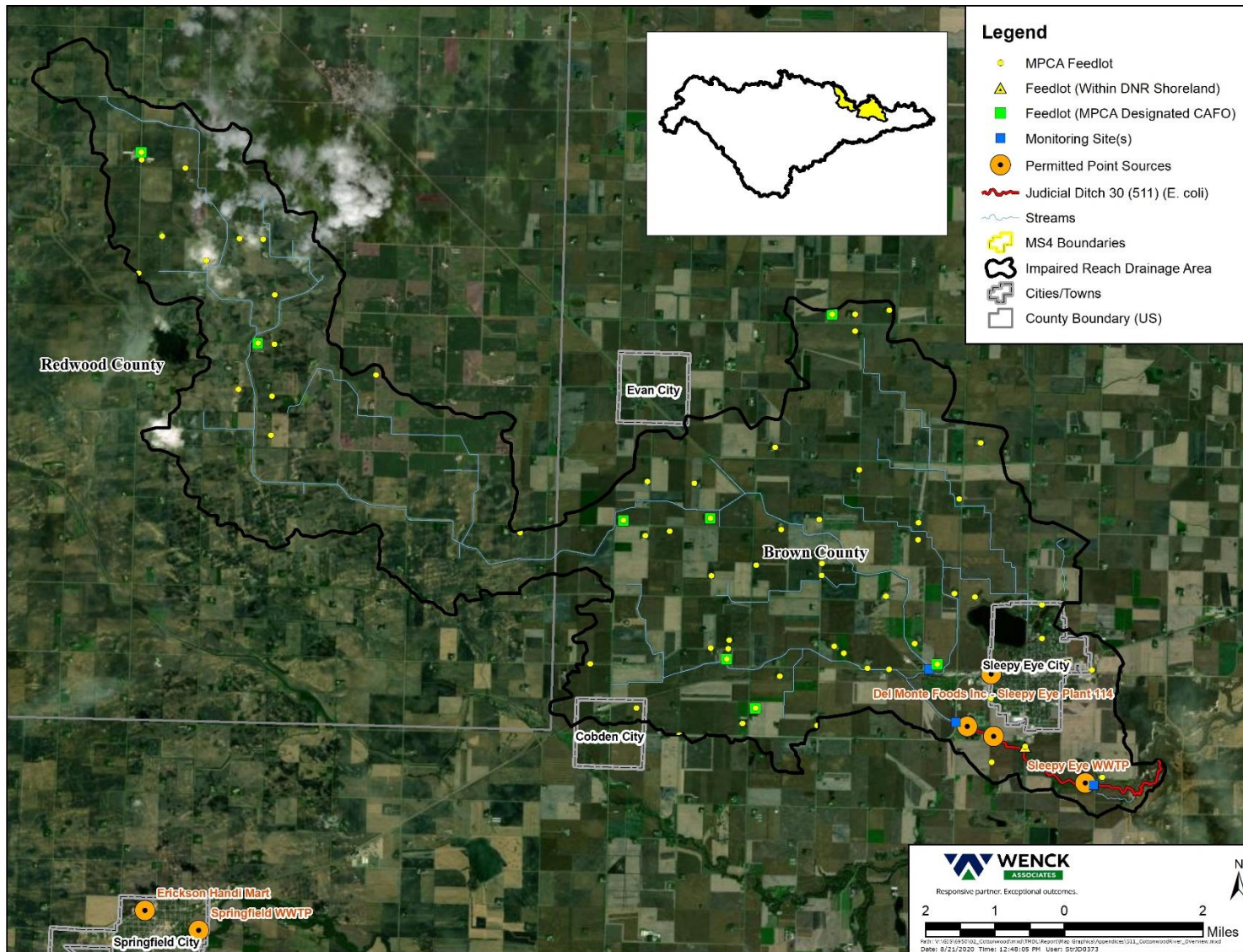


Figure A-15. Judicial Ditch 30 Bacteria Impaired Reach 511 Overview.

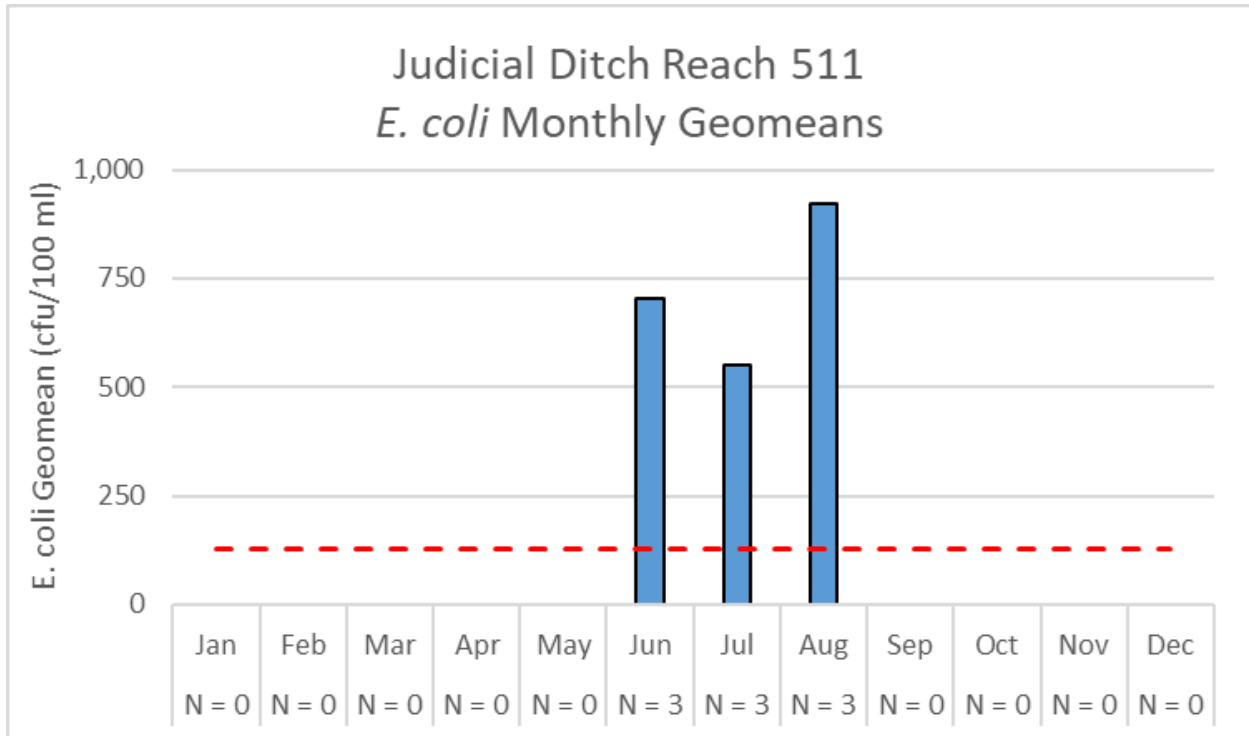


Figure A-16. Judicial Ditch 30 Reach 511 *E. coli* Monthly Geomeans.

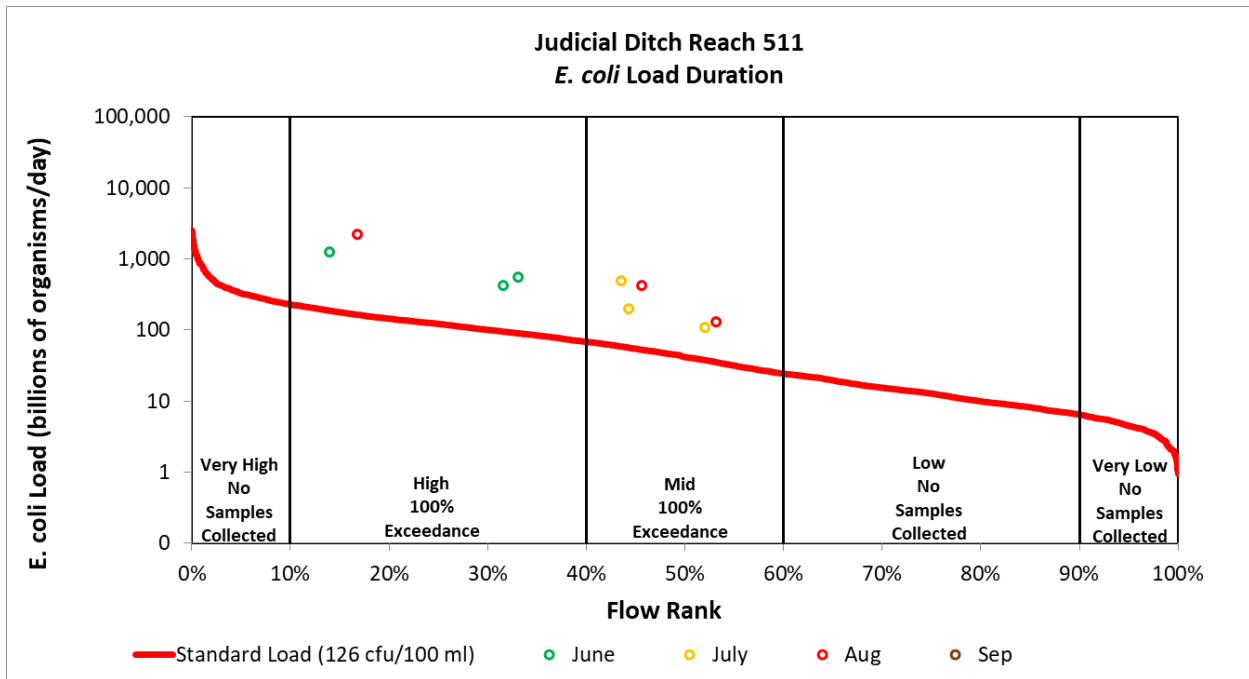


Figure A-17. Judicial Ditch 30 Reach 511 *E. coli* Load Duration Curve (by month).

Table A-2. Judicial Ditch Reach 511 Bacteria Production Exercise.

Major Category	Source	Animal Units* or Individuals in Subwatershed	Fecal Bacteria Organisms Produced Per Unit Per Day	Total Fecal Bacteria Produced Per Day	Total Fecal Bacteria Produced Per Day by Major Category	Percent by Category
			[Billions of Org.] ⁸	[Billions of Org.]	[Billions of Org.]	
Livestock (Surface Applied Manure) ¹	Horse*	12	58.2	698	477,767	99.79%
	Swine*	6,224	32.7	203,515		
	Bovine*	4,689	58.2	272,900		
	Poultry*	-	-	-		
	Other Livestock*, ⁹	20	32.7	654		
Wildlife	Deer ³	293	0.5	147	498	0.10%
	Waterfowl ⁴	879	0.4	352		
Human	Failing Septic Systems ⁵	31	5.7	177	179	0.04%
	WWTP effluent ⁶	1	2.2	2		
Domestic Animals ²	Improperly Managed Pet Waste ⁷	601	0.6	338	338	0.07%

* Values reported as Animal Units.

¹ Livestock animal units estimated based on MPCA registered feedlot database with animal units converted based on MN Dept. of Ag conversion units (<http://www.mda.state.mn.us/animals/feedlots/feedlot-dmt/feedlot-dmt-animal-units.aspx>).

² # of households in watershed multiplied by 0.58 dogs/ household and 0.73 cats/household according to the SE MN Regional TMDL (MPCA, 2002)

³ Assumes average deer density of .0078 deer/acre from Monitoring Population Trends of White-tailed Deer in Minnesota (Minnesota DNR, 2013)

⁴ Estimated from the MN DNR and US Fish & Wildlife Service 2018 Waterfowl Breeding Population Survey (Minnesota DNR, 2018)

⁵ based on county SSTS inventory failure rates reported to MPCA (MPCA personal communication, 2018) and rural population estimates (3 persons/ septic) based on 2010 Census blocks.

⁶ Reported as # of facilities with production based on WWTP effluent data from facility discharge monitoring reports (DMRs)

⁷ Estimated that 35% of the bacteria produced per month attributed to pet waste is improperly managed and available for runoff (CWP, 1999)

⁸ Derived from literature rates in Metcalf and Eddy (1991), Horsley and Witten (1996), Alderisio and De Luca (1999), ASAE Standards (1998) and the Southeast Minnesota Regional TMDL (MPCA, 2002). Values have been reported to two significant digits.

⁹ Other cattle include llama, goat, and sheep.

Supporting Items for Dutch Charley Creek TSS Impaired Reach (07020008-517)

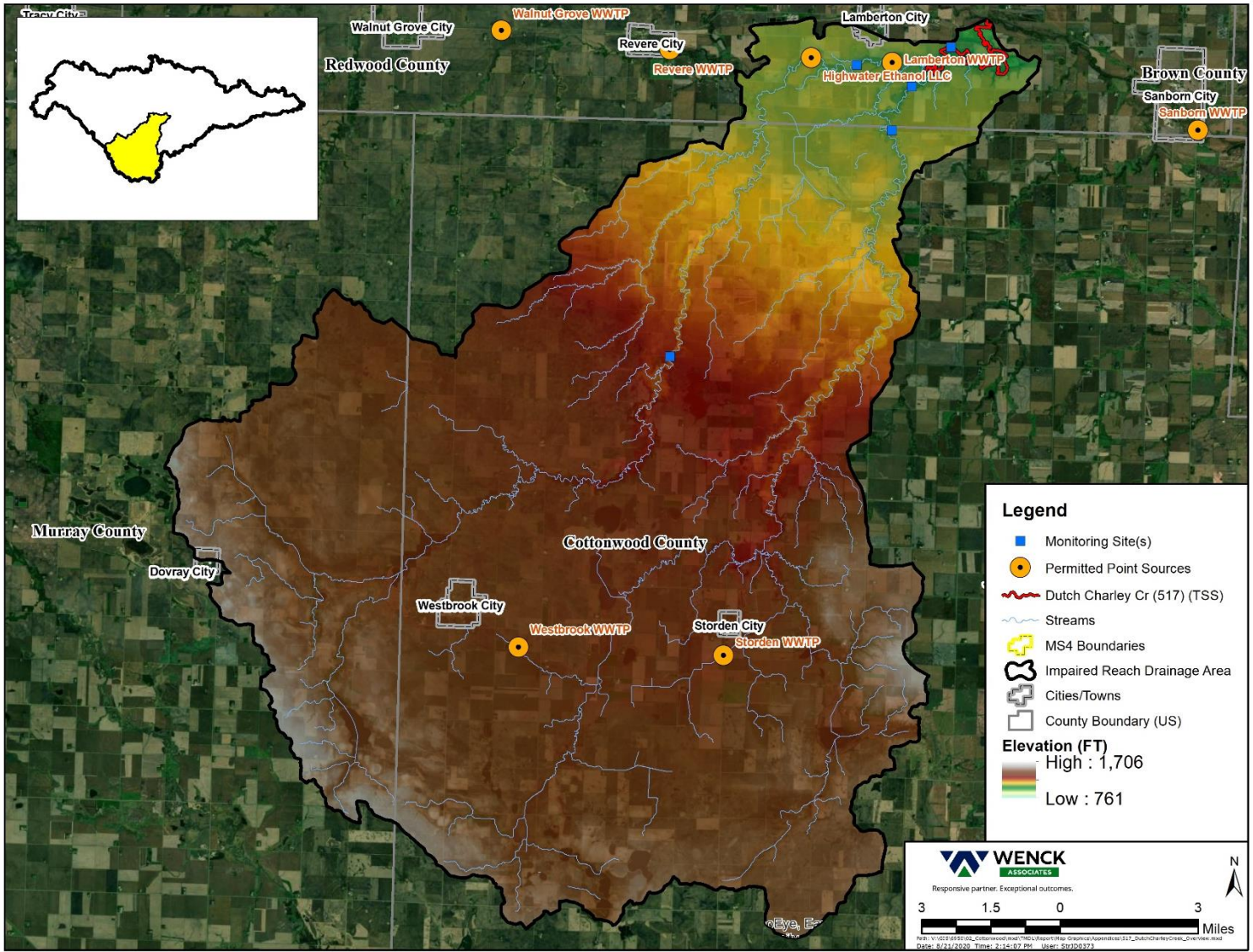


Figure A-18. Dutch Charley Creek Reach 517 Overview.

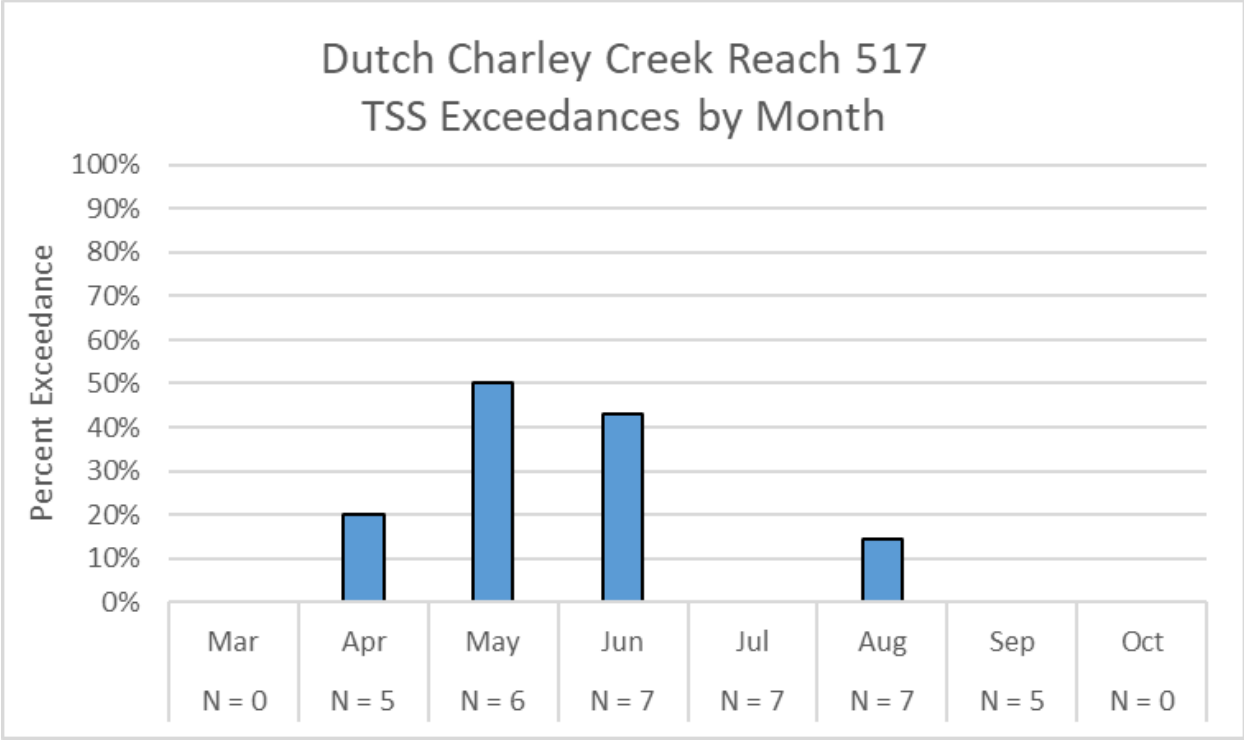


Figure A-19. Dutch Charley Reach 517 TSS Exceedances by Month.

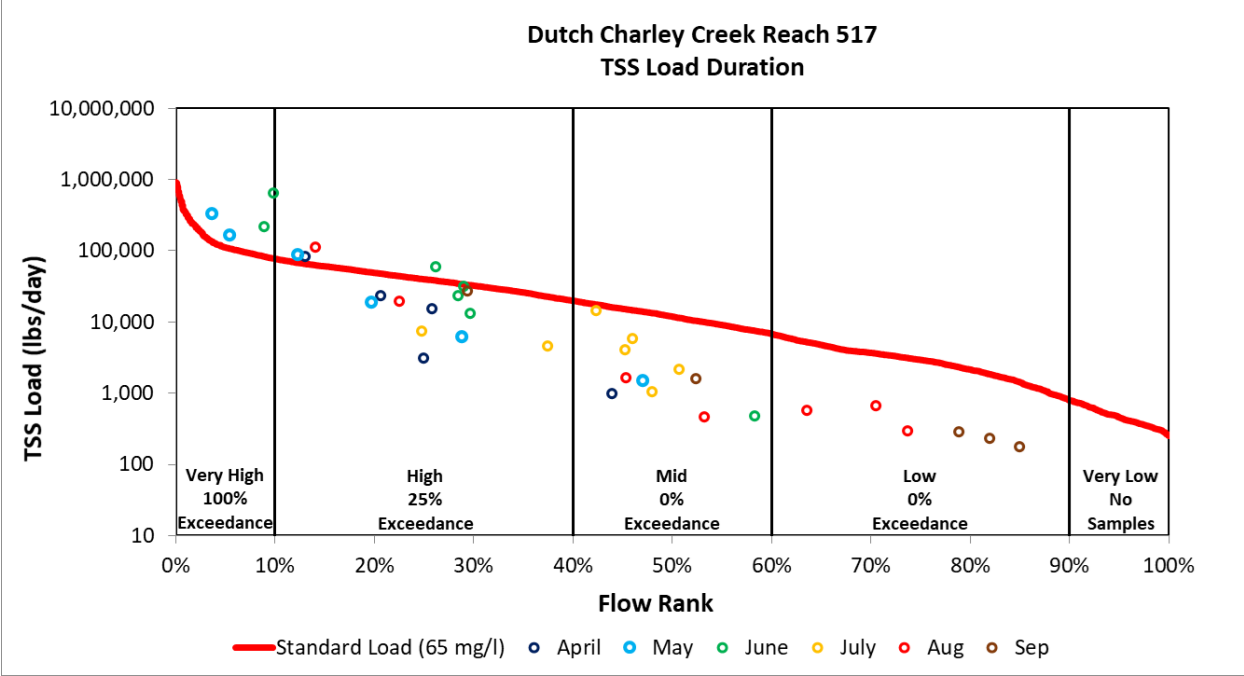


Figure A-20. Dutch Charley Reach 517 TSS Load Duration Curve (by month).

Supporting Items for Dutch Charley Creek TSS Impaired Reach (07020008-518)

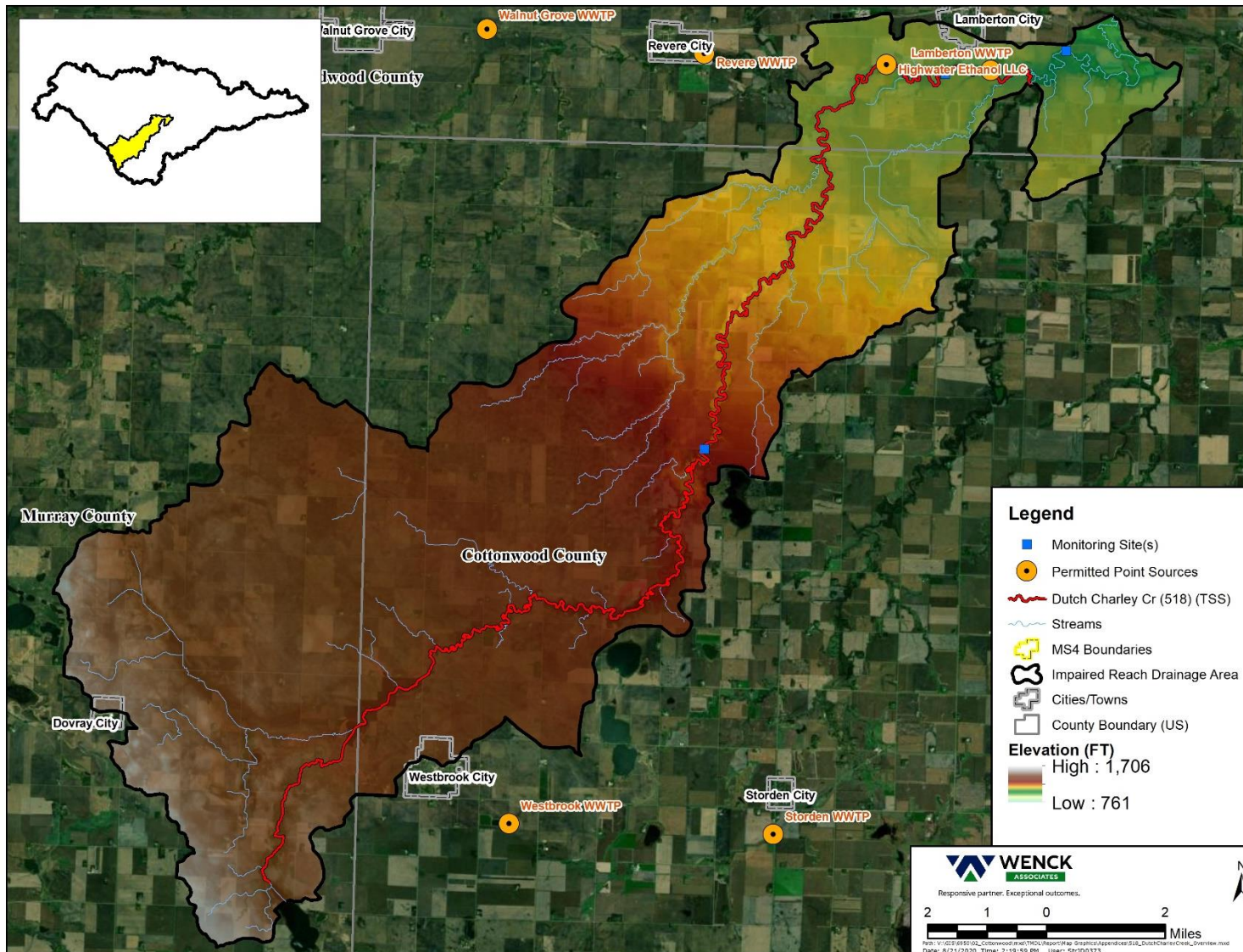


Figure A-21. Dutch Charley Reach 518 Overview.

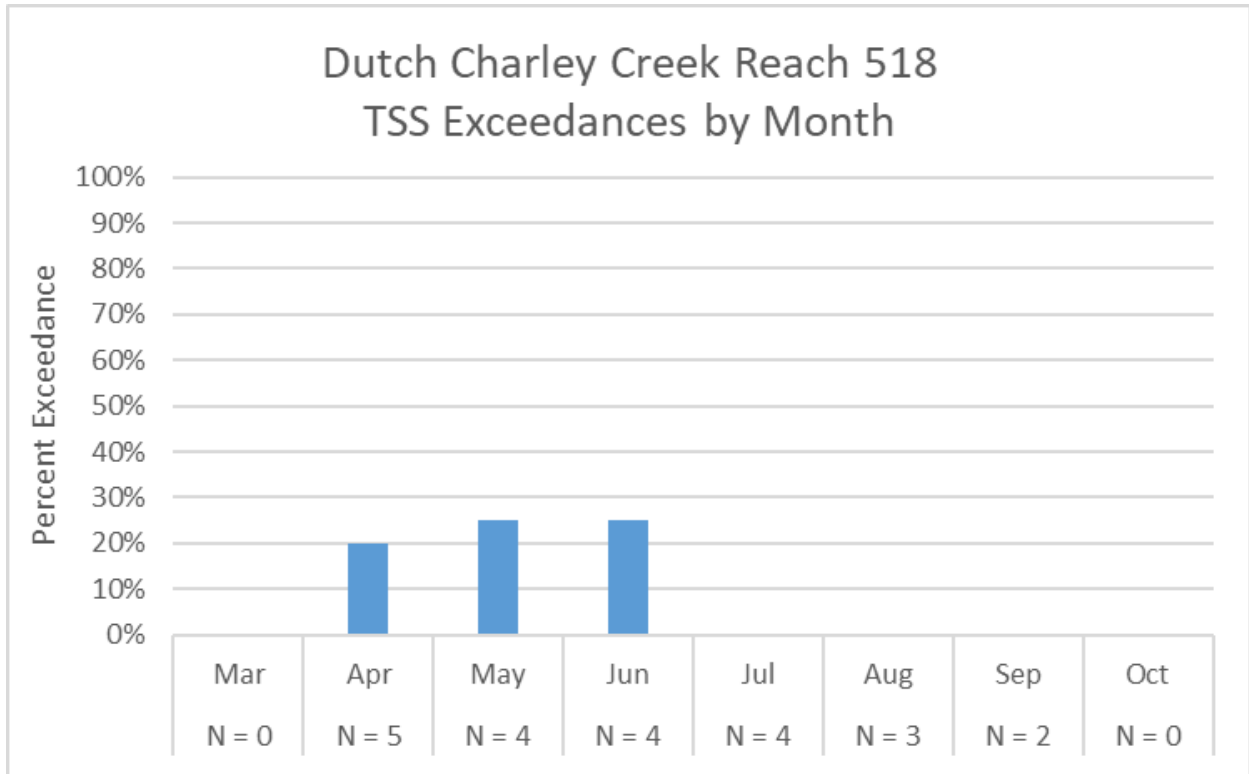


Figure A-22. Dutch Charley Creek Reach 518 TSS Exceedances by Month.

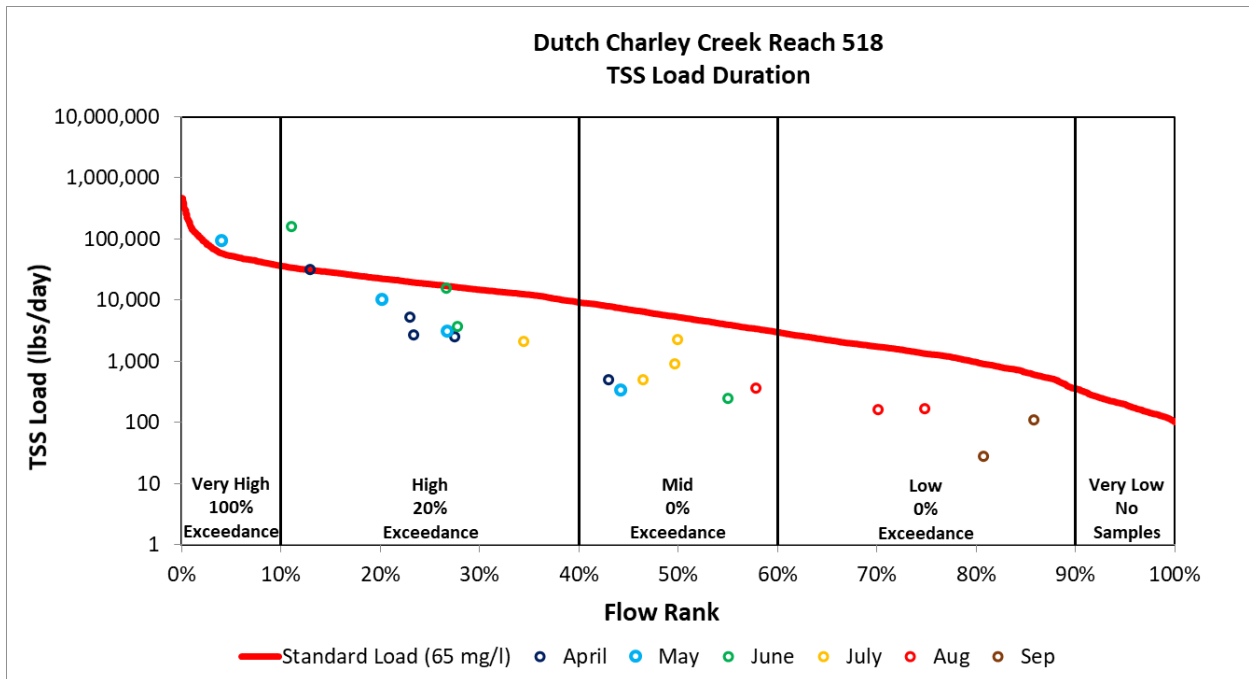


Figure A-23. Dutch Charley Creek Reach 518 TSS Load Duration Curve (by month).

Supporting Items for Highwater Creek TSS and *E. coli* Impaired Reach (07020008-519)

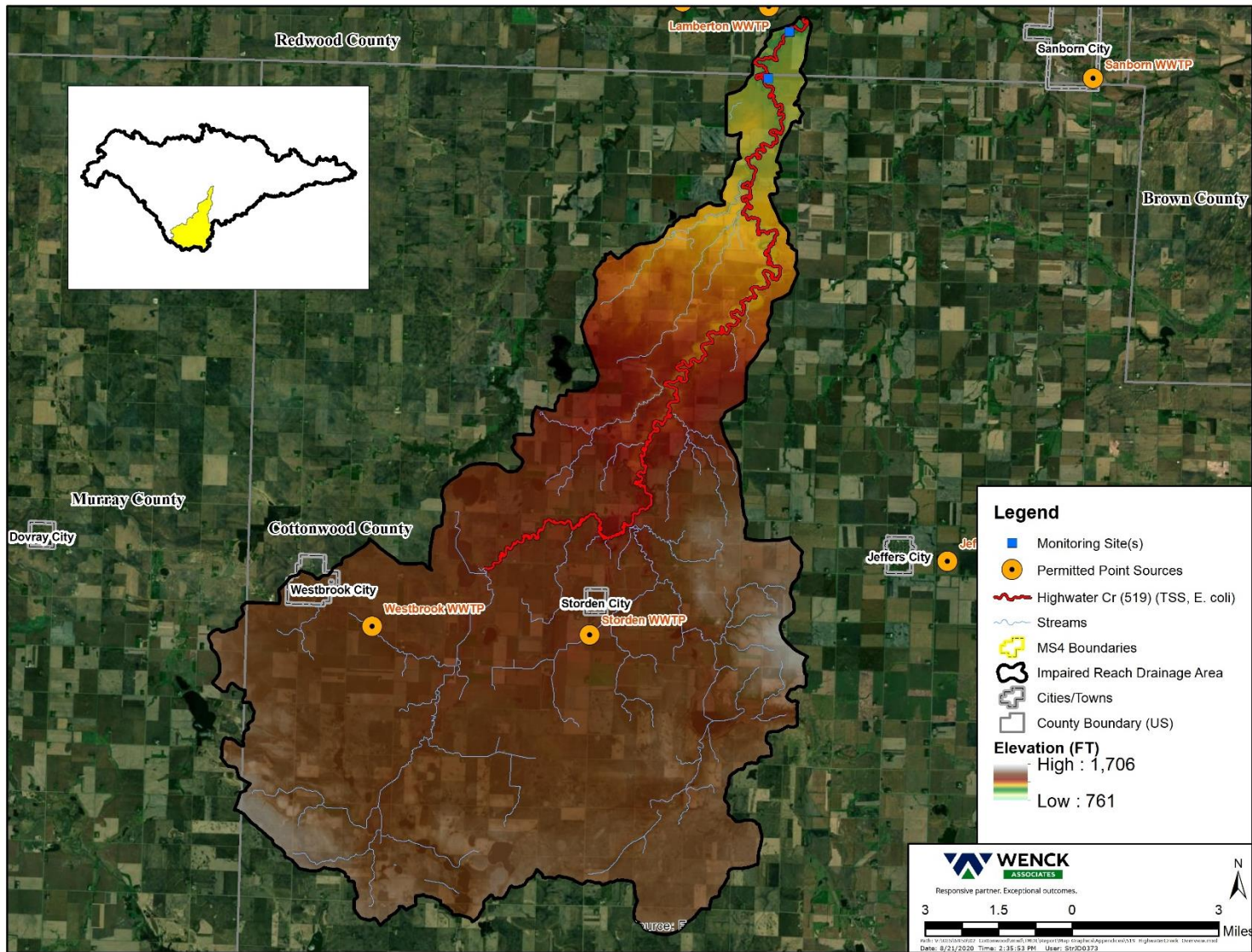


Figure A-24. Highwater Creek Reach 519 Overview.

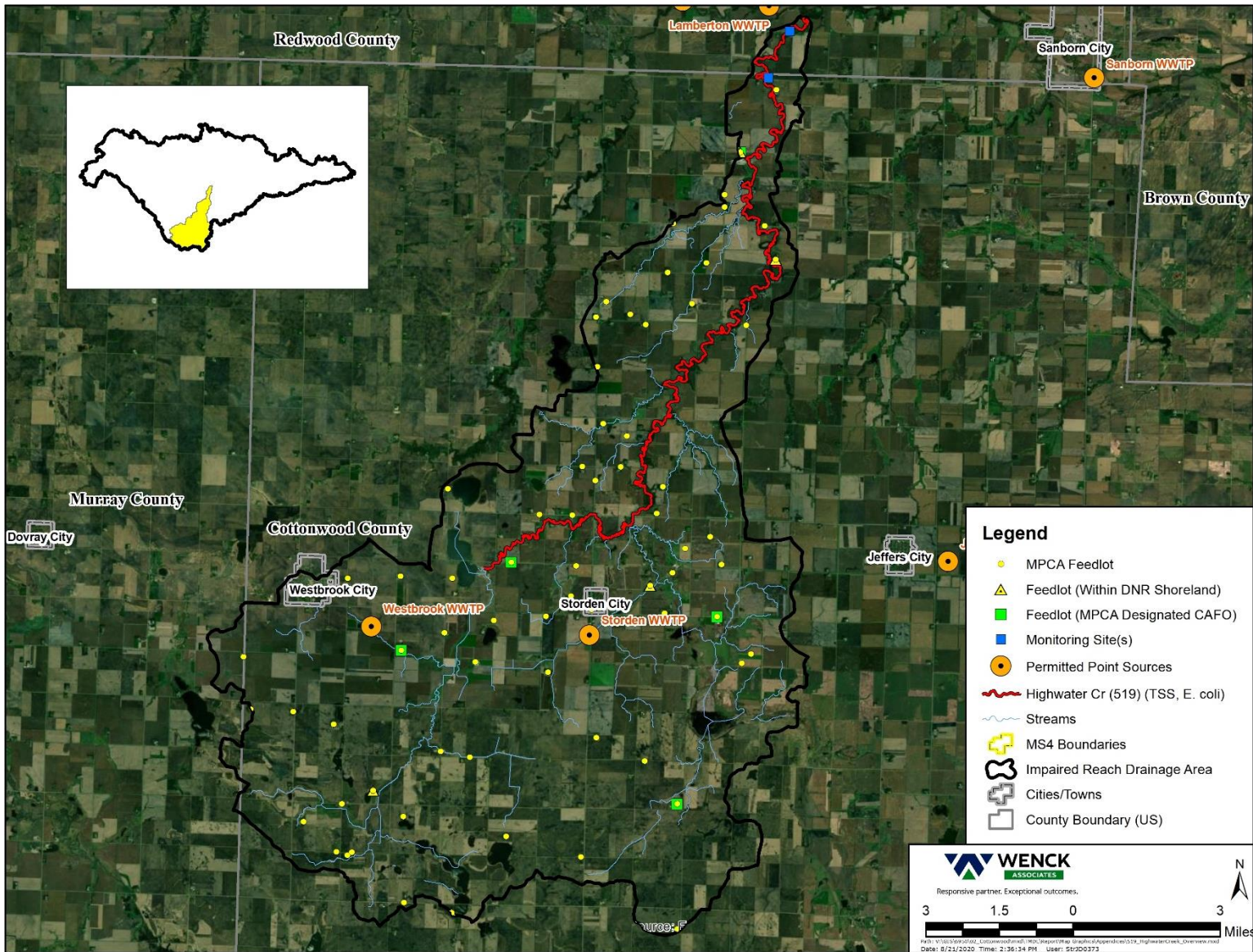


Figure A-25. Highwater Creek Reach 519 Feedlots.

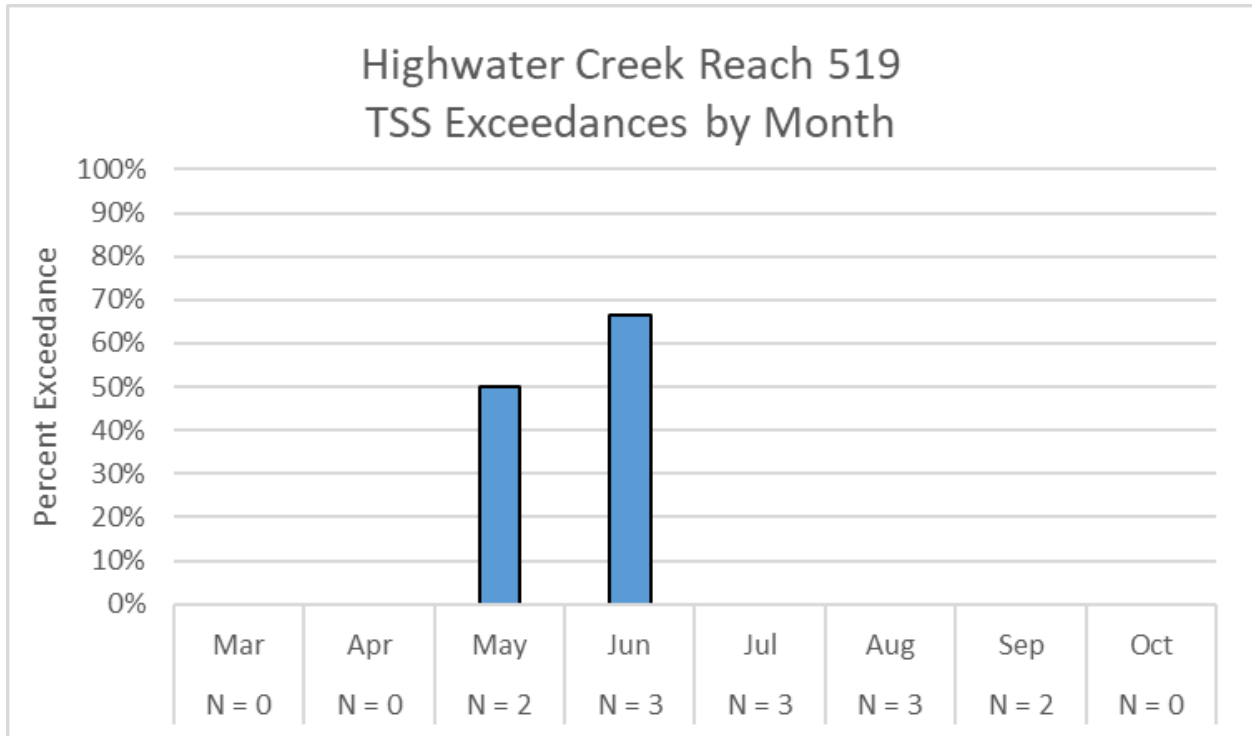


Figure A-26. Highwater Creek Reach 519 TSS Exceedances by Month.

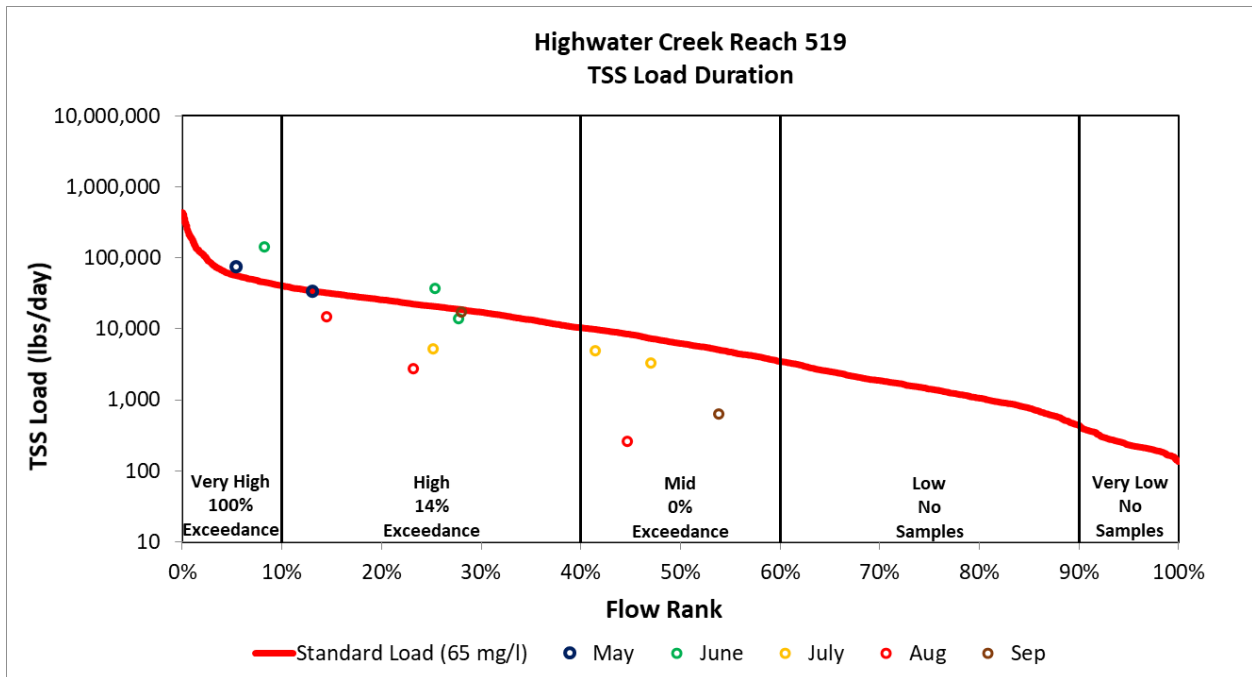


Figure A-27. Highwater Creek Reach 519 TSS Load Duration Curve (by month).

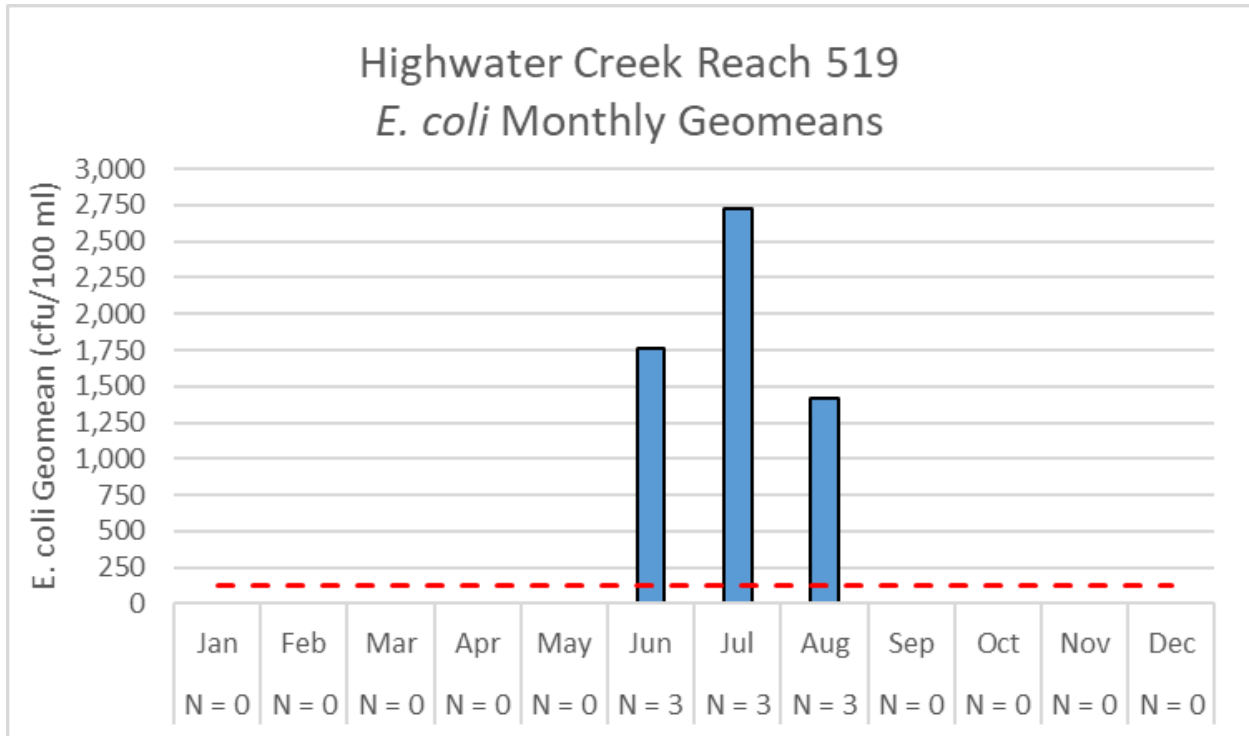


Figure A-28. Highwater Creek Reach 519 *E. coli* Monthly Geomeans.

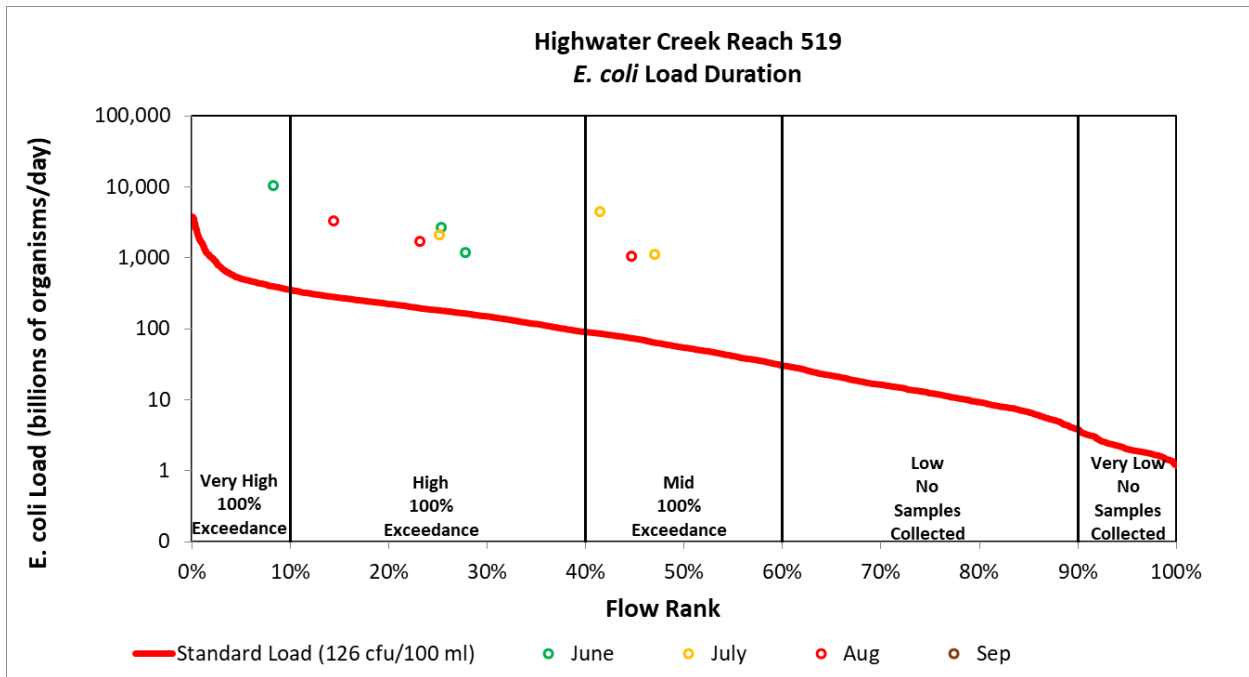


Figure A-29. Highwater Creek Reach 519 *E. coli* Load Duration Curve (by month).

Table A-3. Highwater Creek Reach 519 Bacteria Production Exercise.

Major Category	Source	Animal Units* or Individuals in Subwatershed	Fecal Bacteria Organisms Produced Per Unit Per Day	Total Fecal Bacteria Produced Per Day	Total Fecal Bacteria Produced Per Day by Major Category	Percent by Category
			[Billions of Org.] ⁸	[Billions of Org.]	[Billions of Org.]	
Livestock (Surface Applied Manure) ¹	Horse*	8	58.2	466	826,509	99.81%
	Swine*	5,035	32.7	164,645		
	Bovine*	11,120	58.2	647,201		
	Poultry*	3.4	20.5	71		
	Other Livestock*, ⁹	452	31.3	14,126		
Wildlife	Deer ³	542	0.5	271	922	0.11%
	Waterfowl ⁴	1,627	0.4	651		
Human	Failing Septic Systems ⁵	35	5.7	200	227	0.03%
	WWTP effluent ⁶	2	13.4	27		
Domestic Animals ²	Improperly Managed Pet Waste ⁷	694	0.6	391	391	0.05%

* Values reported as Animal Units.

¹ Livestock animal units estimated based on MPCA registered feedlot database with animal units converted based on MN Dept. of Ag conversion units (<http://www.mda.state.mn.us/animals/feedlots/feedlot-dmt/feedlot-dmt-animal-units.aspx>).

² # of households in watershed multiplied by 0.58 dogs/ household and 0.73 cates/household according to the SE MN Regional TMDL (MPCA, 2002)

³ Assumes average deer density of .0078 deer/acre from Monitoring Population Trends of White-tailed Deer in Minnesota (Minnesota DNR, 2013)

⁴ Estimated from the MN DNR and US Fish & Wildlife Service 2018 Waterfowl Breeding Population Survey (Minnesota DNR, 2018)

⁵ based on county SSTS inventory failure rates reported to MPCA (MPCA personal communication, 2018) and rural population estimates (3 persons/ septic) based on 2010 Census blocks.

⁶ Reported as # of facilities with production based on WWTP effluent data from facility discharge monitoring reports (DMRs)

⁷ Estimated that 35% of the bacteria produced per month attributed to pet waste is improperly managed and available for runoff (CWP, 1999)

⁸ Derived from literature rates in Metcalf and Eddy (1991), Horsley and Witten (1996), Alderisio and De Luca (1999), ASAE Standards (1998) and the Southeast Minnesota Regional TMDL (MPCA, 2002). Values have been reported to two significant digits.

⁹ Other cattle include llama, goat, and sheep.

Supporting Items for Dry Creek *E. coli* Impaired Reach (07020008-520)

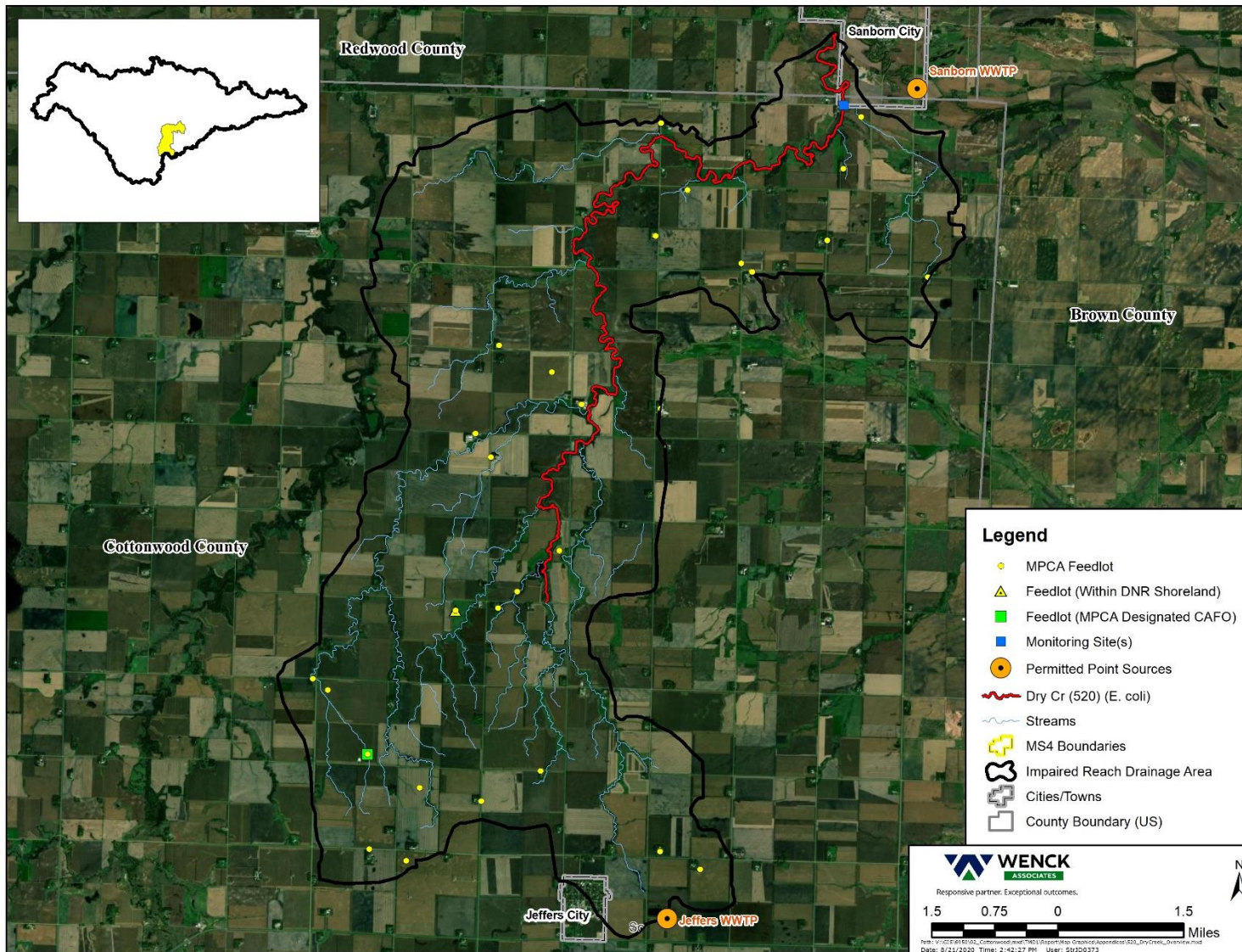


Figure A-30. Dry Creek Reach 520 Feedlots.

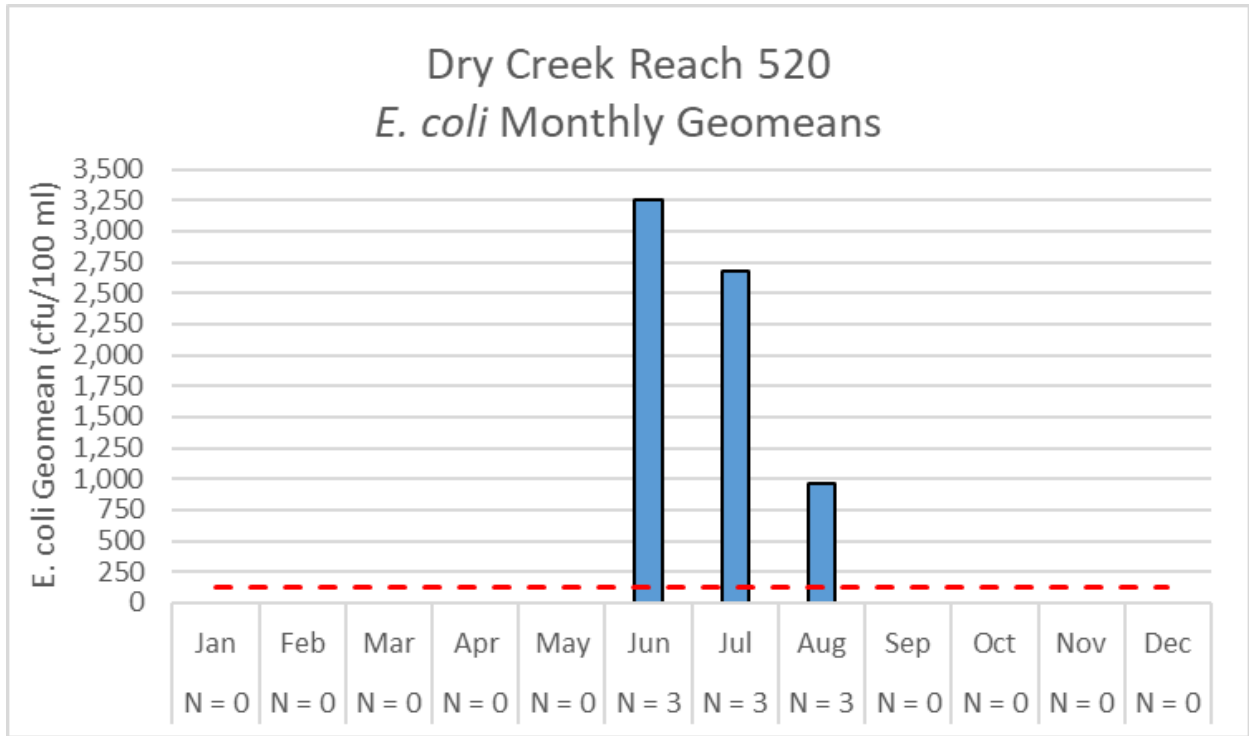


Figure A-31. Dry Creek Reach 520 *E. coli* Monthly Geomeans.

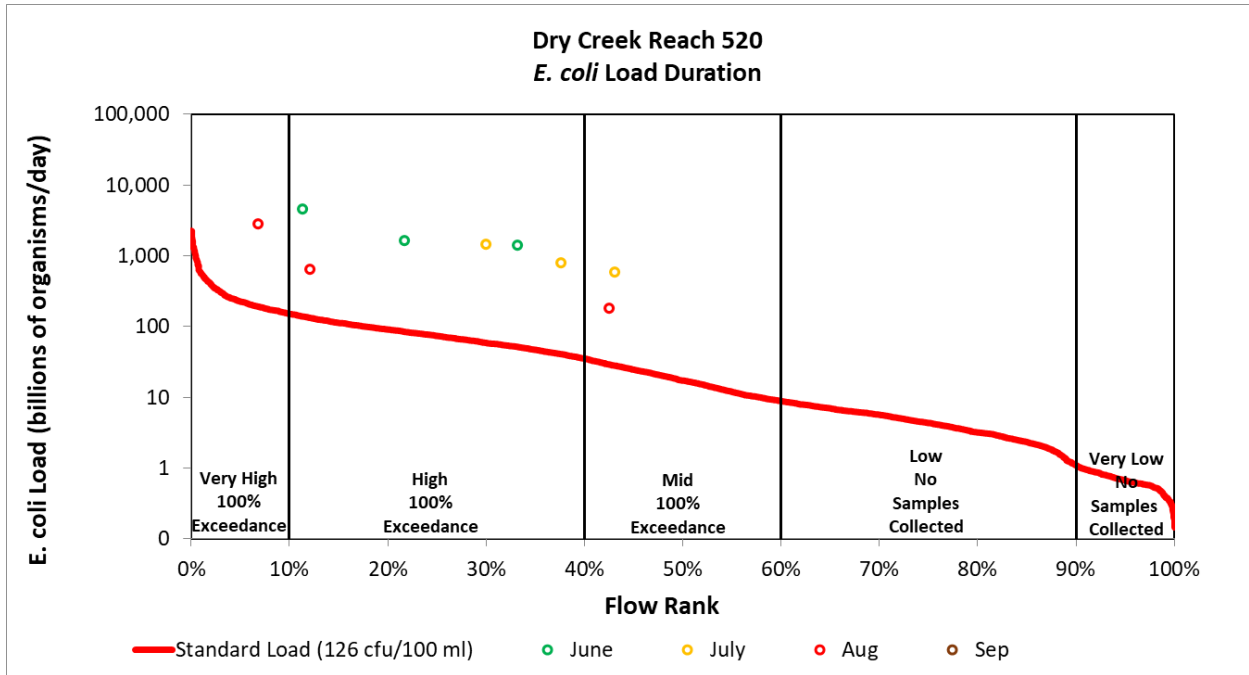


Figure A-32. Dry Creek Reach 520 *E. coli* Load Duration Curve (by month).

Table A-4. Dry Creek Reach 520 Bacteria Production Exercise.

Major Category	Source	Animal Units* or Individuals in Subwatershed	Fecal Bacteria Organisms Produced Per Unit Per Day	Total Fecal Bacteria Produced Per Day	Total Fecal Bacteria Produced Per Day by Major Category	Percent by Category
			[Billions of Org.] ⁸	[Billions of Org.]	[Billions of Org.]	
Livestock (Surface Applied Manure) ¹	Horse*	18	58.2	1,048	317,949	99.75%
	Swine*	1,008	32.7	32,962		
	Bovine*	4,875	58.2	283,719		
	Poultry*	0.5	20.5	11		
	Other Livestock*, ⁹	32	6.6	209		
Wildlife	Deer ³	205	0.5	103	349	0.11%
	Waterfowl ⁴	616	0.4	246		
Human	Failing Septic Systems ⁵	26	5.7	145	145	0.05%
	WWTP effluent ⁶	-	-	-		
Domestic Animals ²	Improperly Managed Pet Waste ⁷	511	0.6	287	287	0.09%

* Values reported as Animal Units.

¹ Livestock animal units estimated based on MPCA registered feedlot database with animal units converted based on MN Dept. of Ag conversion units (<http://www.mda.state.mn.us/animals/feedlots/feedlot-dmt/feedlot-dmt-animal-units.aspx>).

² # of households in watershed multiplied by 0.58 dogs/ household and 0.73 cates/household according to the SE MN Regional TMDL (MPCA, 2002)

³ Assumes average deer density of .0078 deer/acre from Monitoring Population Trends of White-tailed Deer in Minnesota (Minnesota DNR, 2013)

⁴ Estimated from the MN DNR and US Fish & Wildlife Service 2018 Waterfowl Breeding Population Survey (Minnesota DNR, 2018)

⁵ based on county SSTS inventory failure rates reported to MPCA (MPCA personal communication, 2018) and rural population estimates (3 persons/ septic) based on 2010 Census blocks.

⁶ Reported as # of facilities with production based on WWTP effluent data from facility discharge monitoring reports (DMRs)

⁷ Estimated that 35% of the bacteria produced per month attributed to pet waste is improperly managed and available for runoff (CWP, 1999)

⁸ Derived from literature rates in Metcalf and Eddy (1991), Horsley and Witten (1996), Alderisio and De Luca (1999), ASAE Standards (1998) and the Southeast Minnesota Regional TMDL (MPCA, 2002). Values have been reported to two significant digits.

⁹ Other cattle include llama, goat, and sheep.

Supporting Items for Mound Creek *E. coli* Impaired Reach (07020008-521)

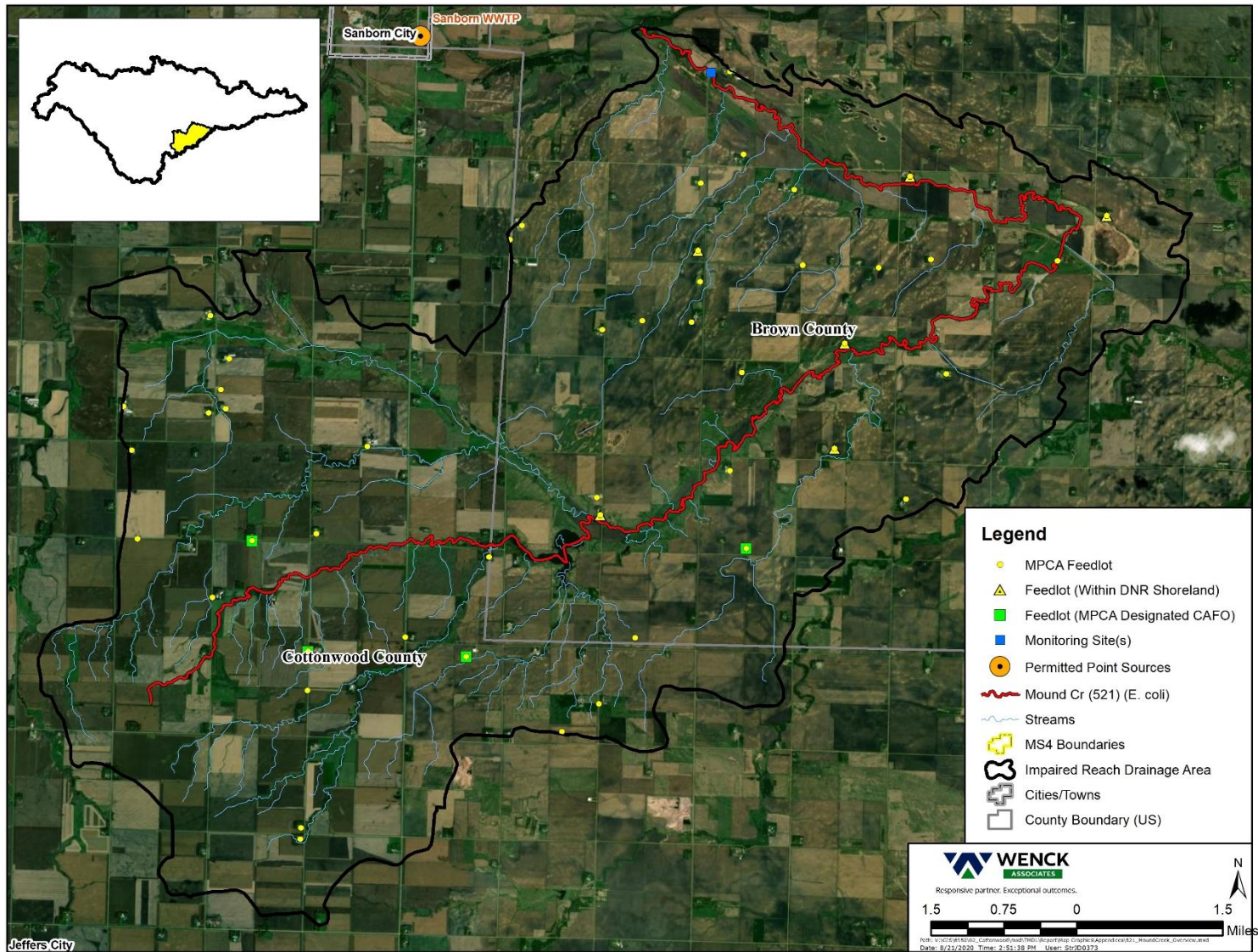


Figure A-33. Mound Creek Reach 521 Feedlots.

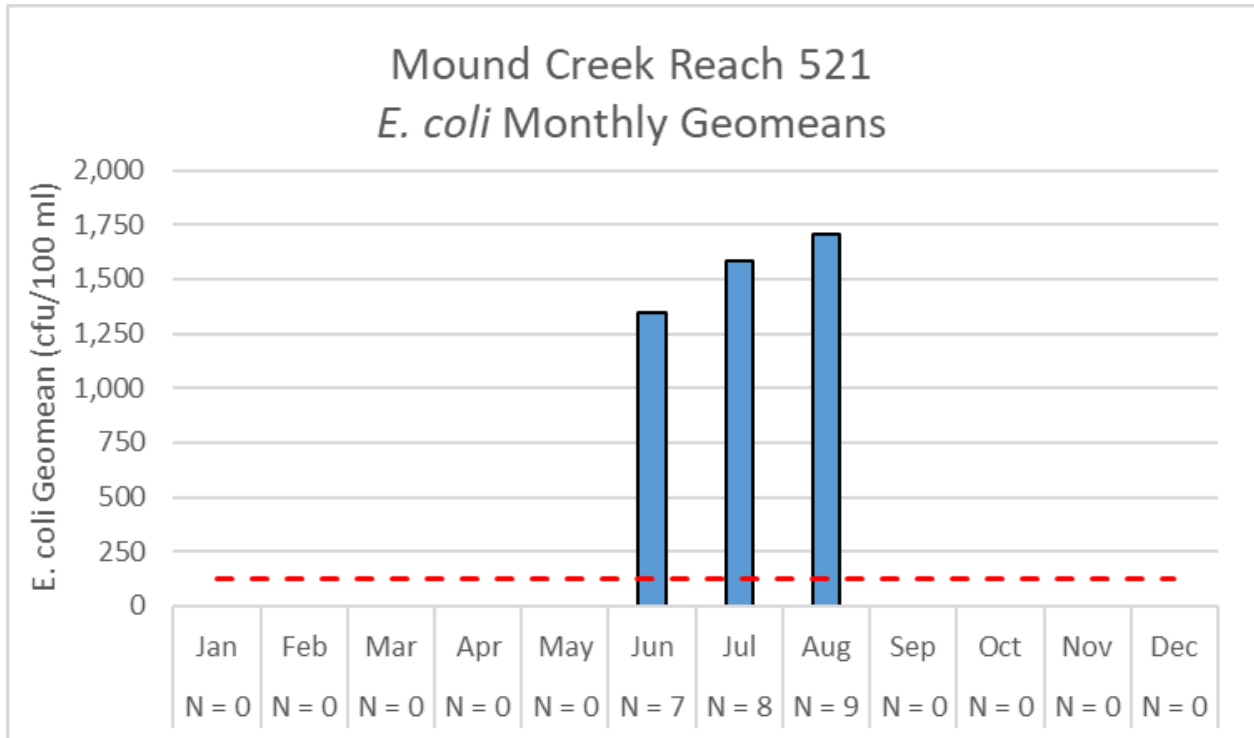


Figure A-34. Mound Creek Reach 521 *E. coli* Monthly Geomeans.

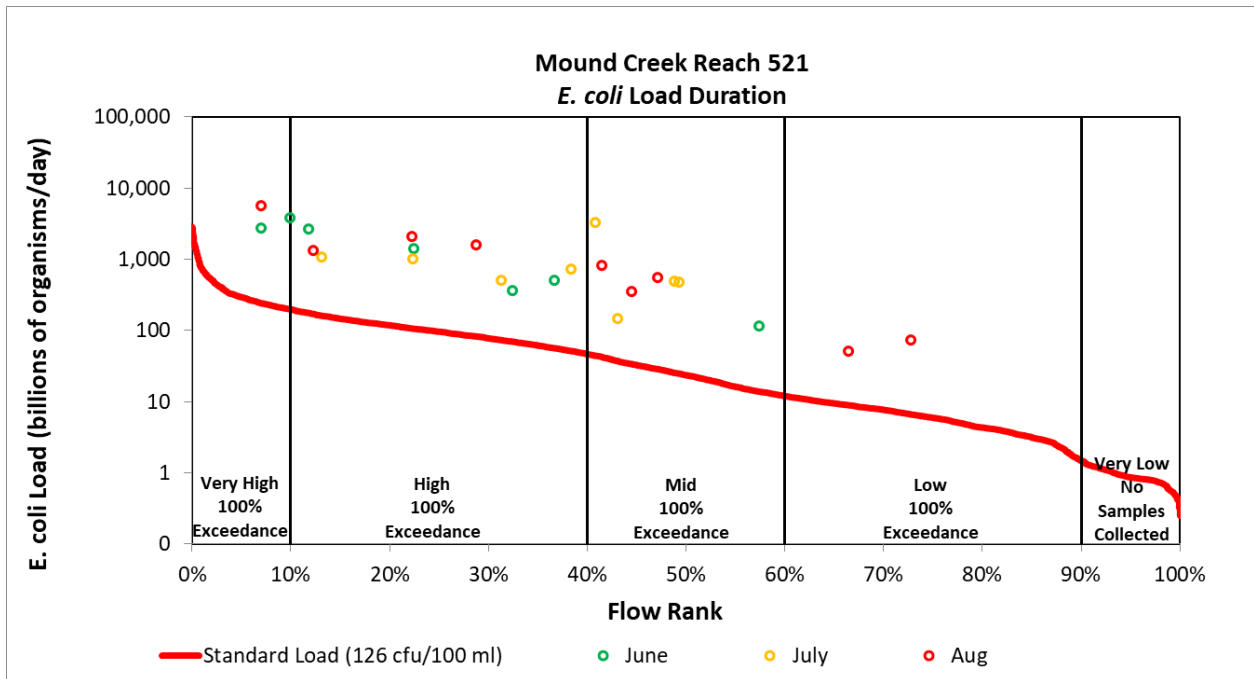


Figure A-35. Mound Creek Reach 521 *E. coli* Load Duration Curve (by month).

Table A-5. Mound Creek Reach 521 Bacteria Production Exercise.

Major Category	Source	Animal Units* or Individuals in Subwatershed	Fecal Bacteria Organisms Produced Per Unit Per Day	Total Fecal Bacteria Produced Per Day	Total Fecal Bacteria Produced Per Day by Major Category	Percent by Category
			[Billions of Org.] ⁸	[Billions of Org.]	[Billions of Org.]	
Livestock (Surface Applied Manure) ¹	Horse*	7	58.2	407	678,335	99.89%
	Swine*	5,677	32.7	185,648		
	Bovine*	8,454	58.2	492,017		
	Poultry*	0.4	20.5	8		
	Other Livestock ^{*,9}	8	32.7	255		
Wildlife	Deer ³	276	0.5	138	469	0.07%
	Waterfowl ⁴	827	0.4	331		
Human	Failing Septic Systems ⁵	20	5.7	114	114	0.02%
	WWTP effluent ⁶	-	-	-		
Domestic Animals ²	Improperly Managed Pet Waste ⁷	342	0.6	192	192	0.03%

* Values reported as Animal Units.

¹ Livestock animal units estimated based on MPCA registered feedlot database with animal units converted based on MN Dept. of Ag conversion units (<http://www.mda.state.mn.us/animals/feedlots/feedlot-dmt/feedlot-dmt-animal-units.aspx>).

² # of households in watershed multiplied by 0.58 dogs/ household and 0.73 cates/household according to the SE MN Regional TMDL (MPCA, 2002)

³ Assumes average deer density of .0078 deer/acre from Monitoring Population Trends of White-tailed Deer in Minnesota (Minnesota DNR, 2013)

⁴ Estimated from the MN DNR and US Fish & Wildlife Service 2018 Waterfowl Breeding Population Survey (Minnesota DNR, 2018)

⁵ based on county SSTS inventory failure rates reported to MPCA (MPCA personal communication, 2018) and rural population estimates (3 persons/ septic) based on 2010 Census blocks.

⁶ Reported as # of facilities with production based on WWTP effluent data from facility discharge monitoring reports (DMRs)

⁷ Estimated that 35% of the bacteria produced per month attributed to pet waste is improperly managed and available for runoff (CWP, 1999)

⁸ Derived from literature rates in Metcalf and Eddy (1991), Horsley and Witten (1996), Alderisio and De Luca (1999), ASAE Standards (1998) and the Southeast Minnesota Regional TMDL (MPCA, 2002). Values have been reported to two significant digits.

⁹ Other cattle include llama, goat, and sheep.

Supporting Items for Pell Creek *E. coli* Impaired Reach (07020008-523)

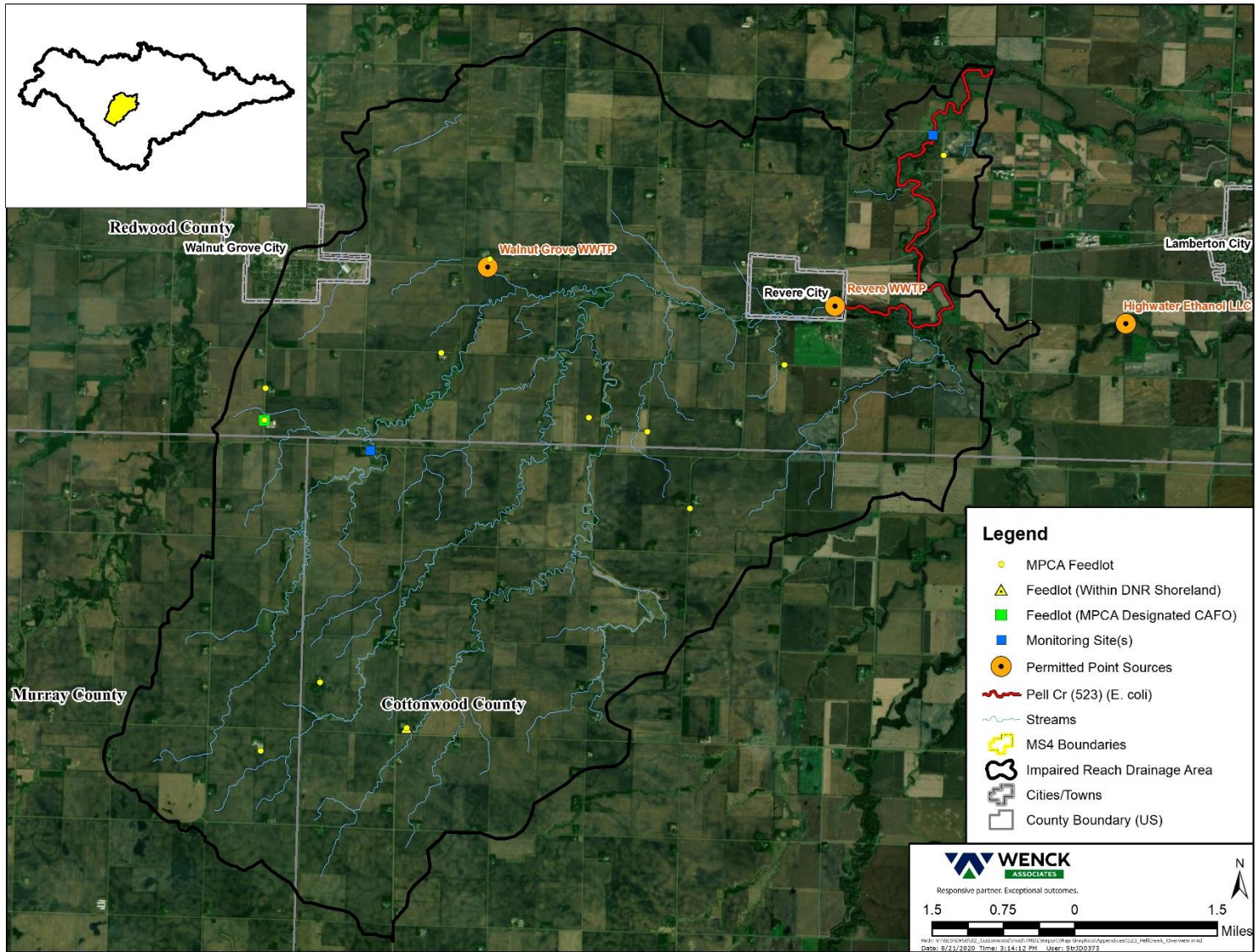


Figure A-36. Pell Creek Reach 523 Feedlots.

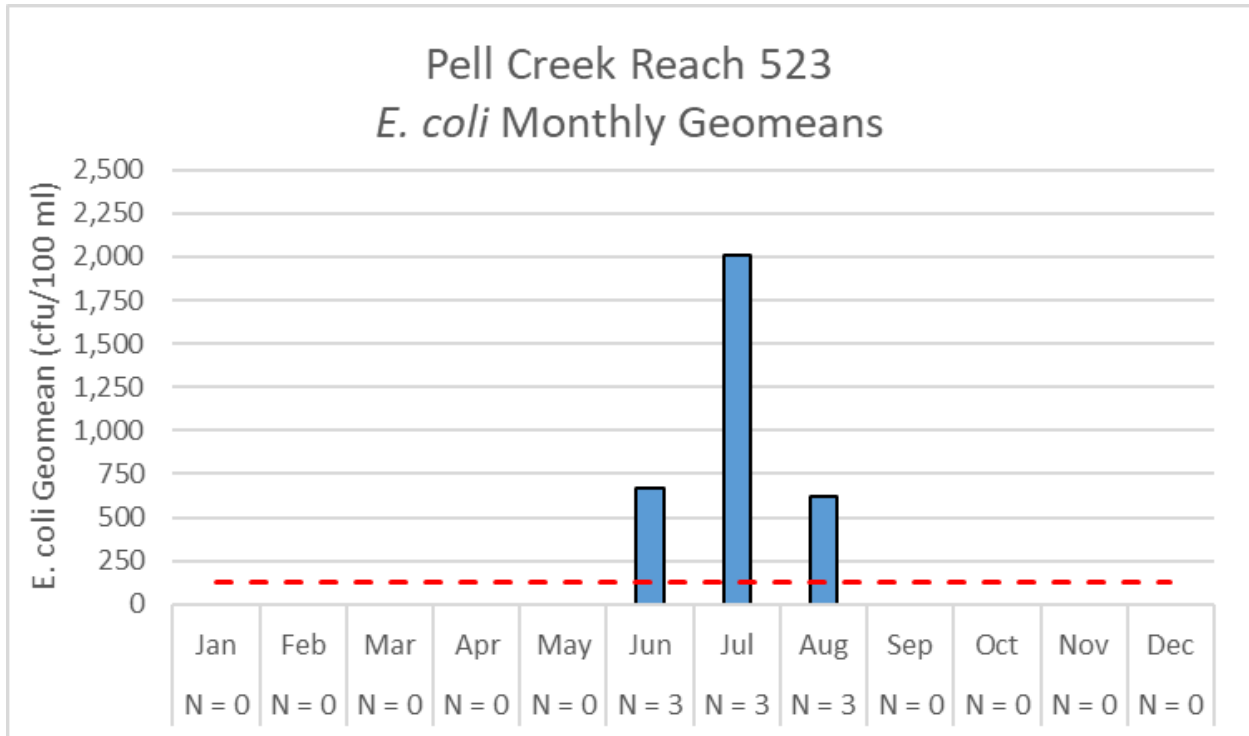


Figure A-37. Pell Creek Reach 523 *E. coli* Monthly Geomeans.

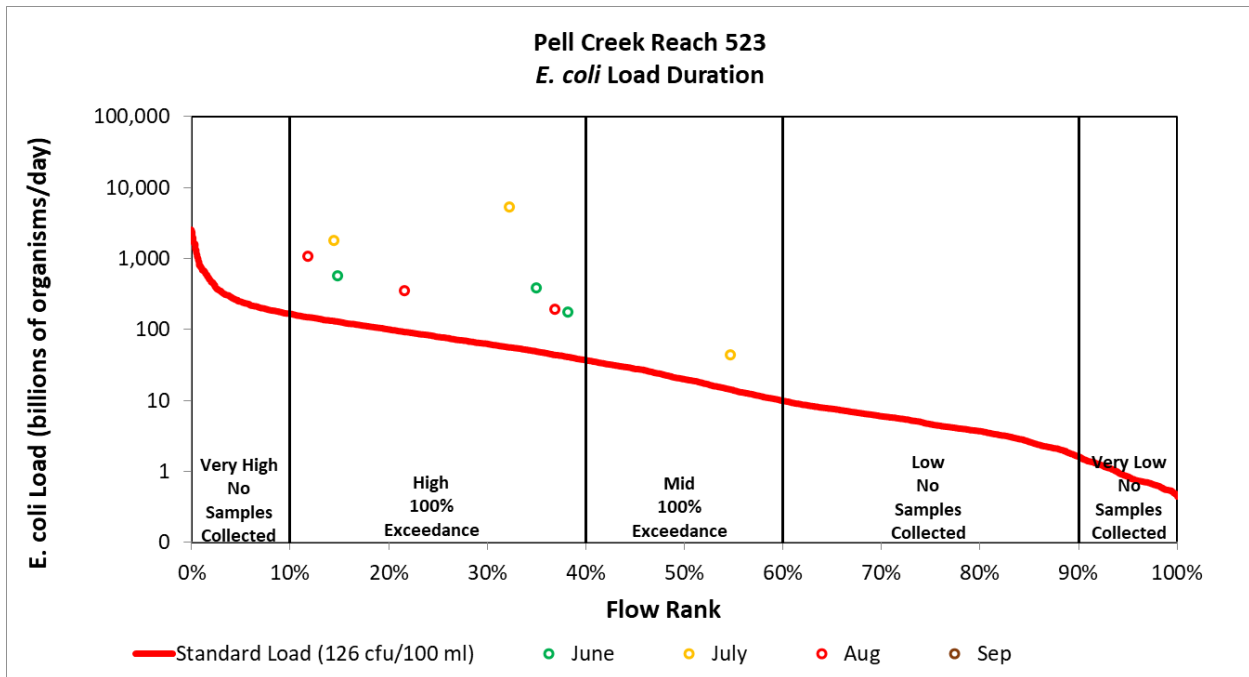


Figure A-38. Pell Creek Reach 523 *E. coli* Load Duration Curve (by month).

Table A-6. Pell Creek Reach 523 Bacteria Production Exercise.

Major Category	Source	Animal Units* or Individuals in Subwatershed	Fecal Bacteria Organisms Produced Per Unit Per Day	Total Fecal Bacteria Produced Per Day	Total Fecal Bacteria Produced Per Day by Major Category	Percent by Category
			[Billions of Org.] ⁸	[Billions of Org.]	[Billions of Org.]	
Livestock (Surface Applied Manure) ¹	Horse*	1	58.2	58	102,951	99.33%
	Swine*	60	32.7	1,962		
	Bovine*	1,730	58.2	100,686		
	Poultry*	-	-	-		
	Other Livestock*, ⁹	8	32.7	245		
Wildlife	Deer ³	259	0.5	130	441	0.43%
	Waterfowl ⁴	777	0.4	311		
Human	Failing Septic Systems ⁵	12	5.7	65	66	0.06%
	WWTP effluent ⁶	2	0.1	0		
Domestic Animals ²	Improperly Managed Pet Waste ⁷	343	0.6	193	193	0.19%

* Values reported as Animal Units.

¹ Livestock animal units estimated based on MPCA registered feedlot database with animal units converted based on MN Dept. of Ag conversion units (<http://www.mda.state.mn.us/animals/feedlots/feedlot-dmt/feedlot-dmt-animal-units.aspx>).

² # of households in watershed multiplied by 0.58 dogs/ household and 0.73 cates/household according to the SE MN Regional TMDL (MPCA, 2002)

³ Assumes average deer density of .0078 deer/acre from Monitoring Population Trends of White-tailed Deer in Minnesota (Minnesota DNR, 2013)

⁴ Estimated from the MN DNR and US Fish & Wildlife Service 2018 Waterfowl Breeding Population Survey (Minnesota DNR, 2018)

⁵ based on county SSTS inventory failure rates reported to MPCA (MPCA personal communication, 2018) and rural population estimates (3 persons/ septic) based on 2010 Census blocks.

⁶ Reported as # of facilities with production based on WWTP effluent data from facility discharge monitoring reports (DMRs)

⁷ Estimated that 35% of the bacteria produced per month attributed to pet waste is improperly managed and available for runoff (CWP, 1999)

⁸ Derived from literature rates in Metcalf and Eddy (1991), Horsley and Witten (1996), Alderisio and De Luca (1999), ASAE Standards (1998) and the Southeast Minnesota Regional TMDL (MPCA, 2002). Values have been reported to two significant digits.

⁹ Other cattle include llama, goat, and sheep.

Supporting Items for Pell Creek TSS Impaired Reach (07020008-535)

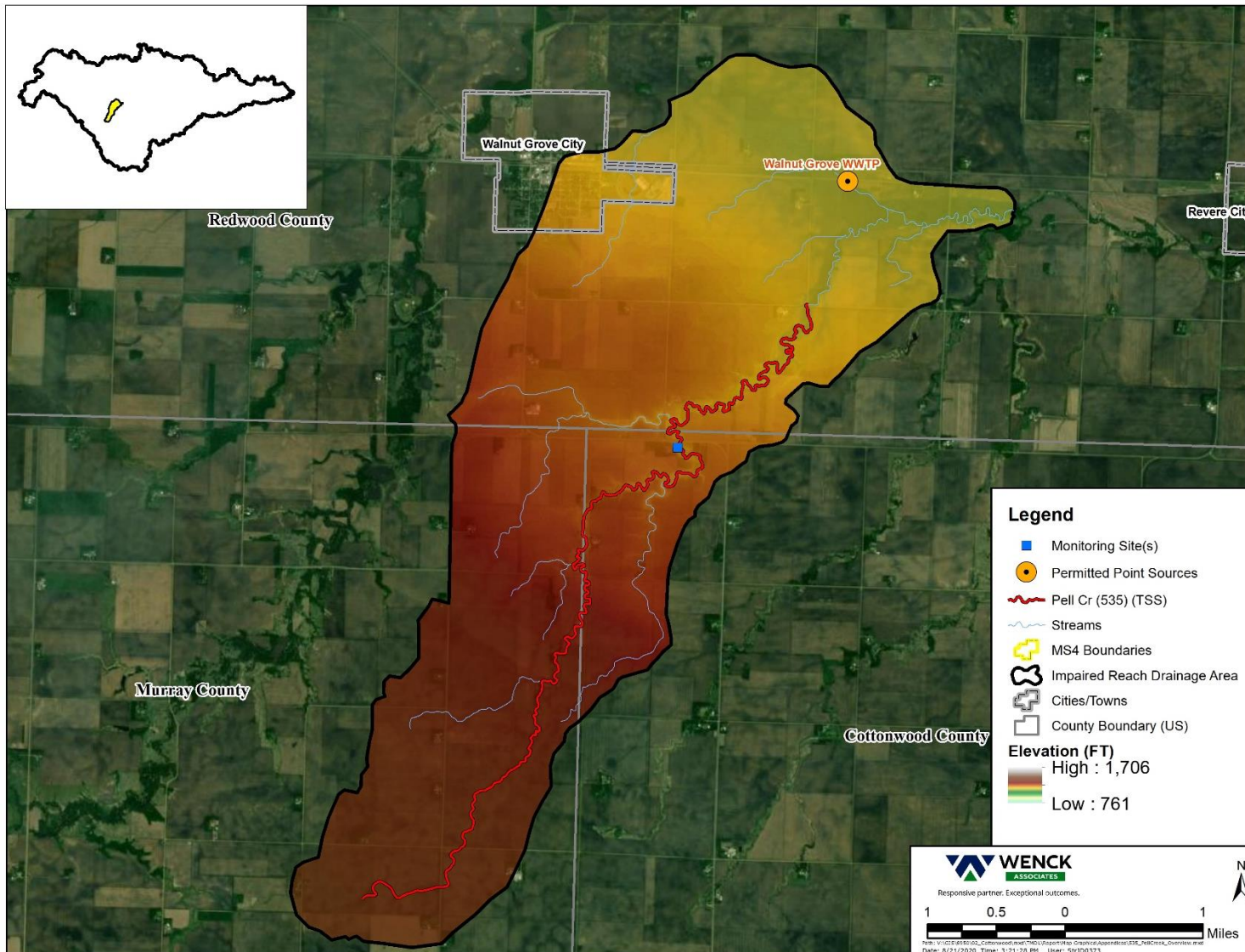


Figure A-39. Pell Creek Reach 535 Overview.

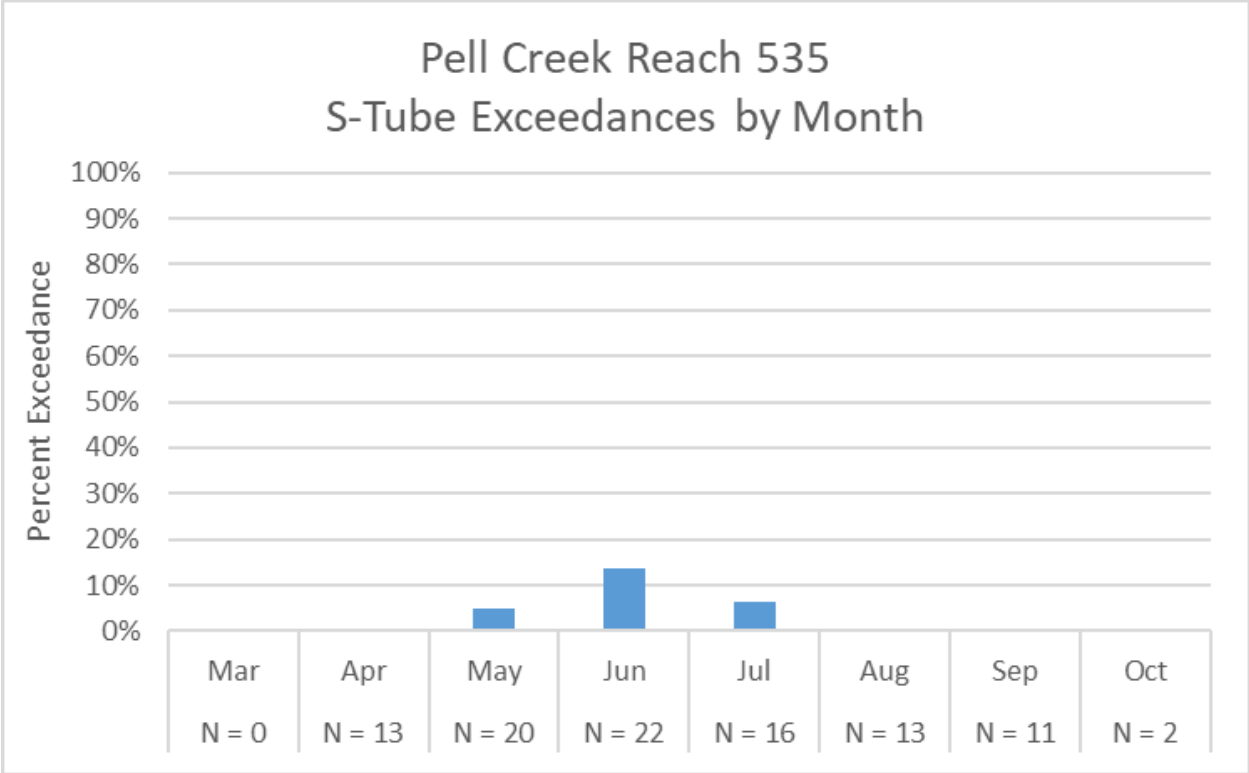


Figure A-40. Pell Creek Reach 535 S-Tube Exceedances by Month.

Note: No TSS samples have been collected for this reach

Supporting Items for Sleepy Eye Creek TSS Impaired Reach (07020008-599)

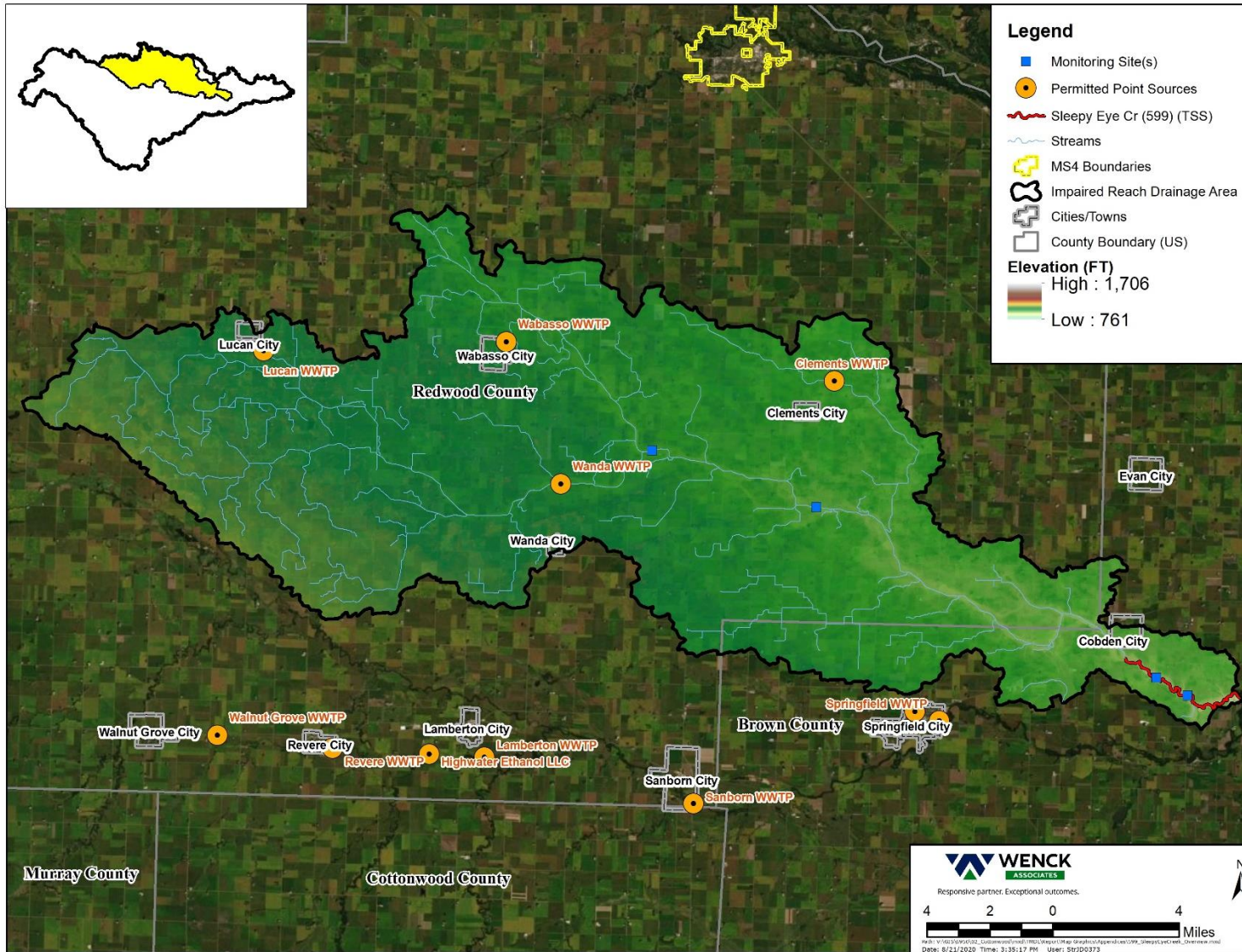


Figure A-41. Sleepy Eye Creek Reach 599 Overview.

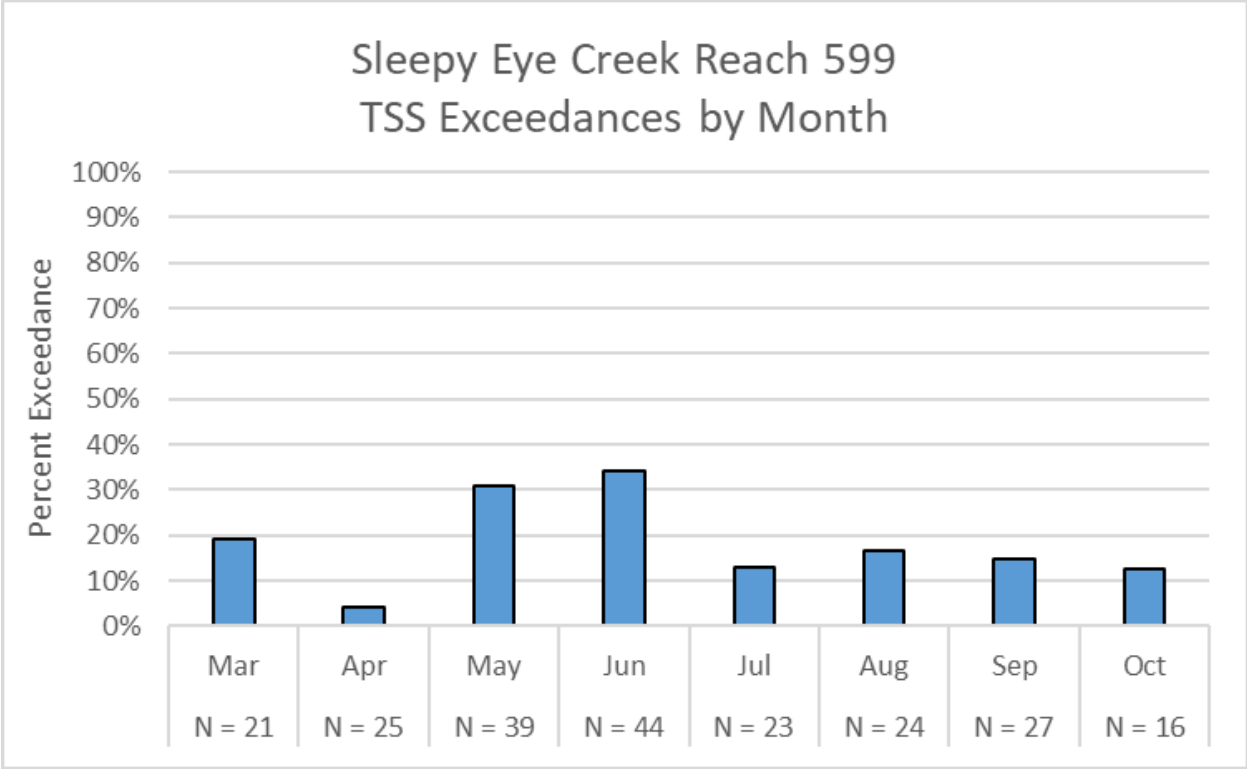


Figure A-42. Sleepy Eye Creek Reach 599 TSS Exceedances by Month.

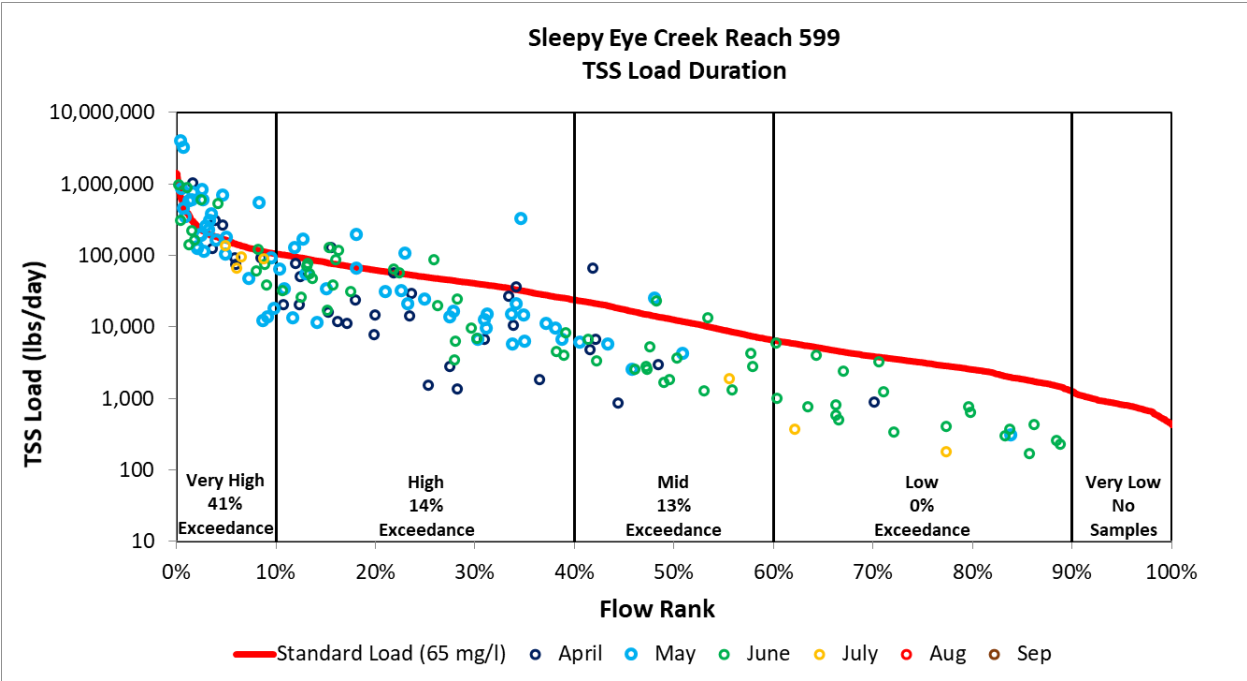


Figure A-43. Sleepy Eye Creek Reach 599 TSS Load Duration Curve (by month).

Supporting Items for Plum Creek (JD 20A) TSS Impaired Reaches (07020008-602 & 603)

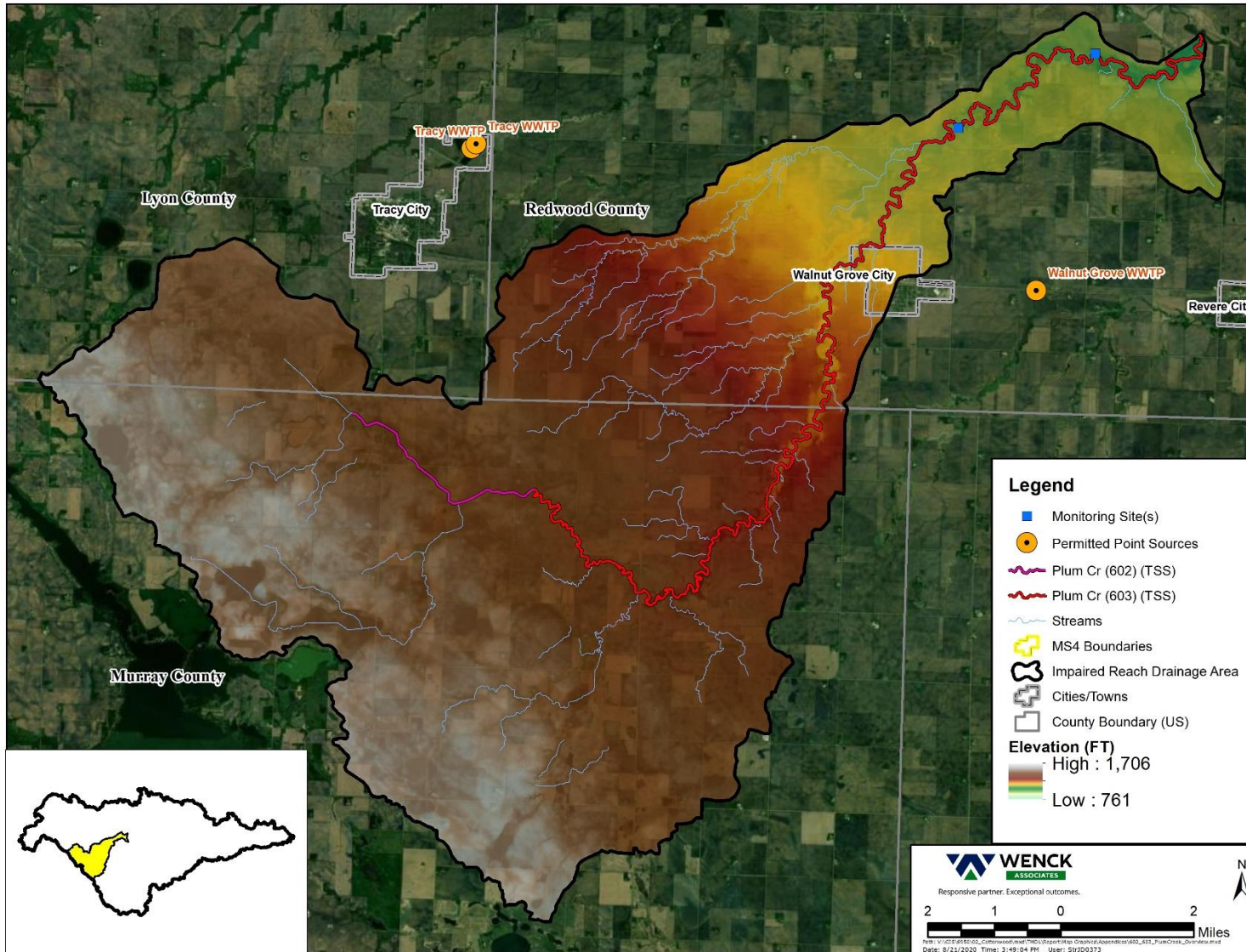


Figure A-44. Plum Creek (JD 20A) Reach 602 & 603 Overview.

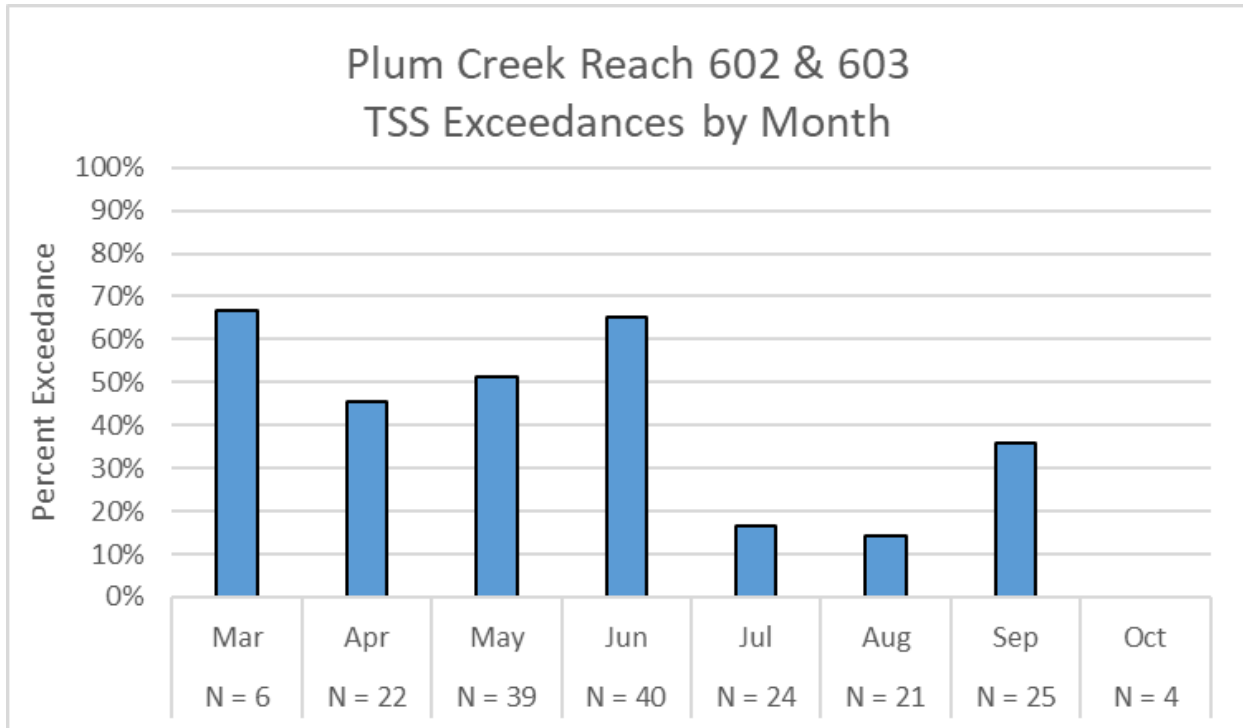


Figure A-45. Plum Creek (JD 20A) Reach 602 & 603 TSS Exceedances by Month.

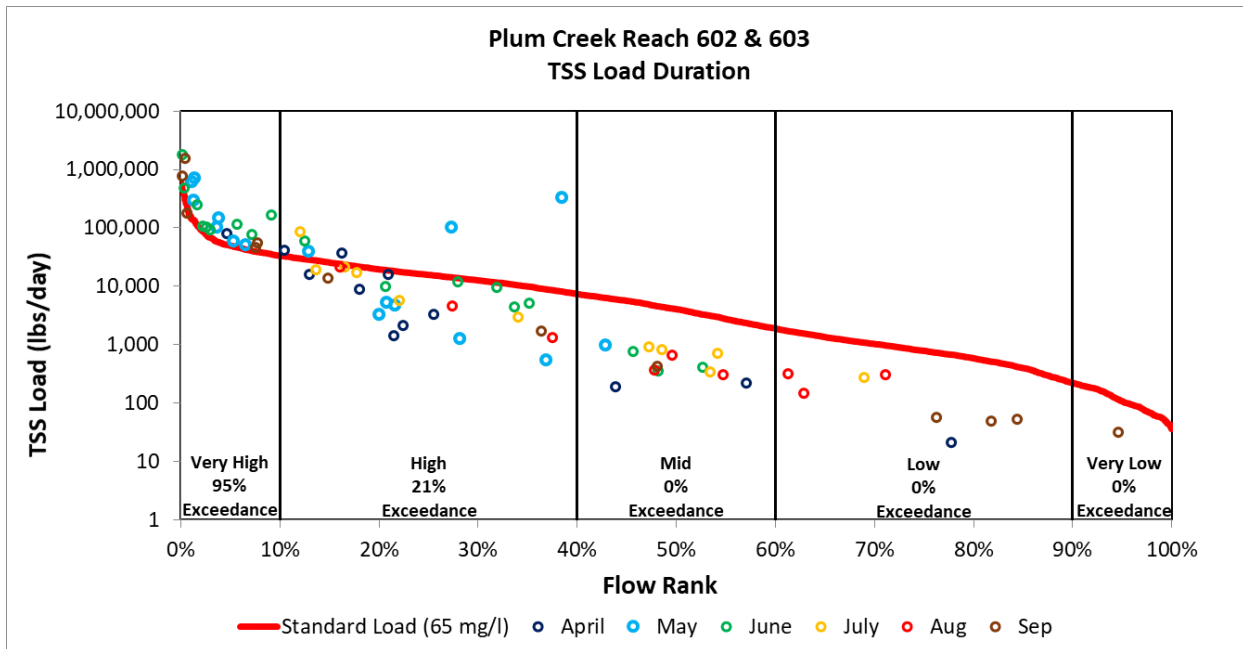


Figure A-46. Plum Creek (JD 20A) Reach 602 & 603 TSS Load Duration Curve (by month).

Supporting Items for Coal Mine Creek *E. coli* Impaired Reach (07020008-604)

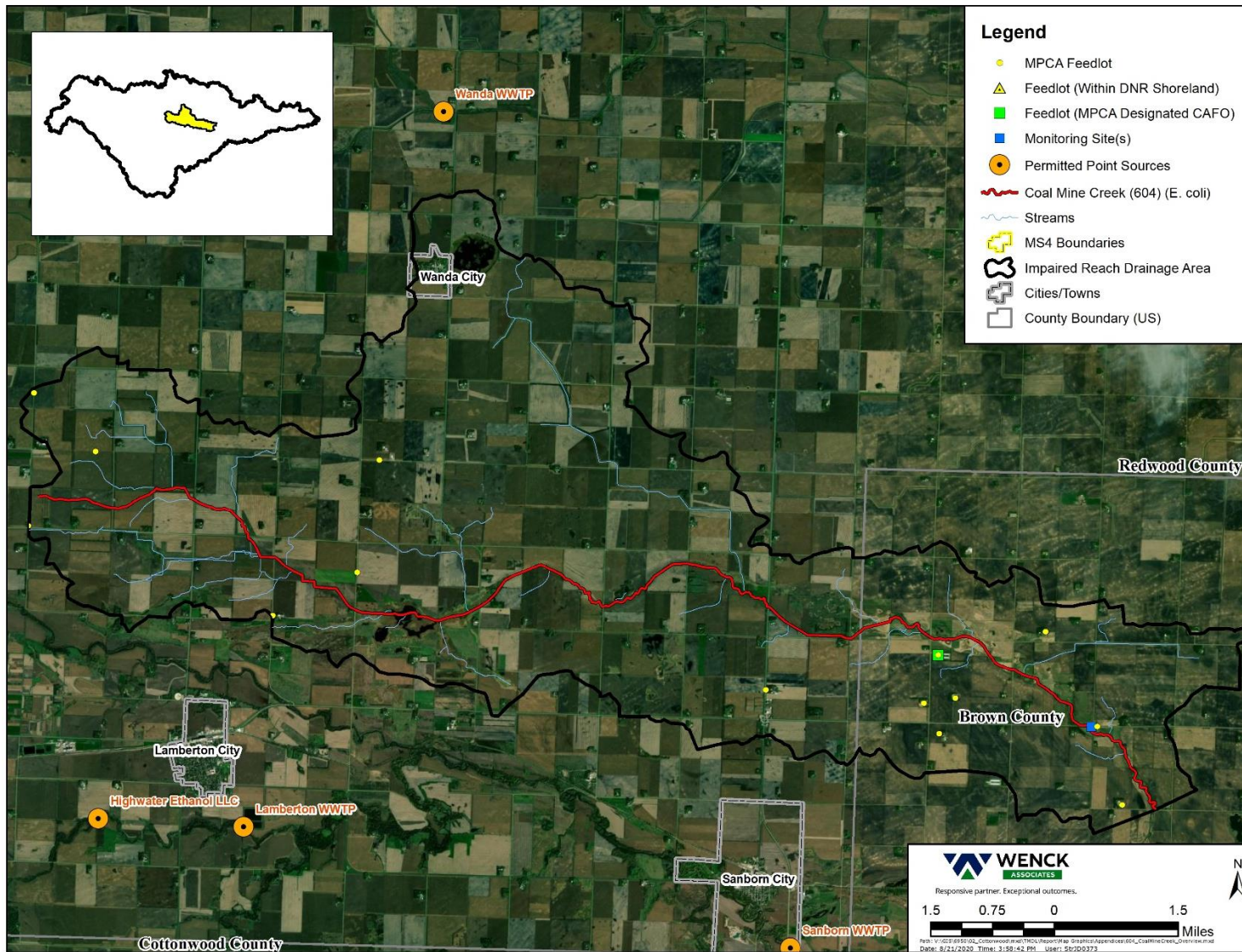


Figure A-47. Coal Mine Creek Reach 604 Feedlots.

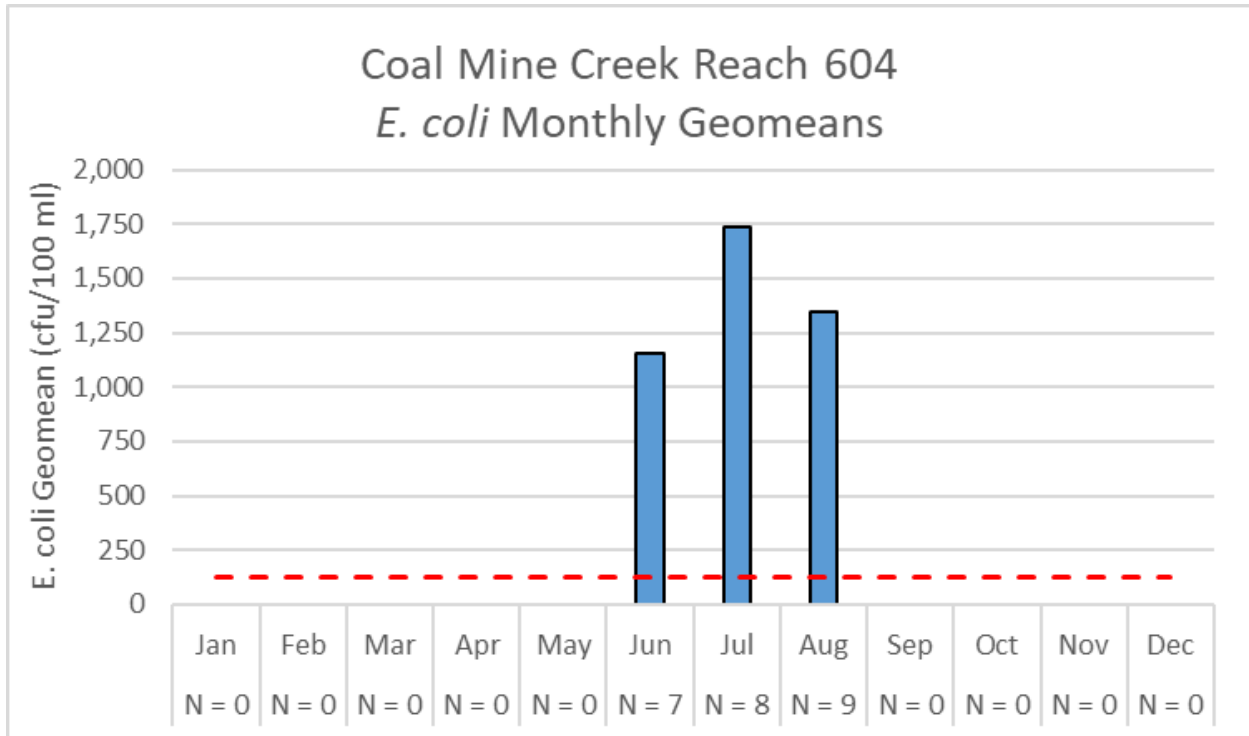


Figure A-48. Coal Mine Creek Reach 604 *E. coli* Monthly Geomeans.

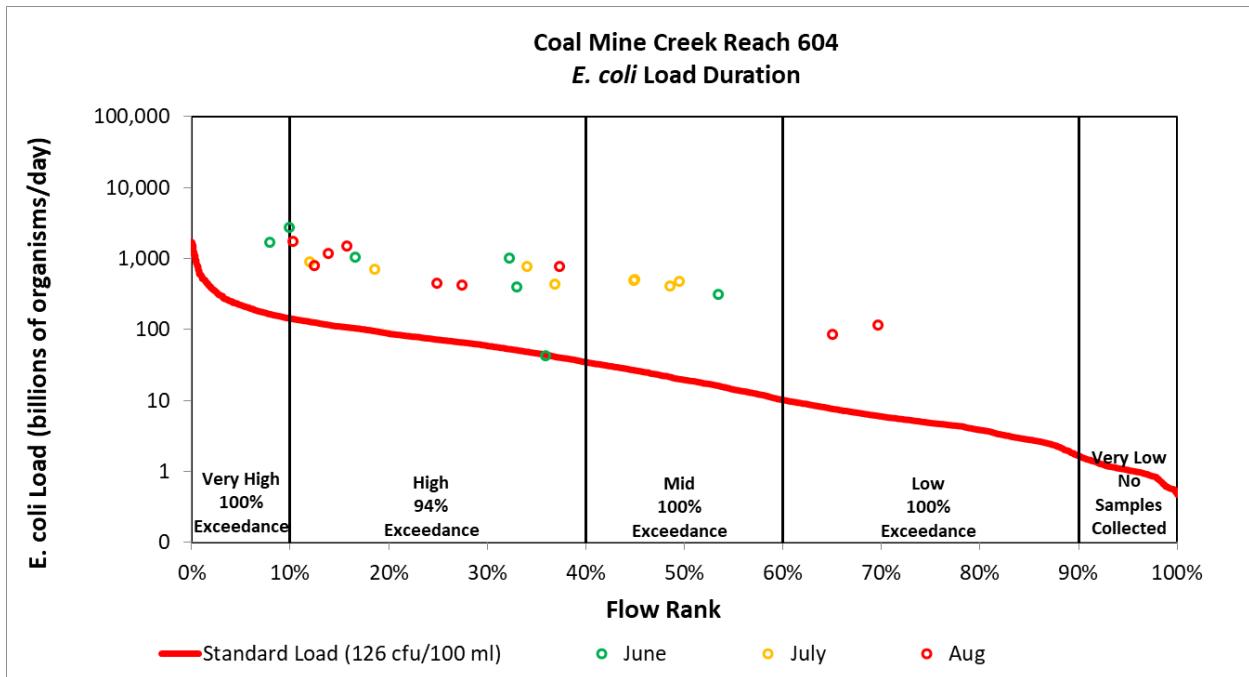


Figure A-49. Coal Mine Creek Reach 523 *E. coli* Load Duration Curve (by month).

Table A-7. Coal Mine Creek Reach 604 Bacteria Production Exercise.

Major Category	Source	Animal Units* or Individuals in Subwatershed	Fecal Bacteria Organisms Produced Per Unit Per Day	Total Fecal Bacteria Produced Per Day	Total Fecal Bacteria Produced Per Day by Major Category	Percent by Category
			[Billions of Org.] ⁸	[Billions of Org.]	[Billions of Org.]	
Livestock (Surface Applied Manure) ¹	Horse*	-	-	-	149,337	99.51%
	Swine*	1,665	32.7	54,446		
	Bovine*	1,241	58.2	72,203		
	Poultry*	1,107	20.5	22,688		
	Other Livestock*, ⁹	0	-	-		
Wildlife	Deer ³	230	0.5	115	391	0.26%
	Waterfowl ⁴	689	0.4	276		
Human	Failing Septic Systems ⁵	12	5.7	71	71	0.05%
	WWTP effluent ⁶	-	-	-		
Domestic Animals ²	Improperly Managed Pet Waste ⁷	478	0.6	269	269	0.18%

* Values reported as Animal Units.

¹ Livestock animal units estimated based on MPCA registered feedlot database with animal units converted based on MN Dept. of Ag conversion units (<http://www.mda.state.mn.us/animals/feedlots/feedlot-dmt/feedlot-dmt-animal-units.aspx>).

² # of households in watershed multiplied by 0.58 dogs/ household and 0.73 cates/household according to the SE MN Regional TMDL (MPCA, 2002)

³ Assumes average deer density of .0078 deer/acre from Monitoring Population Trends of White-tailed Deer in Minnesota (Minnesota DNR, 2013)

⁴ Estimated from the MN DNR and US Fish & Wildlife Service 2018 Waterfowl Breeding Population Survey (Minnesota DNR, 2018)

⁵ based on county SSTS inventory failure rates reported to MPCA (MPCA personal communication, 2018) and rural population estimates (3 persons/ septic) based on 2010 Census blocks.

⁶ Reported as # of facilities with production based on WWTP effluent data from facility discharge monitoring reports (DMRs)

⁷ Estimated that 35% of the bacteria produced per month attributed to pet waste is improperly managed and available for runoff (CWP, 1999)

⁸ Derived from literature rates in Metcalf and Eddy (1991), Horsley and Witten (1996), Alderisio and De Luca (1999), ASAE Standards (1998) and the Southeast Minnesota Regional TMDL (MPCA, 2002). Values have been reported to two significant digits.

⁹ Other cattle include llama, goat, and sheep.

Supporting Items for Judicial Ditch 30 *E. coli* Impaired Reach (07020008-609)

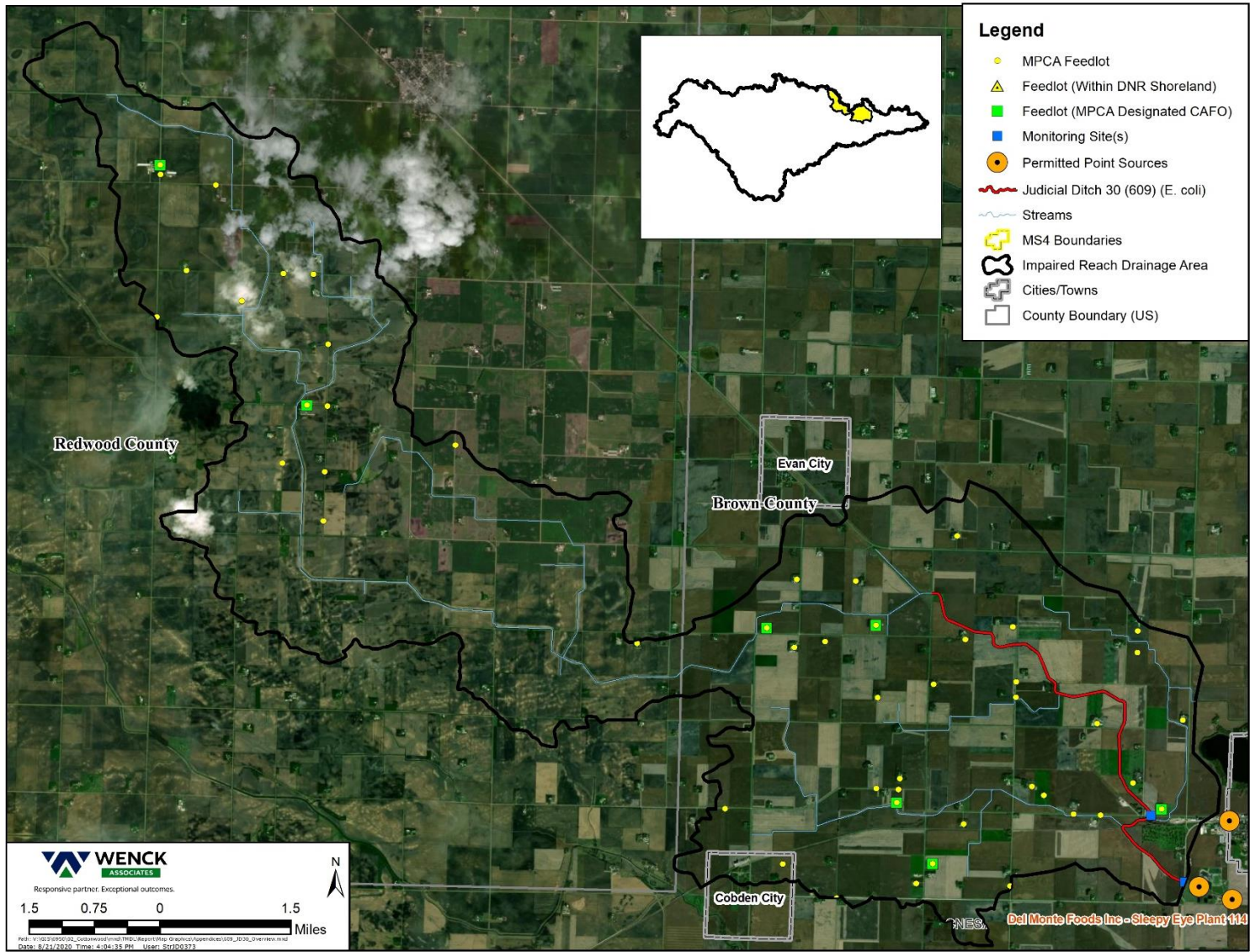


Figure A-50. Judicial Ditch 30 Reach 609 Feedlots.

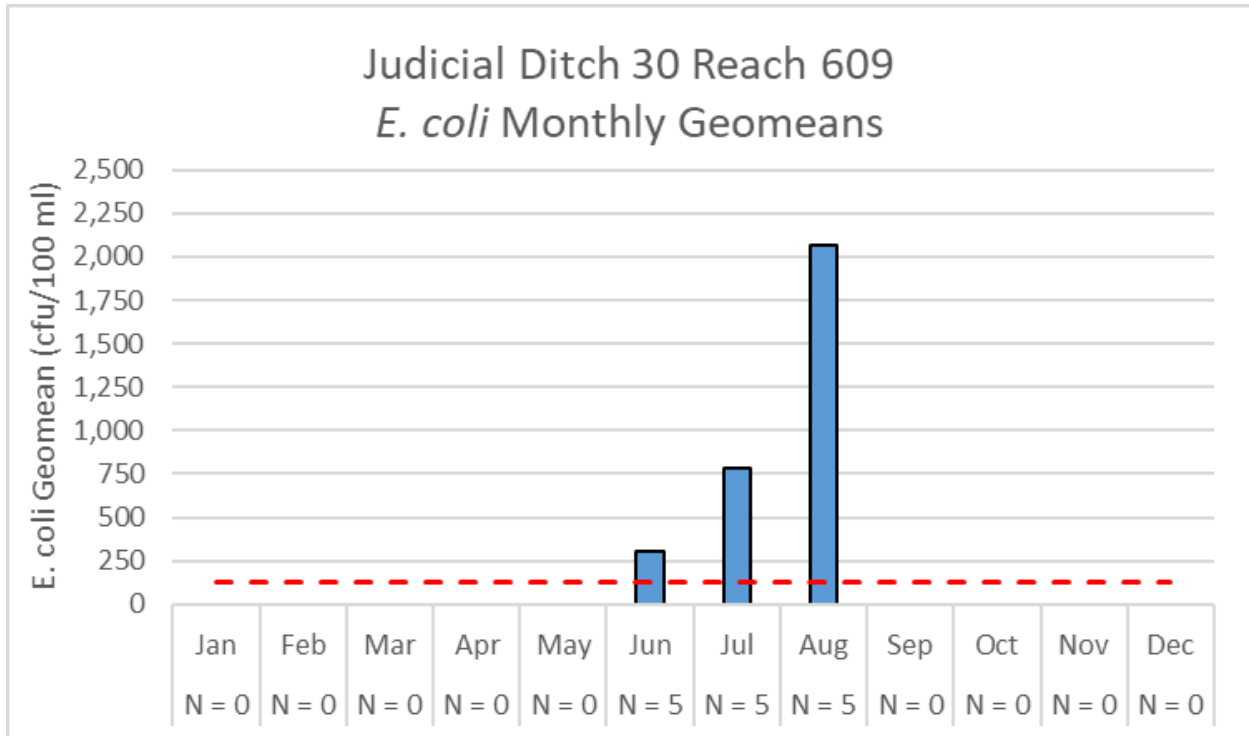


Figure A-51. Judicial Ditch 30 Reach 609 *E. coli* Monthly Geomeans.

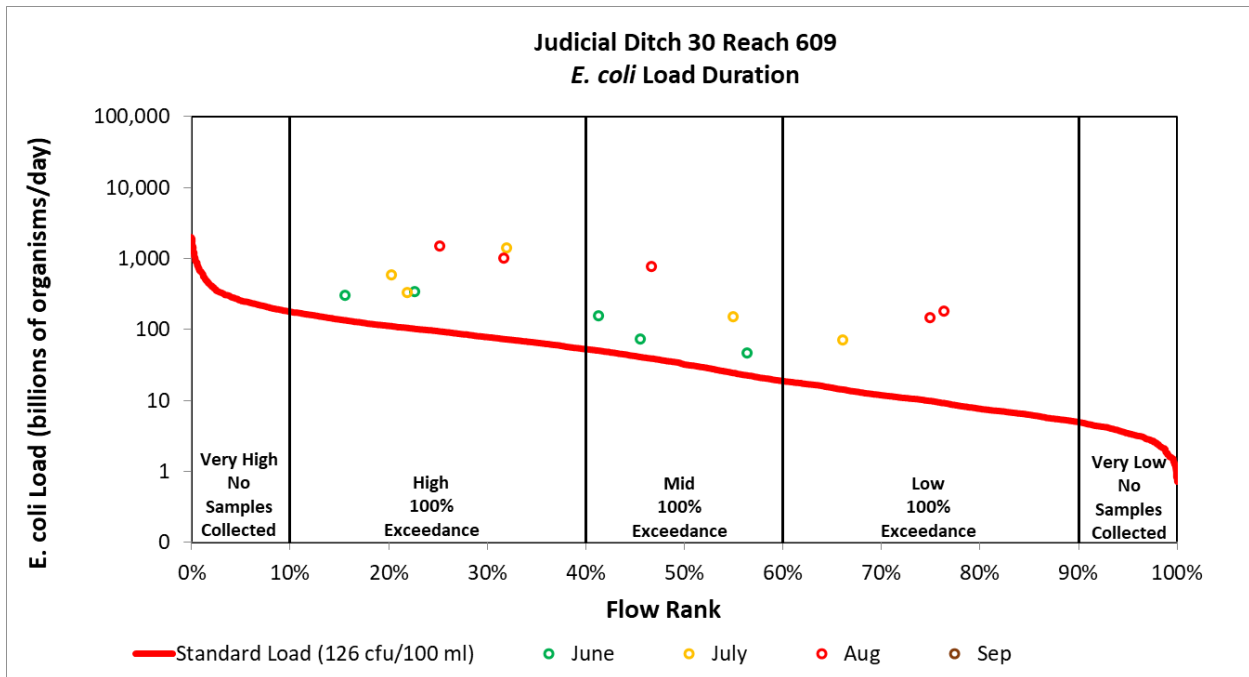


Figure A-52. Judicial Ditch 30 Reach 609 *E. coli* Load Duration Curve (by month).

Table A-8. Judicial Ditch 30 Reach 609 Bacteria Production Exercise.

Major Category	Source	Animal Units* or Individuals in Subwatershed	Fecal Bacteria Organisms Produced Per Unit Per Day	Total Fecal Bacteria Produced Per Day	Total Fecal Bacteria Produced Per Day by Major Category	Percent by Category
			[Billions of Org.] ⁸	[Billions of Org.]	[Billions of Org.]	
Livestock (Surface Applied Manure) ¹	Horse*	4	58.2	233	422,974	99.83%
	Swine*	5,380	32.7	175,910		
	Bovine*	4,241	58.2	246,832		
	Poultry*	-	-	-		
	Other Livestock*, ⁹	0	-	-		
Wildlife	Deer ³	223	0.5	111	378	0.09%
	Waterfowl ⁴	668	0.4	267		
Human	Failing Septic Systems ⁵	19	5.7	110	110	0.03%
	WWTP effluent ⁶	-	-	-		
Domestic Animals ²	Improperly Managed Pet Waste ⁷	262	0.9	239	239	0.06%

* Values reported as Animal Units.

¹ Livestock animal units estimated based on MPCA registered feedlot database with animal units converted based on MN Dept. of Ag conversion units (<http://www.mda.state.mn.us/animals/feedlots/feedlot-dmt/feedlot-dmt-animal-units.aspx>).

² # of households in watershed multiplied by 0.58 dogs/ household and 0.73 cates/household according to the SE MN Regional TMDL (MPCA, 2002)

³ Assumes average deer density of .0078 deer/acre from Monitoring Population Trends of White-tailed Deer in Minnesota (Minnesota DNR, 2013)

⁴ Estimated from the MN DNR and US Fish & Wildlife Service 2018 Waterfowl Breeding Population Survey (Minnesota DNR, 2018)

⁵ based on county SSTS inventory failure rates reported to MPCA (MPCA personal communication, 2018) and rural population estimates (3 persons/ septic) based on 2010 Census blocks.

⁶ Reported as # of facilities with production based on WWTP effluent data from facility discharge monitoring reports (DMRs)

⁷ Estimated that 35% of the bacteria produced per month attributed to pet waste is improperly managed and available for runoff (CWP, 1999)

⁸ Derived from literature rates in Metcalf and Eddy (1991), Horsley and Witten (1996), Alderisio and De Luca (1999), ASAE Standards (1998) and the Southeast Minnesota Regional TMDL (MPCA, 2002). Values have been reported to two significant digits.

⁹ Other cattle include llama, goat, and sheep.

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Supporting Items for Lake Bean (17005400)

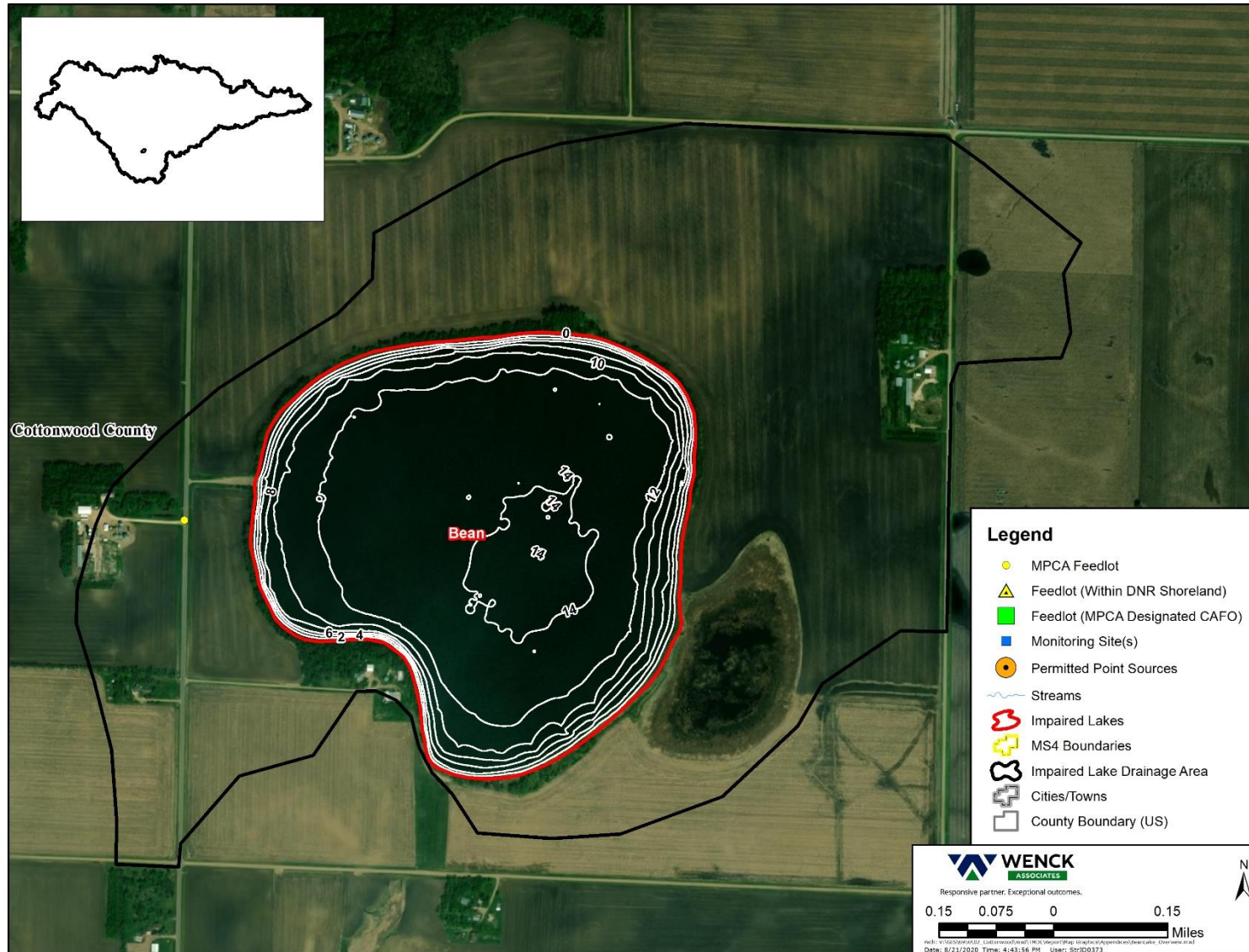


Figure C-1. Lake Bean Overview.

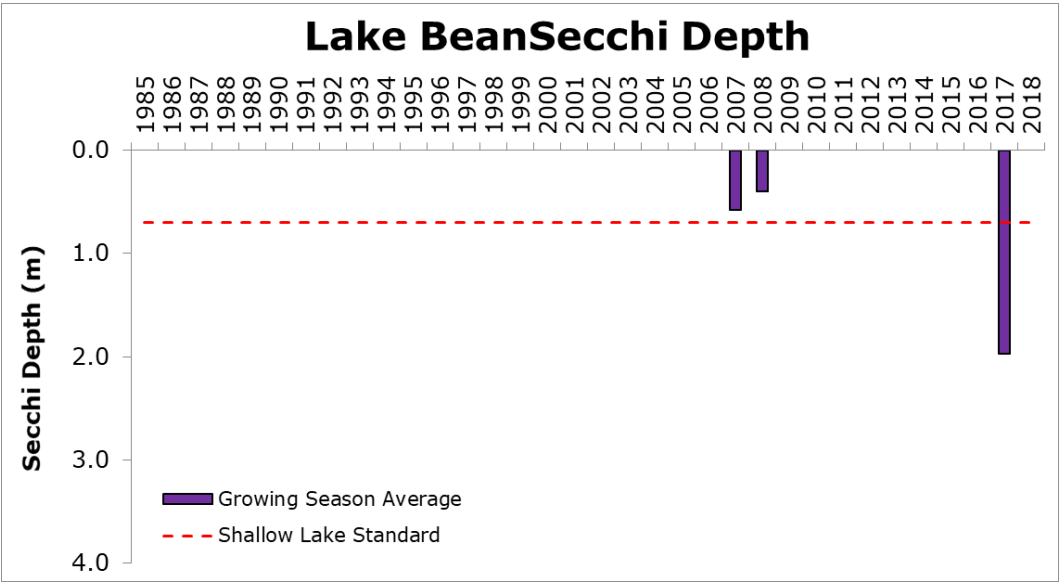
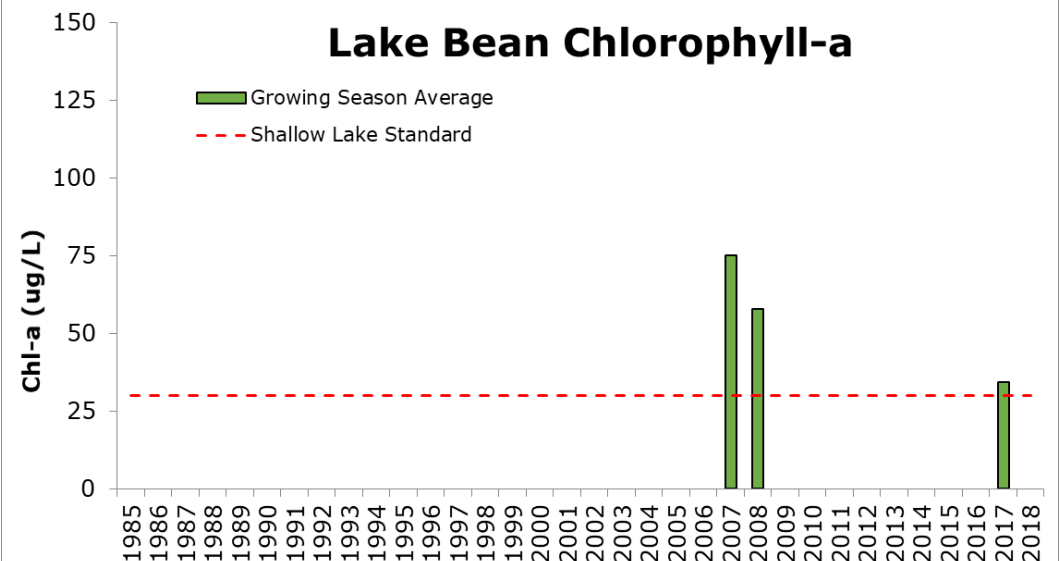
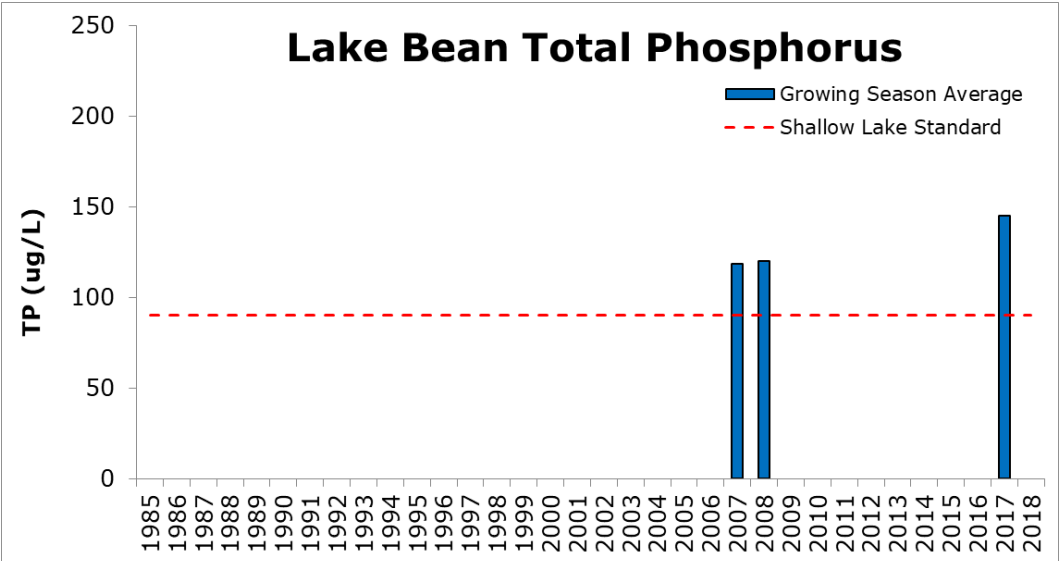


Figure C-2. Lake Bean Historic Water Quality.

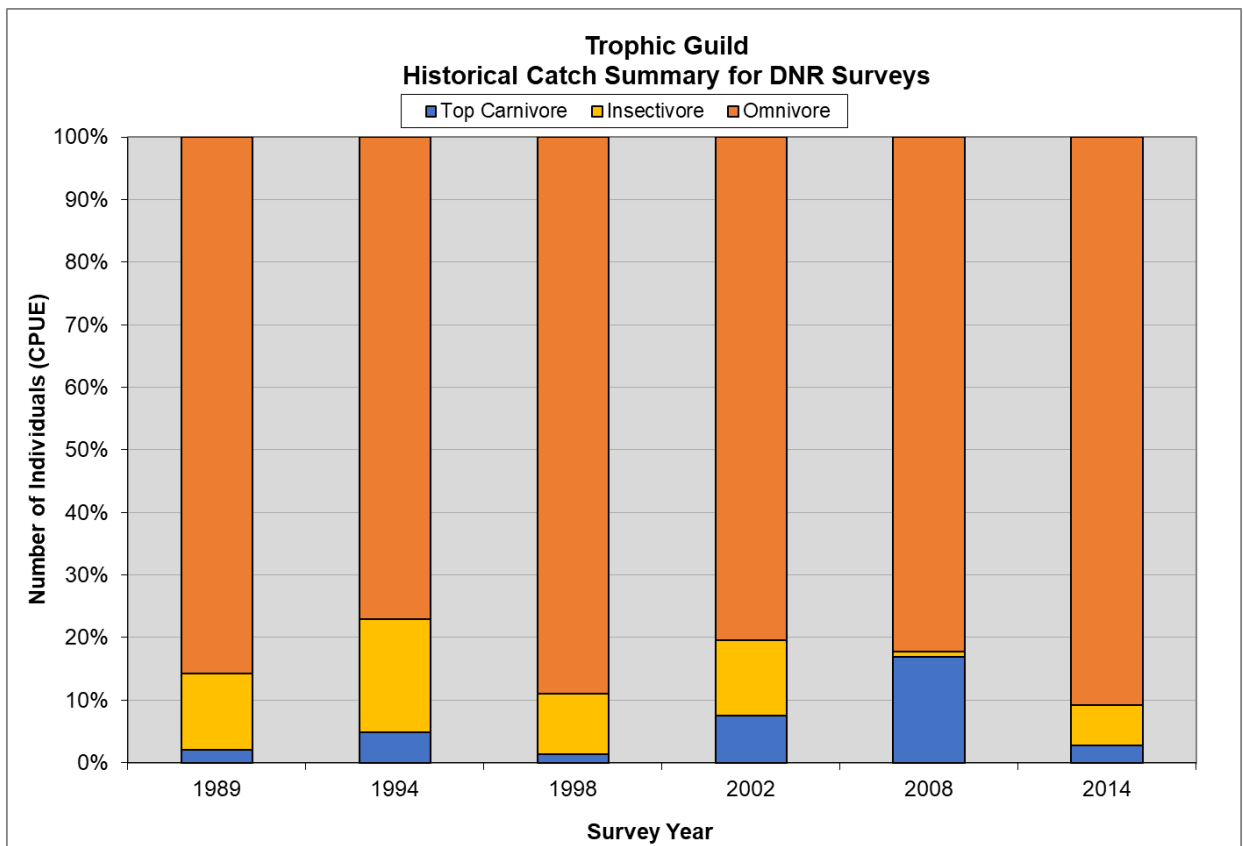


Figure C-3. Lake Bean DNR Fish Survey Historic Catch Summarized by Trophic Guild and Catch Per Unit Effort (CPUE).

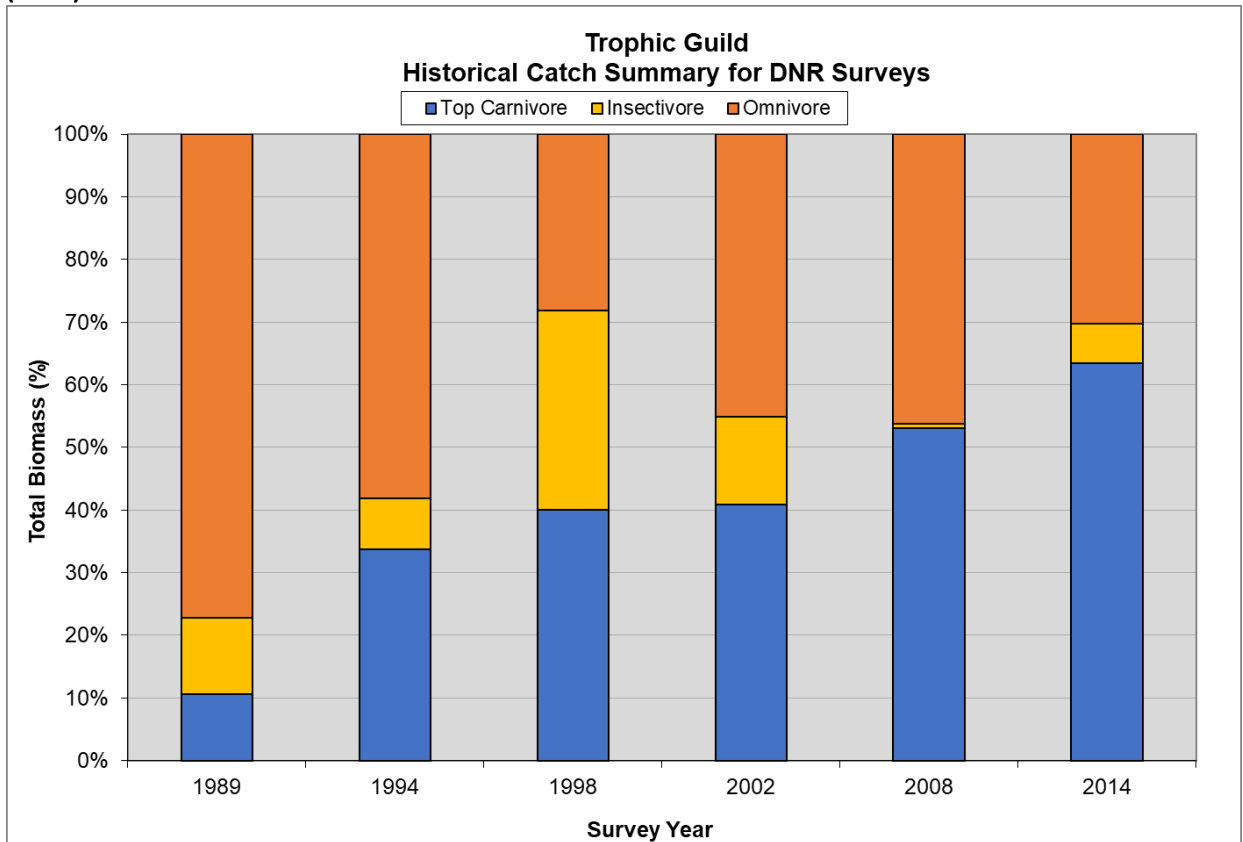


Figure C-4. Lake Bean DNR Fish Survey Historic Catch Summarized by Trophic Guild and Total Biomass.

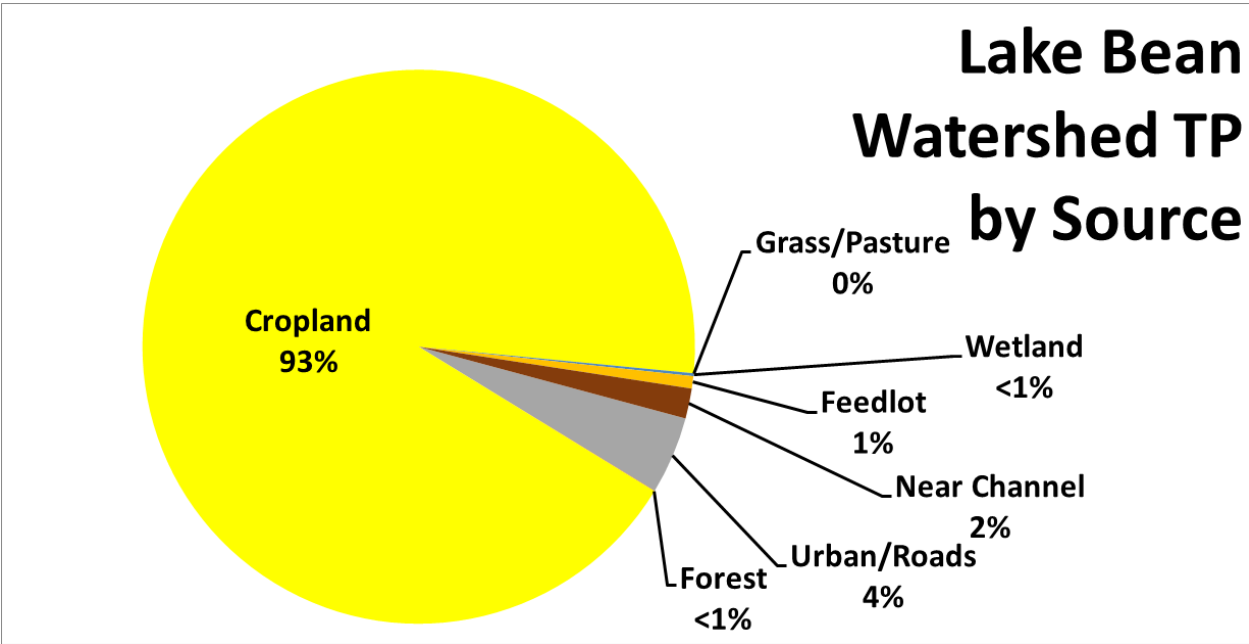


Figure C-5. Lake Bean watershed TP load contribution by source predicted by HSPF.

Table C-1. Lake Bean Current Condition Lake Response Model.

Average Loading Summary for Bean							
Water Budgets				Phosphorus Loading			
Inflow from Drainage Areas							
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load	
	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]	
1	Direct watershed (HSPF 274)	372	18.4	569	211	1.0	326
2							
3							
4							
5							
6							
<i>Summation</i>		372	18	569.03			326
Failing Septic Systems							
	Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]	Load [lb/yr]	
1		0	2	0	0%	3	
2							
3							
4							
5							
<i>Summation</i>		2	0	0.0	12%	3	
Inflow from Upstream Lakes							
	Name		Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]	Load [lb/yr]	
1				-	1.0		
2				-	1.0		
3				-	1.0		
4				-	1.0		
5				-	1.0		
<i>Summation</i>			0.0	-		0.0	
Atmosphere							
	Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]
	164	26.7	26.7	0.00	0.24	1.0	39
Dry-year total P deposition =					0.222		
Average-year total P deposition =					0.239		
Wet-year total P deposition =					0.259		
(Barr Engineering 2004)							
Internal							
	Lake Area [km ²]	Anoxic Factor [days]		Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]	
	0.66	0	Oxic		1.0	0	
	0.66	45.6	Anoxic		1.0	1,192	
<i>Summation</i>						1,192	
Net Discharge [ac-ft/yr] =				569	Net Load [lb/yr] =		
					1,560		

Average Lake Response Modeling for Bean				
Modeled Parameter	Equation	Parameters	Value	[Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION				
$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)			
		C _P =	1.00	[--]
		C _{CB} =	0.162	[--]
		b =	0.458	[--]
	W (total P load = inflow + atm.) =		708	[kg/yr]
	Q (lake outflow) =		0.7	[10 ⁶ m ³ /yr]
	V (modeled lake volume) =		2.3	[10 ⁶ m ³]
	T = V/Q =		3.21	[yr]
	P _i = W/Q =		1008	[ug/l]
Model Predicted In-Lake [TP]			122.4	[ug/l]
Observed In-Lake [TP]			122.4	[ug/l]

Table C-2. Lake Bean TMDL Condition Lake Response Model.

TMDL Loading Summary for Bean						
Water Budgets				Phosphorus Loading		
Inflow from Drainage Areas						
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load
Name	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]
1 Direct watershed (HSPF 274)	372	18.4	569	150	0.7	232
2						
3						
4						
5						
6						
<i>Summation</i>	372	18	569.03			232
Failing Septic Systems						
Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]		Load [lb/yr]
1	0	2	0	0%		1
2						
3						
4						
5						
<i>Summation</i>	2	0	0.0	0%		1
Inflow from Upstream Lakes						
Name		Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]		Load [lb/yr]
1			-	1.0		
2			-	1.0		
3			-	1.0		
4			-	1.0		
5			-	1.0		
<i>Summation</i>			0.0	-		0.0
Atmosphere						
Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]
164	26.7	26.7	0.00	0.24	1.0	39
				Dry-year total P deposition = 0.222		
				Average-year total P deposition = 0.239		
				Wet-year total P deposition = 0.259		
				(Barr Engineering 2004)		
Internal						
Lake Area [km ²]	Anoxic Factor [days]			Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]
0.66	0		Oxic		1.0	0
0.66	45.6		Anoxic		1.0	665
<i>Summation</i>						665
<i>Net Discharge [ac-ft/yr] =</i>			569	<i>Net Load [lb/yr] =</i>		
				937		

TMDL Lake Response Modeling for Bean			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
$P = \frac{P_i}{\left(1 + C_p \times C_{CB} \times \left(\frac{W_p}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)		
		C _p =	1.00 [--]
		C _{CB} =	0.162 [--]
		b =	0.458 [--]
	W (total P load = inflow + atm.) =		425 [kg/yr]
	Q (lake outflow) =		0.7 [10 ⁶ m ³ /yr]
	V (modeled lake volume) =		2.3 [10 ⁶ m ³]
	T = V/Q =		3.21 [yr]
	P _i = W/Q =		606 [ug/l]
Model Predicted In-Lake [TP]			90.0 [ug/l]
Observed In-Lake [TP]			122.4 [ug/l]

Supporting Items for Double (North Portion) Lake (17005601)

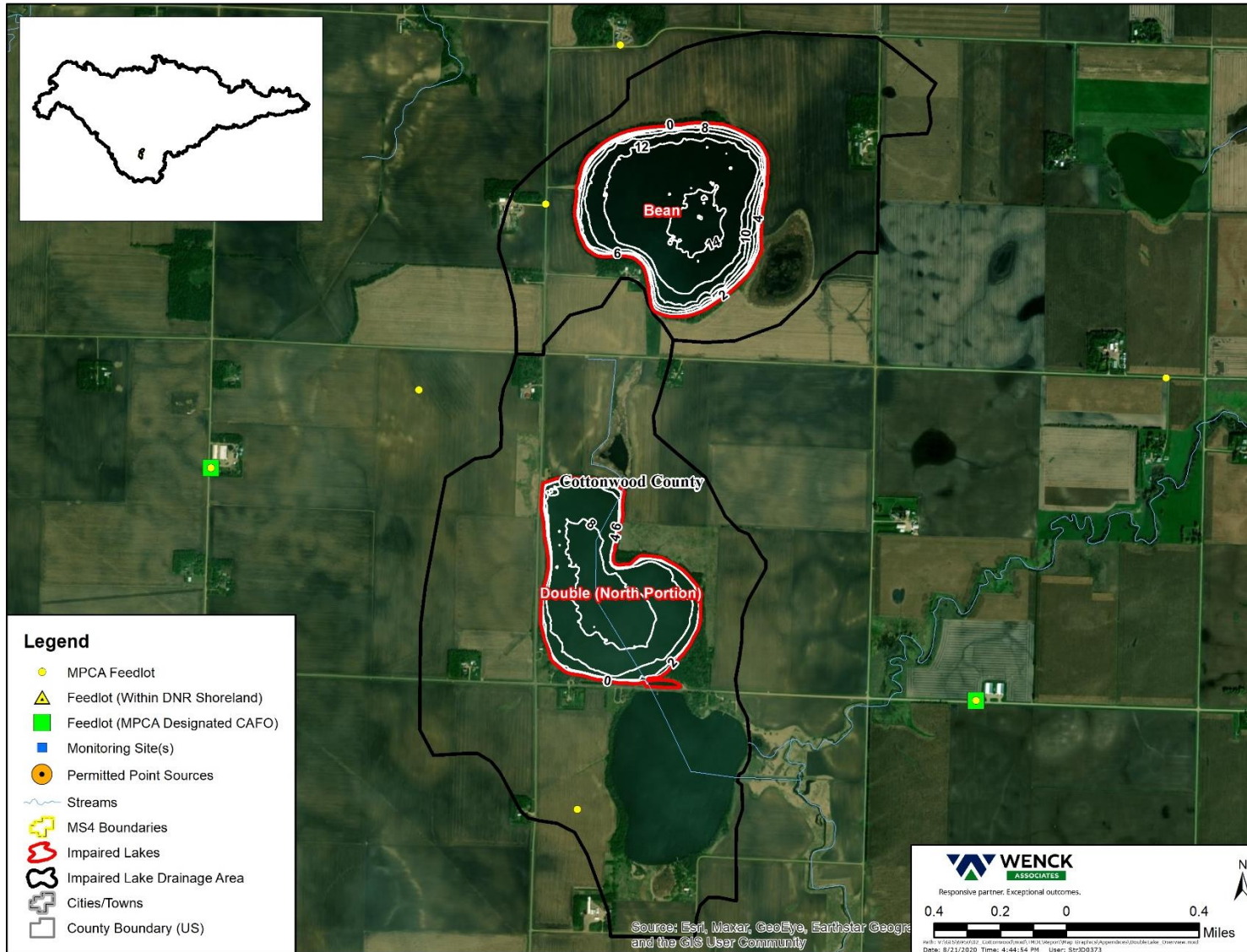


Figure C-6. Double (North Portion) Lake Overview.

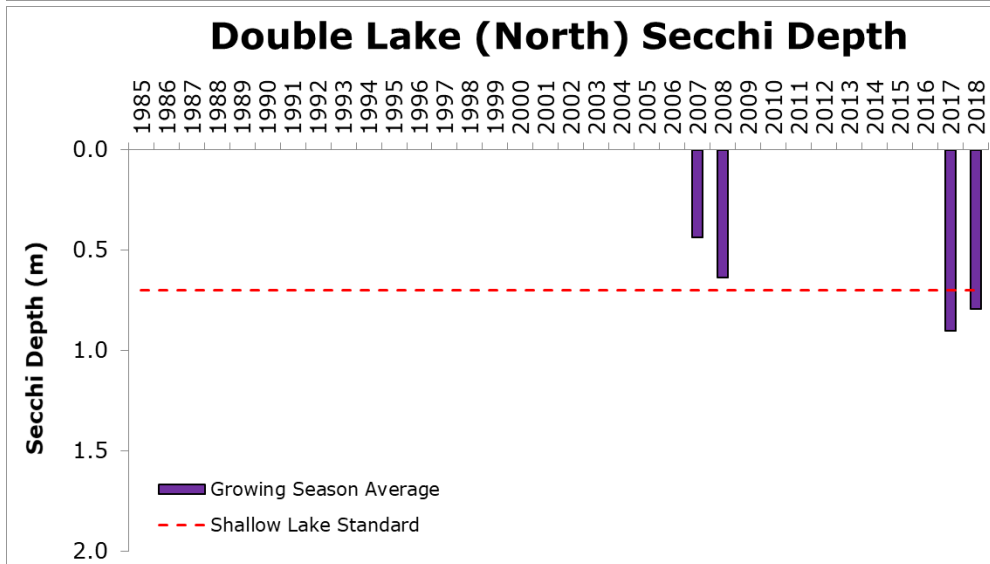
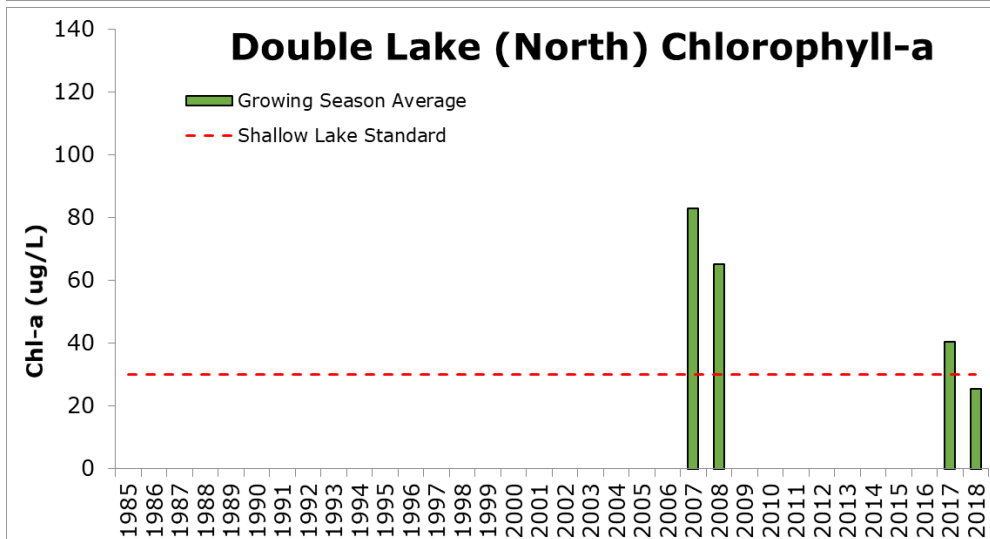
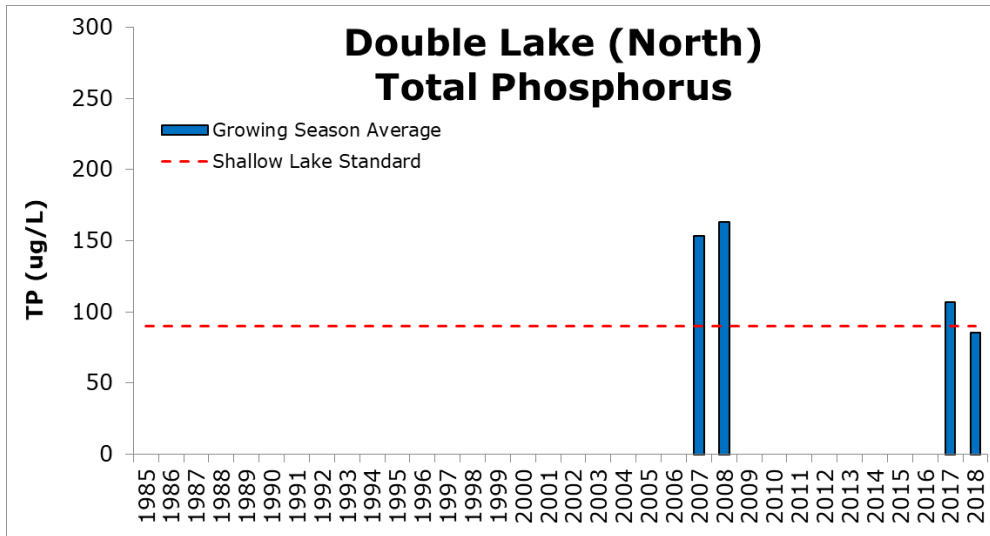


Figure C-7. Double (North Portion) Lake Historic Water Quality.

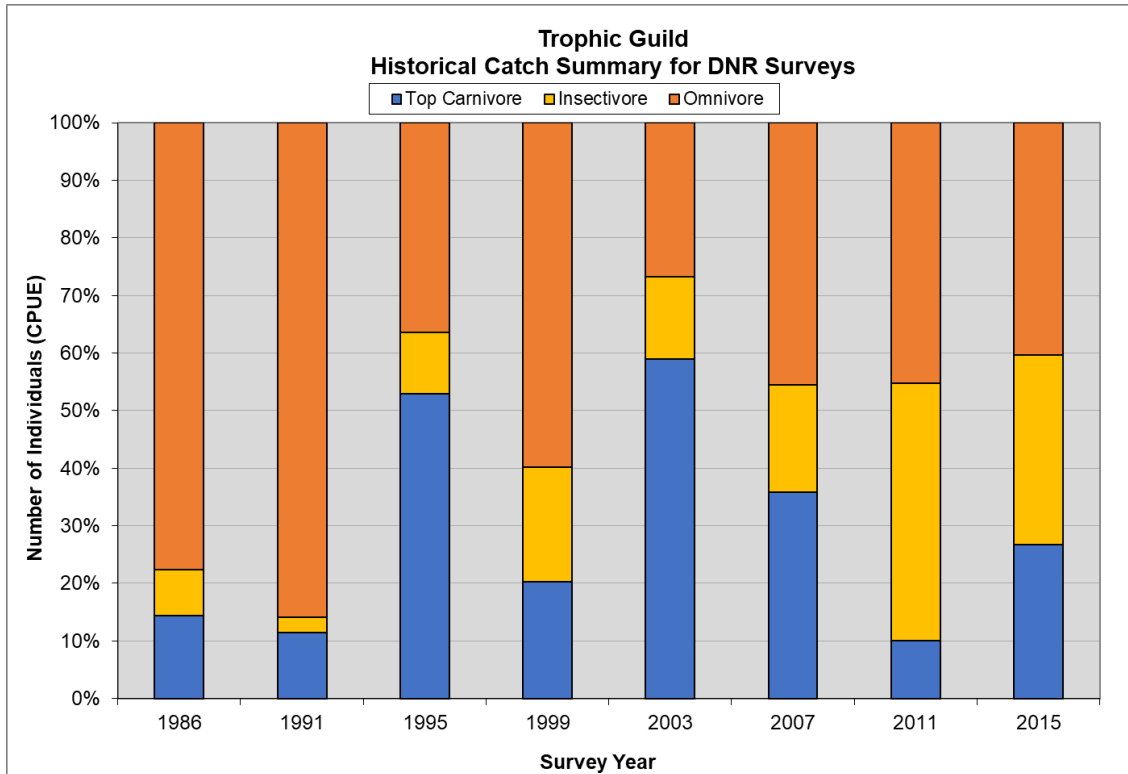


Figure C-8. Double (North Portion) Lake DNR Fish Survey Historic Catch Summarized by Trophic Guild and Catch Per Unit Effort (CPUE).

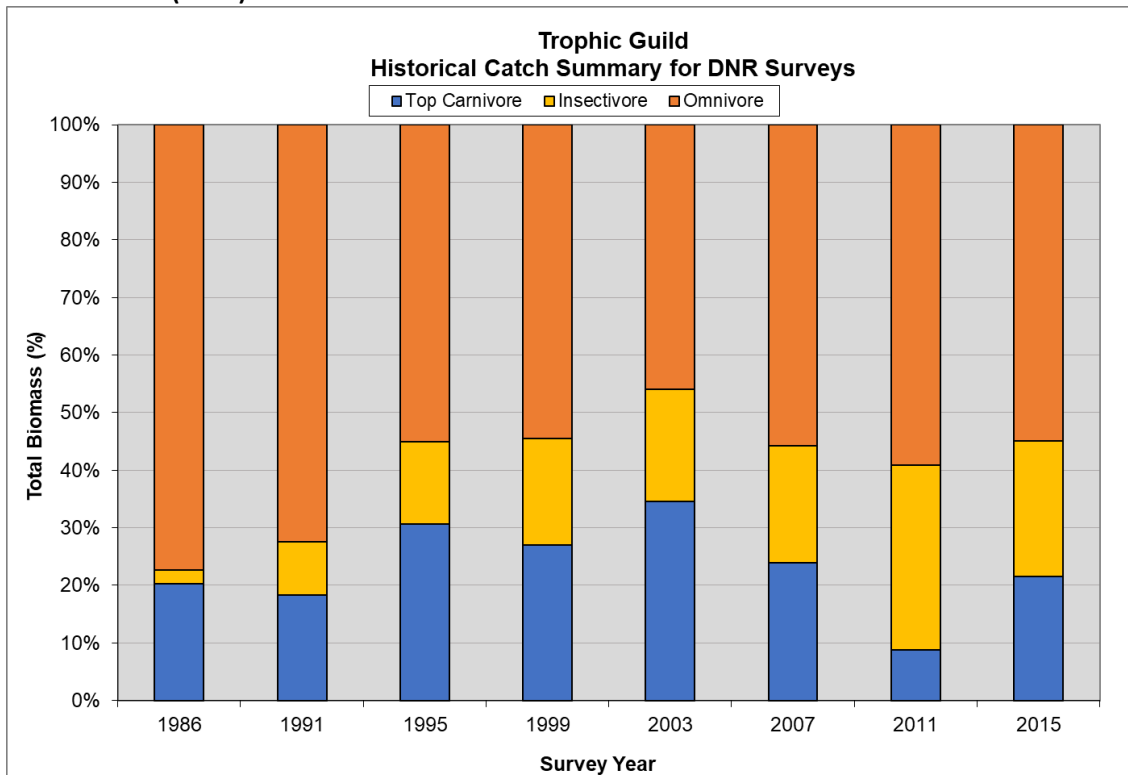


Figure C-9. Double (North Portion) Lake DNR Fish Survey Historic Catch Summarized by Trophic Guild and Total Biomass.

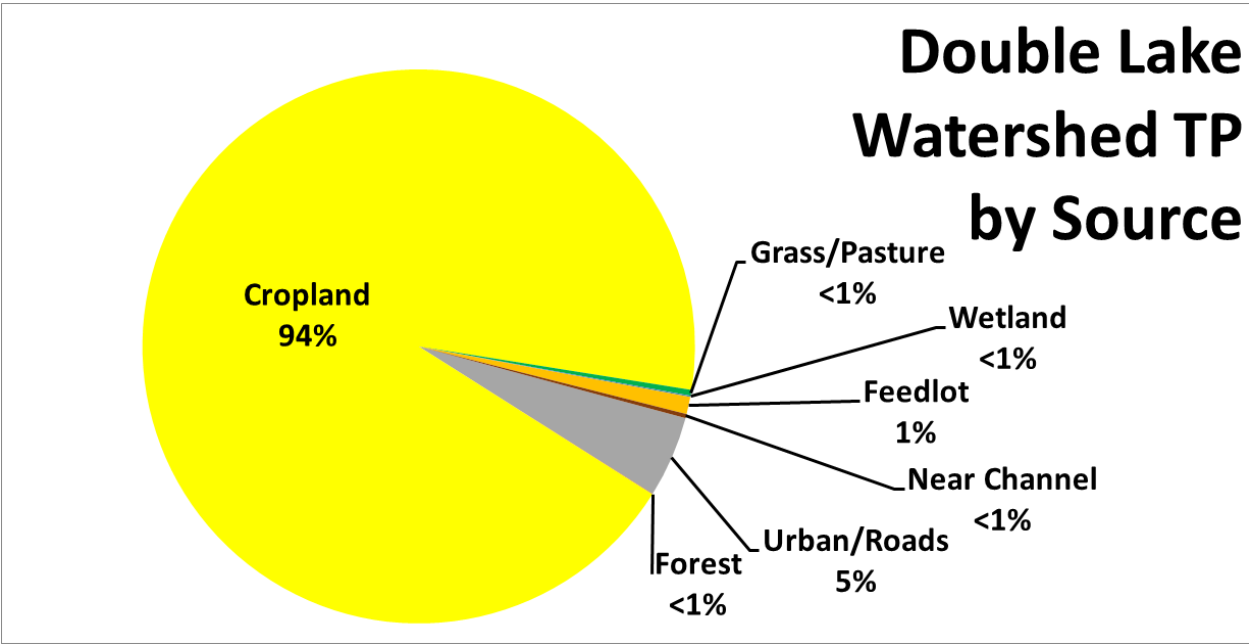


Figure C-10. Double (North Portion) Lake watershed TP load contribution by source predicted by HSPF.

Table C-3. Double (North Portion) Lake Current Condition Lake Response Model.

Average Loading Summary for Double (North)							
Water Budgets				Phosphorus Loading			
Inflow from Drainage Areas							
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load	
	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]	
1	Direct Watershed (HSPF 276)	710	5.3	313	429	1.0	366
2							
3							
4							
5							
6							
	Summation	710	5	313.35			366
Failing Septic Systems							
	Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]	Load [lb/yr]	
1		9	1	0	12%	11	
2							
3							
4							
5							
	Summation	9	1	0.0	12%	11	
Inflow from Upstream Lakes							
	Name		Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]	Load [lb/yr]	
1	Bean		438	122.4	1.0	146	
2							
3							
4							
5							
	Summation		437.7	122.4		146	
Atmosphere							
	Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]
	136	30.1	30.1	0.00	0.24	1.0	33
					Dry-year total P deposition = 0.222		
					Average-year total P deposition = 0.239		
					Wet-year total P deposition = 0.259		
					(Barr Engineering 2004)		
Model Residual Load							
	Name				Loading Calibration Factor (CF) ¹ [--]	Load [lb/yr]	
1	Model Residual Load				1.0	412	
	Summation					412	
Internal							
	Lake Area [km ²]	Anoxic Factor [days]		Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]	
	0.55	0	Oxic		1.0	0	
	0.55	5.0	Anoxic	9.2	1.0	56	
	Summation					56	
			Net Discharge [ac-ft/yr] = 751		Net Load [lb/yr] = 1,023		

Average Lake Response Modeling for Double (North)			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
	$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)	
		C _P =	1.00 [--]
		C _{CB} =	0.162 [--]
		b =	0.458 [--]
		W (total P load = inflow + atm.) =	464 [kg/yr]
		Q (lake outflow) =	0.9 [10 ⁶ m ³ /yr]
		V (modeled lake volume) =	1.1 [10 ⁶ m ³]
		T = V/Q =	1.17 [yr]
		P _i = W/Q =	501 [ug/l]
Model Predicted In-Lake [TP]			124.0 [ug/l]
Observed In-Lake [TP]			124.0 [ug/l]

Table C-4. Double (North Portion) Lake TMDL Condition Lake Response Model.

TMDL Loading Summary for Double (North)						
Water Budgets				Phosphorus Loading		
Inflow from Drainage Areas						
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load
Name	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]
1 Direct Watershed (HSPF 276)	710	5.3	313	150	0.3	128
2						
3						
4						
5						
6						
<i>Summation</i>	710	5	313.35			128
Failing Septic Systems						
Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]		Load [lb/yr]
1	9	0	0	0%		5
2						
3						
4						
5						
<i>Summation</i>	9	0	0.0	0%		5
Inflow from Upstream Lakes						
Name			Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]	Load [lb/yr]
1 Bean			438	90.0	0.7	107
2						
3						
4						
5						
<i>Summation</i>			437.7	90.0		107
Atmosphere						
Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]
136	30.1	30.1	0.00	0.24	1.0	33
				Dry-year total P deposition =	0.222	
				Average-year total P deposition =	0.239	
				Wet-year total P deposition =	0.259	
				(Barr Engineering 2004)		
Model Residual Load						
Name					Loading Calibration Factor (CF) ¹	Load [lb/yr]
1 Model Residual Load					0.7	303
<i>Summation</i>						303
Internal						
Lake Area [km ²]	Anoxic Factor [days]			Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]
0.55	0	Oxic			1.0	0
0.55	5.0	Anoxic		9.2	1.0	56
<i>Summation</i>						56
			Net Discharge [ac-ft/yr] =	751	Net Load [lb/yr] = 632	

Average Lake Response Modeling for Double (North)			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b\right) \times T}$			as f(W,Q,V) from Canfield & Bachmann (1981)
		C _P =	1.00 [--]
		C _{CB} =	0.162 [--]
		b =	0.458 [--]
		W (total P load = inflow + atm.) =	287 [kg/yr]
		Q (lake outflow) =	0.9 [10 ⁶ m ³ /yr]
		V (modeled lake volume) =	1.1 [10 ⁶ m ³]
		T = V/Q =	1.17 [yr]
		P _i = W/Q =	309 [ug/l]
Model Predicted In-Lake [TP]			90.0 [ug/l]
Observed In-Lake [TP]			124.0 [ug/l]

Supporting Items for Rock Lake (42005200)

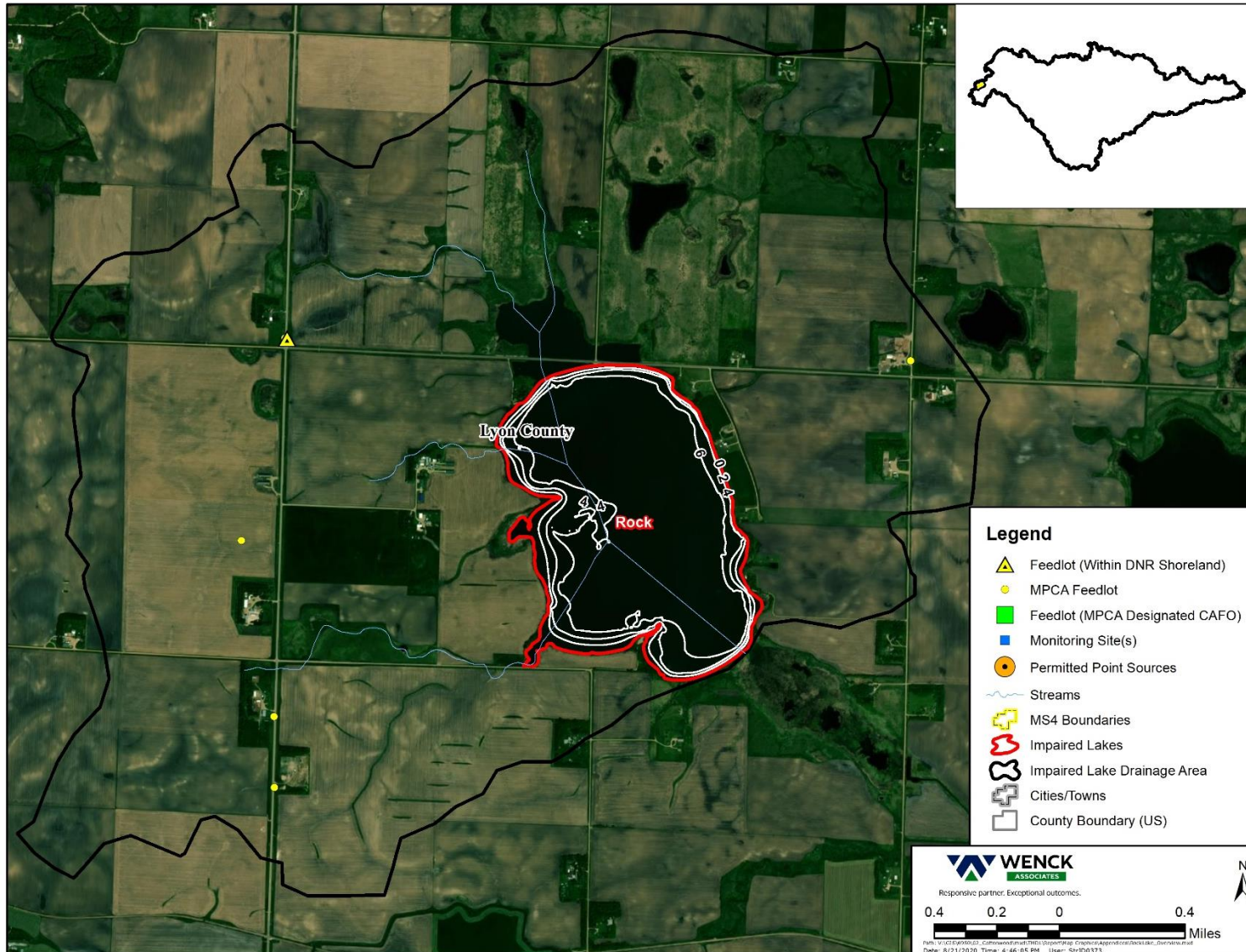


Figure C-11. Rock Lake Overview.

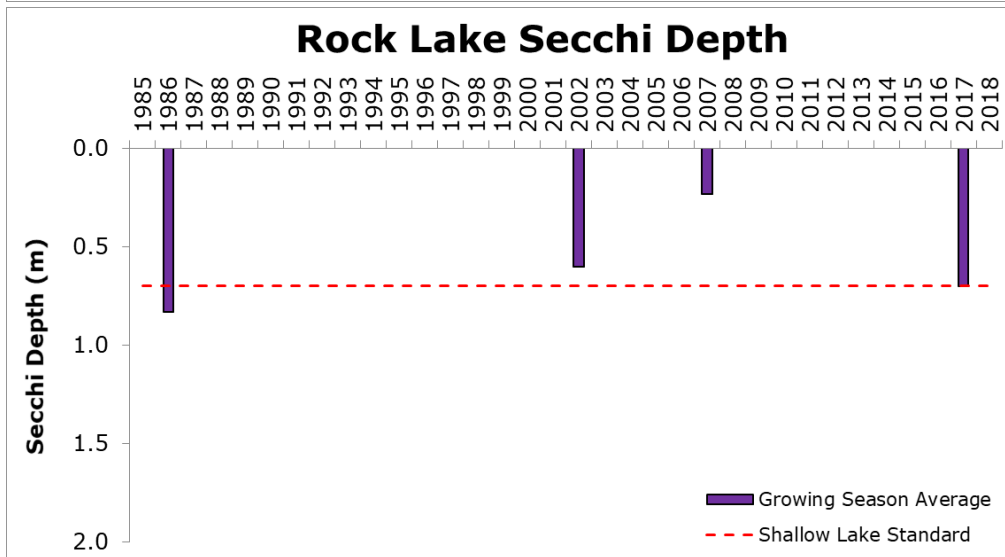
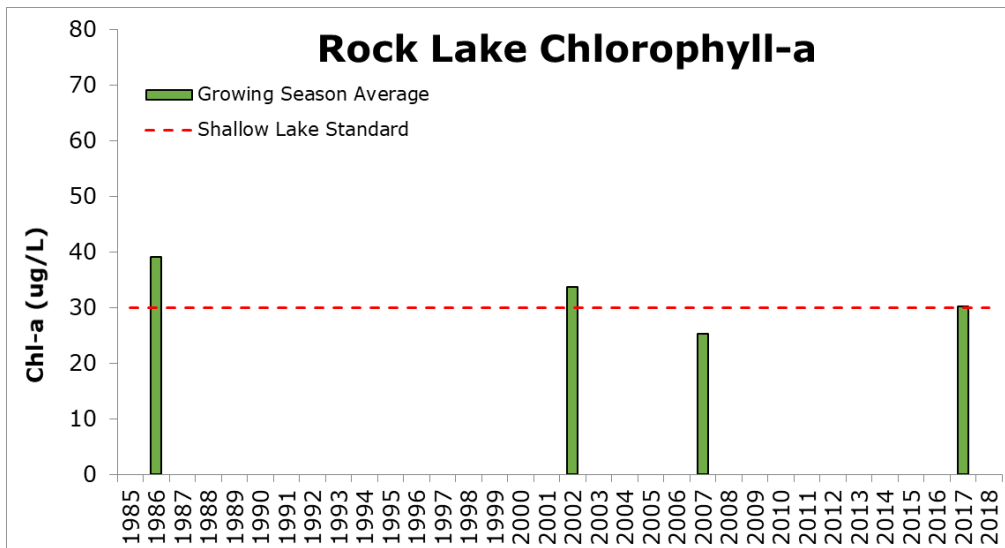
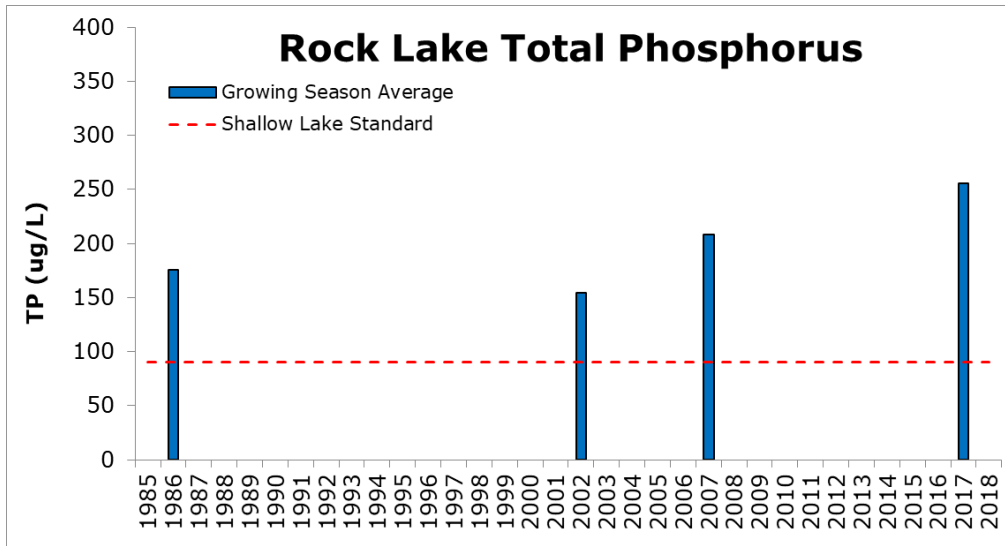


Figure C-12. Rock Lake Historic Water Quality.

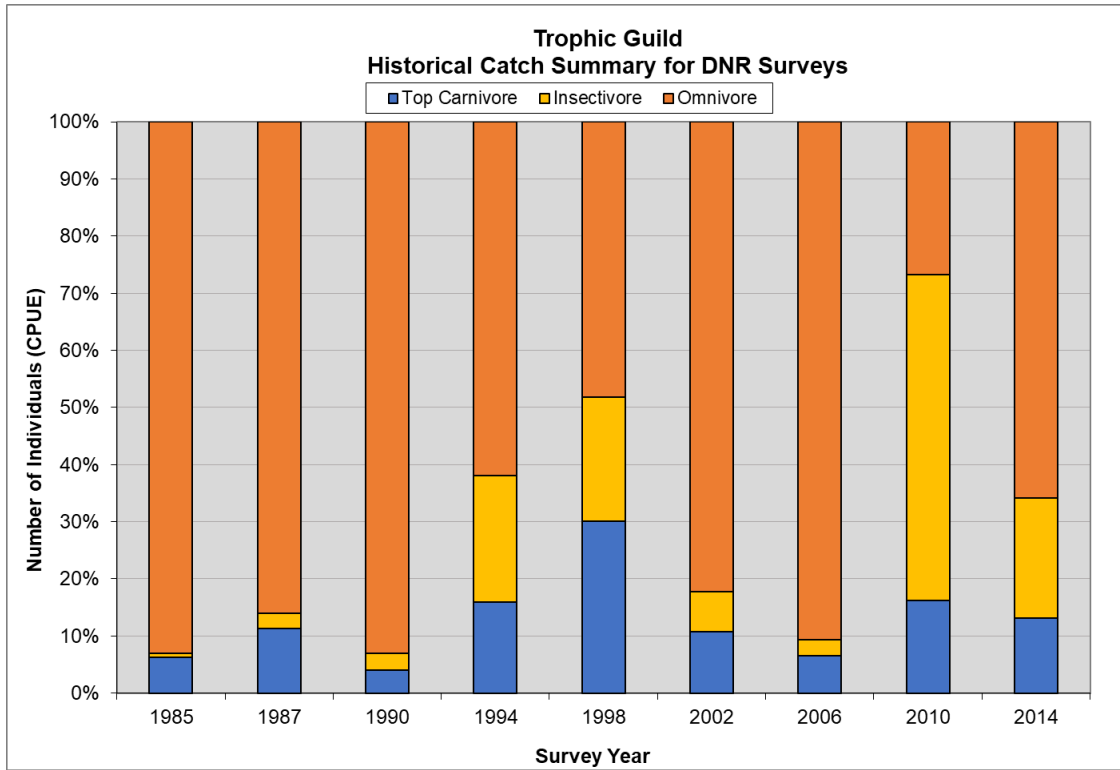


Figure C-13. Rock Lake DNR Fish Survey Historic Catch Summarized by Trophic Guild and Catch Per Unit Effort (CPUE).

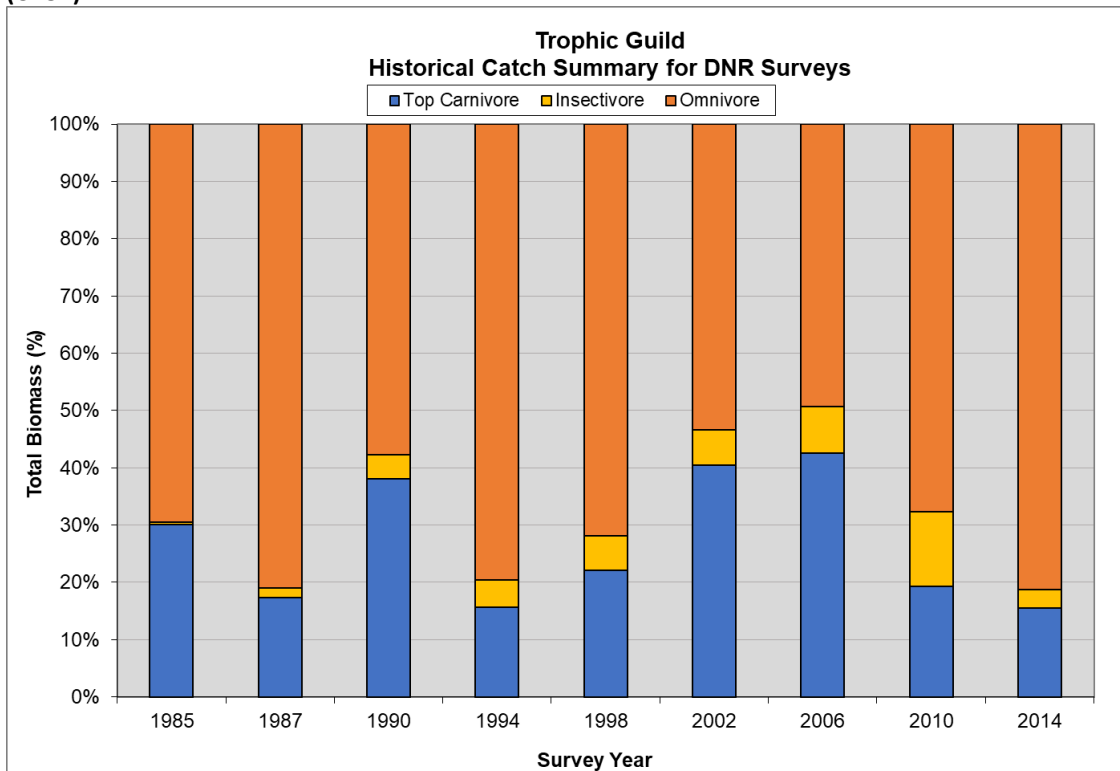


Figure C-14. Rock Lake DNR Fish Survey Historic Catch Summarized by Trophic Guild and Total Biomass.

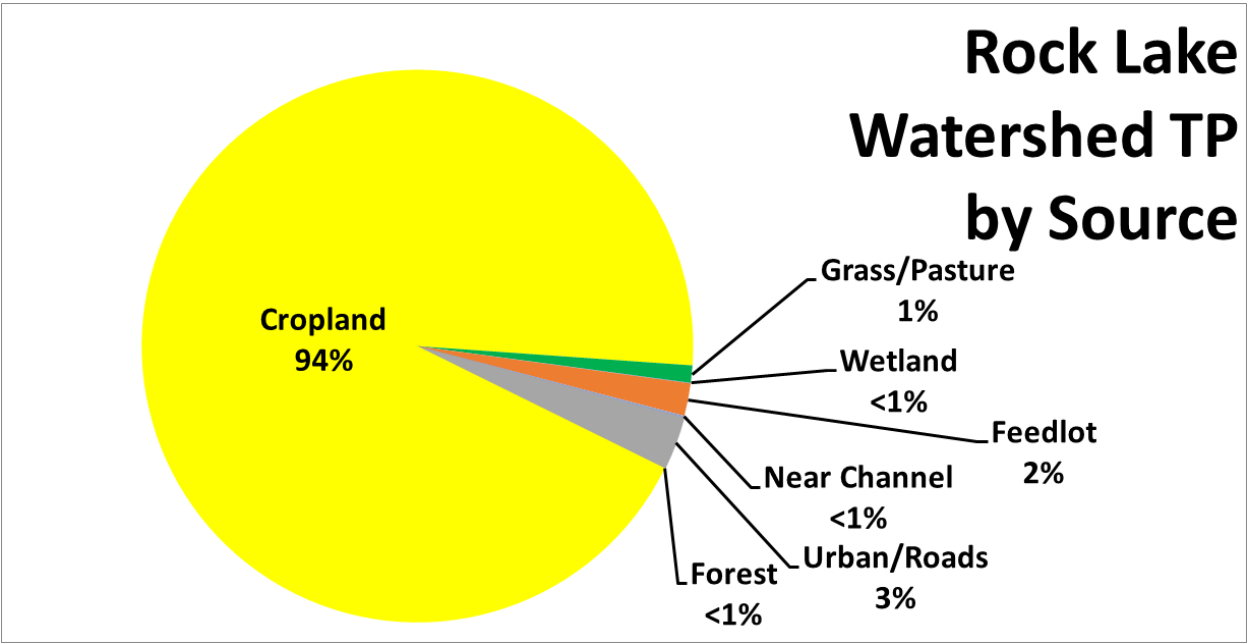


Figure C-15. Rock Lake watershed TP load contribution by source predicted by HSPF.

Table C-5. Rock Lake Current Condition Lake Response Model.

Average Loading Summary for Rock							
Water Budgets				Phosphorus Loading			
Inflow from Drainage Areas							
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load	
	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]	
1	Direct Watershed (HSPF 12)	3,208	8.2	2,190	286	1.0	1,702
2							
3							
4							
5							
6							
Summation		3,208	8	2,190.18			1,702
Failing Septic Systems							
	Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]	Load [lb/yr]	
1		0	16	5	0	33%	15
2							
3							
4							
5							
Summation		16	5	0.0	33%		15
Inflow from Upstream Lakes							
			Discharge	Estimated P Concentration	Calibration Factor	Load	
	Name		[ac-ft/yr]	[ug/L]	[--]	[lb/yr]	
1				-	1.0		
2				-	1.0		
3				-	1.0		
4				-	1.0		
5				-	1.0		
Summation			0.0	-		0.0	
Atmosphere							
	Lake Area	Precipitation	Evaporation	Net Inflow	Aerial Loading Rate	Calibration Factor	Load
	[acre]	[in/yr]	[in/yr]	[ac-ft/yr]	[lb/ac-yr]	[--]	[lb/yr]
	379	27.5	27.5	0.00	0.24	1.0	91
Dry-year total P deposition =					0.222		
Average-year total P deposition =					0.239		
Wet-year total P deposition =					0.259		
(Barr Engineering 2004)							
Internal							
	Lake Area	Anoxic Factor			Release Rate	Calibration Factor	Load
	[km ²]	[days]			[mg/m ² -day]	[--]	[lb/yr]
	1.53	0		Oxic		1.0	0
	1.53	34.3		Anoxic		1.0	3,722
Summation							3,722
Net Discharge [ac-ft/yr] =				2,190	Net Load [lb/yr] = 5,529		

Average Lake Response Modeling for Rock			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)		
		C _P =	1.00 [--]
		C _{CB} =	0.162 [--]
		b =	0.458 [--]
		W (total P load = inflow + atm.) =	2,508 [kg/yr]
		Q (lake outflow) =	2.7 [10 ⁶ m ³ /yr]
		V (modeled lake volume) =	2.4 [10 ⁶ m ³]
		T = V/Q =	0.90 [yr]
		P _i = W/Q =	928 [ug/l]
Model Predicted In-Lake [TP]			206.3 [ug/l]
Observed In-Lake [TP]			206.3 [ug/l]

Table C-6. Rock Lake TMDL Condition Lake Response Model.

TMDL Loading Summary for Rock						
Water Budgets				Phosphorus Loading		
Inflow from Drainage Areas						
Name	Drainage Area [acre]	Runoff Depth [in/yr]	Discharge [ac-ft/yr]	Phosphorus Concentration [ug/L]	Loading Calibration Factor (CF) ¹ [--]	Load [lb/yr]
1 Direct Watershed (HSPF 12)	3,208	8.2	2,190	150	0.5	894
2						
3						
4						
5						
6						
Summation			3,208	8	2,190.18	894
Failing Septic Systems						
Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]		Load [lb/yr]
1	0	16	0	0%		9
2						
3						
4						
5						
Summation			16	0	0.0	9
Inflow from Upstream Lakes						
Name		Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]		Load [lb/yr]
1			-	1.0		
2			-	1.0		
3			-	1.0		
4			-	1.0		
5			-	1.0		
Summation			0.0	-		0.0
Atmosphere						
Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]
379	27.5	27.5	0.00	0.24	1.0	91
Dry-year total P deposition =				0.222		
Average-year total P deposition =				0.239		
Wet-year total P deposition =				0.259		
				(Barr Engineering 2004)		
Internal						
Lake Area [km ²]	Anoxic Factor [days]			Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]
1.53	0		Oxic		1.0	0
1.53	34.3		Anoxic		1.0	605
Summation						605
Net Discharge [ac-ft/yr] =			2,190	Net Load [lb/yr] =		1,599

TMDL Lake Response Modeling for Rock			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)		
		C _P =	1.00 [--]
		C _{CB} =	0.162 [--]
		b =	0.458 [--]
	W (total P load = inflow + atm.) =		725 [kg/yr]
	Q (lake outflow) =		2.7 [10 ⁶ m ³ /yr]
	V (modeled lake volume) =		2.4 [10 ⁶ m ³]
	T = V/Q =		0.90 [yr]
	P _i = W/Q =		268 [µg/l]
Model Predicted In-Lake [TP]			90.0 [ug/l]
Observed In-Lake [TP]			206.3 [ug/l]

Supporting Items for Sleepy Eye Lake (08004500)

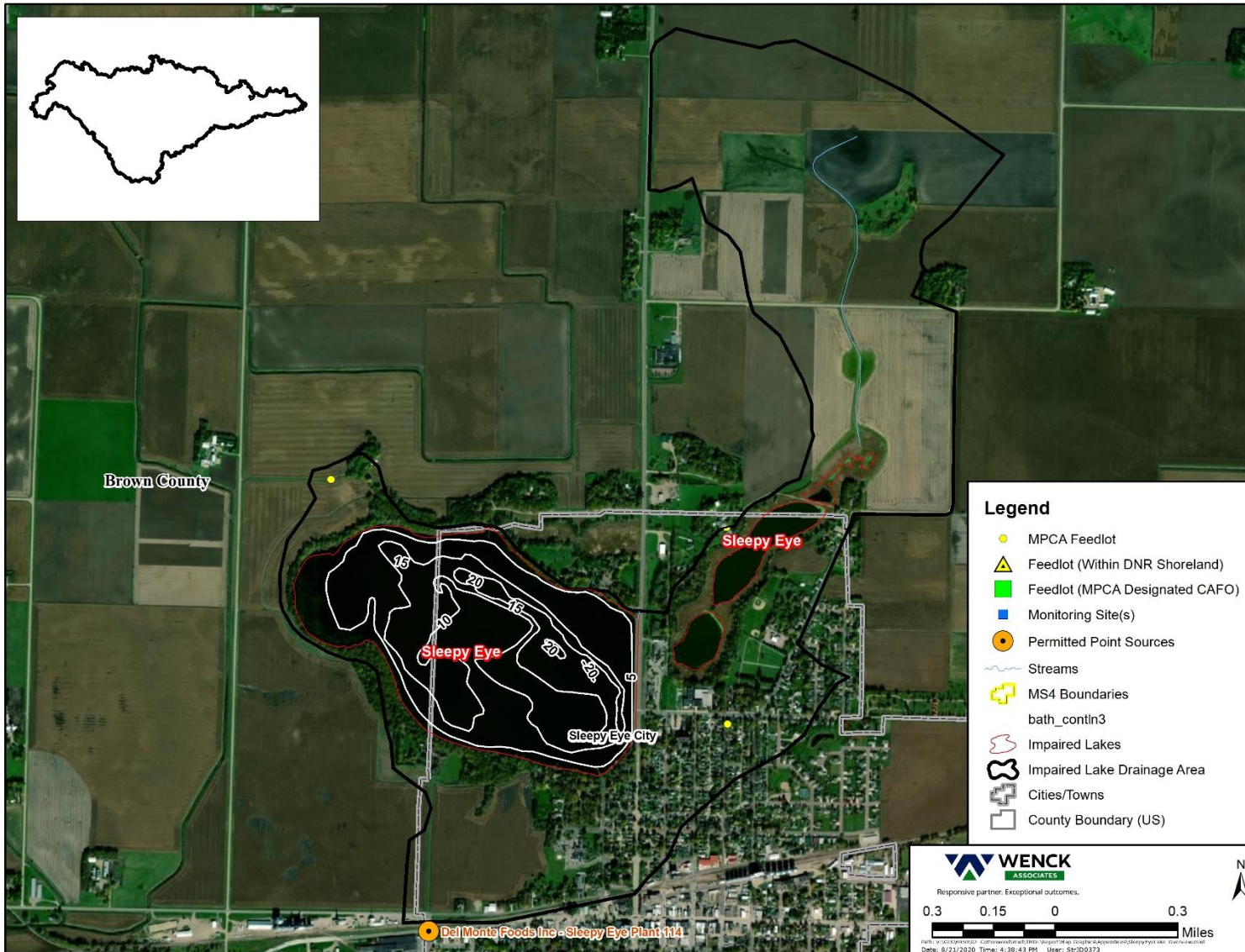


Figure C-16. Sleepy Eye Lake Overview.

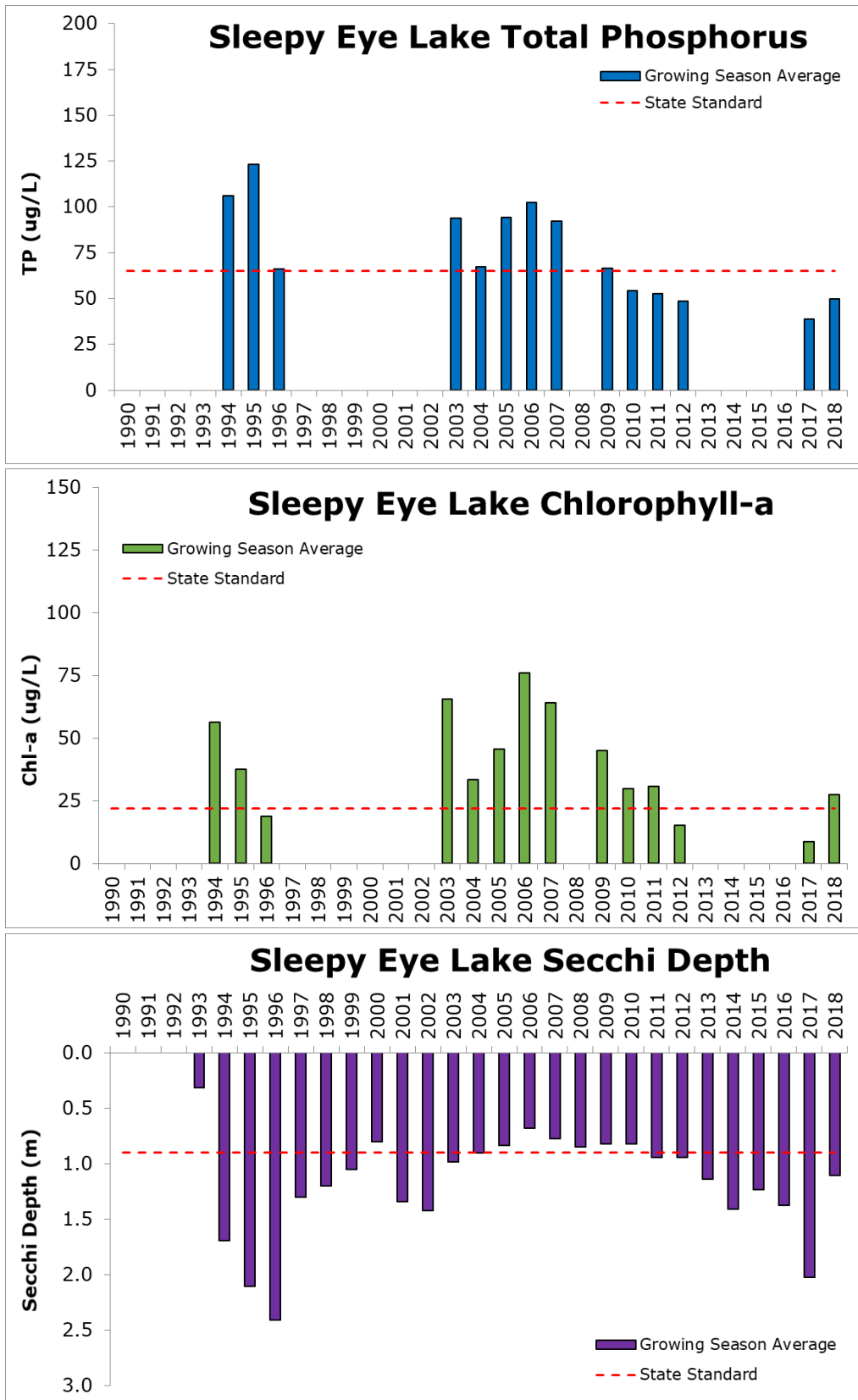


Figure C-17. Sleepy Eye Lake Historic Water Quality.

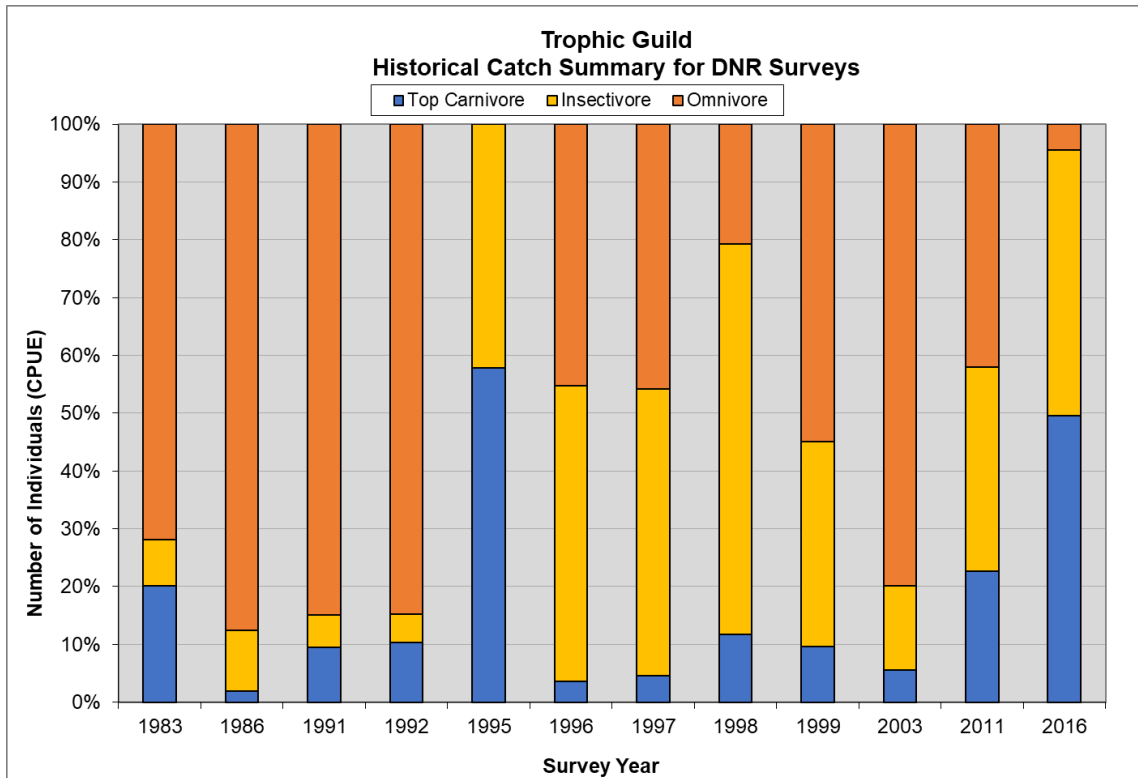


Figure C-18. Sleepy Eye Lake DNR Fish Survey Historic Catch Summarized by Trophic Guild and Catch Per Unit Effort (CPUE).

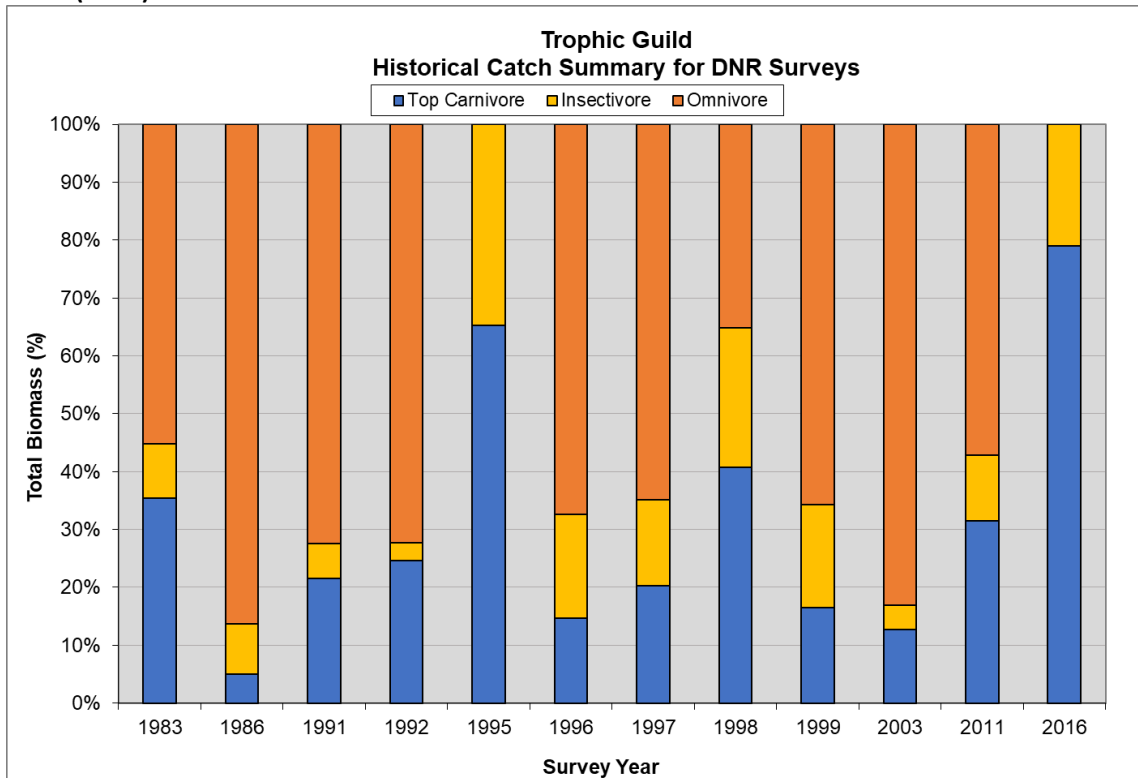


Figure C-19. Sleepy Eye Lake DNR Fish Survey Historic Catch Summarized by Trophic Guild and Total Biomass.

Table C-7. Sleepy Eye Lake summer growing season averages for each water quality parameter.

Lake Name	"Average" Condition Calculation Years	In-Lake Average Condition [Calculated June – September]		
		TP Concentration [µg/L]	Chl- <i>a</i> Concentration [µg/L]	Secchi Depth [m]
WCBP Ecoregion 2B Lake Standards		65	22	0.9
Sleepy Eye	2003-2007*, 2009-2012*, 2017-2018	69	40	1.0

*Data from these years not currently available in EDA database. This data was collected by St. Mary's High School and was analyzed by MVTL Laboratories in New Ulm, MN.

Table C-8. Sleepy Eye Lake (08-0045-00) phosphorus TMDL.

Phosphorus		Existing TP load*		Allowable TP load		Estimated load reduction	
Sources		lbs/year	lbs/day	lbs/year	lbs/day	lbs/year**	%
Wasteload	Construction/Industrial SW	0.8	0.002	0.8	0.002	0.0	0%
	Total WLA	0.8	0.002	0.8	0.002	0.0	0%
Load	Watershed runoff	537.3	1.471	407.2	1.115	130.1	24%
	SSTS	0.0	0.000	0.0	0.000	0.0	0%
	Atmospheric deposition	50.7	0.139	50.7	0.139	0.0	0%
	Internal load	117.7	0.322	117.7	0.322	0.0	0%
	Total LA	705.7	1.932	575.6	1.576	130.1	18%
MOS				64.0	0.175		
Total load		706.5	1.934	640.4	1.753	130.1	9%

* Model calibration year(s): 2003-2007, 2009-2012 and 2017-2018

** Net reduction from current load to TMDL is 66.1 lbs/yr; but the gross load reduction from all sources must accommodate the MOS as well, and hence is 66.1 + 64.0 = 130.1 lbs/yr.

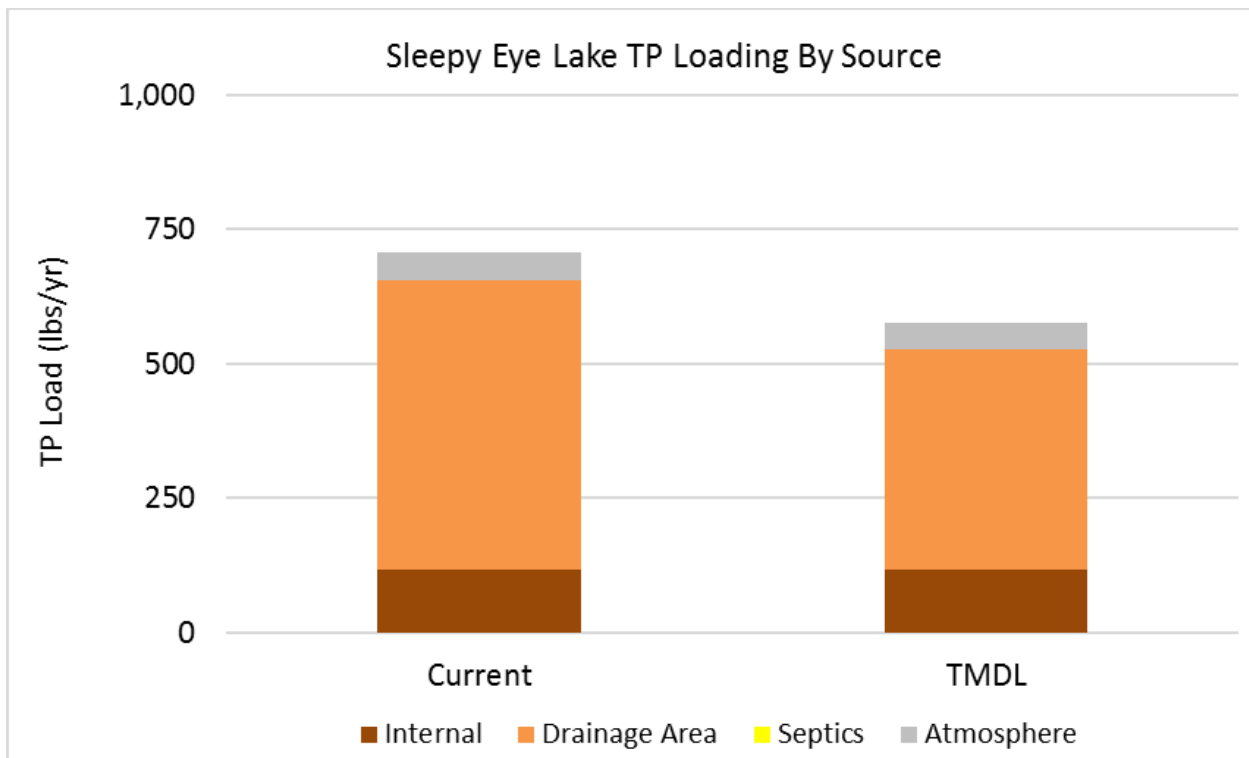


Figure C-20. Sleepy Eye Lake phosphorus source reductions to meet TMDL.

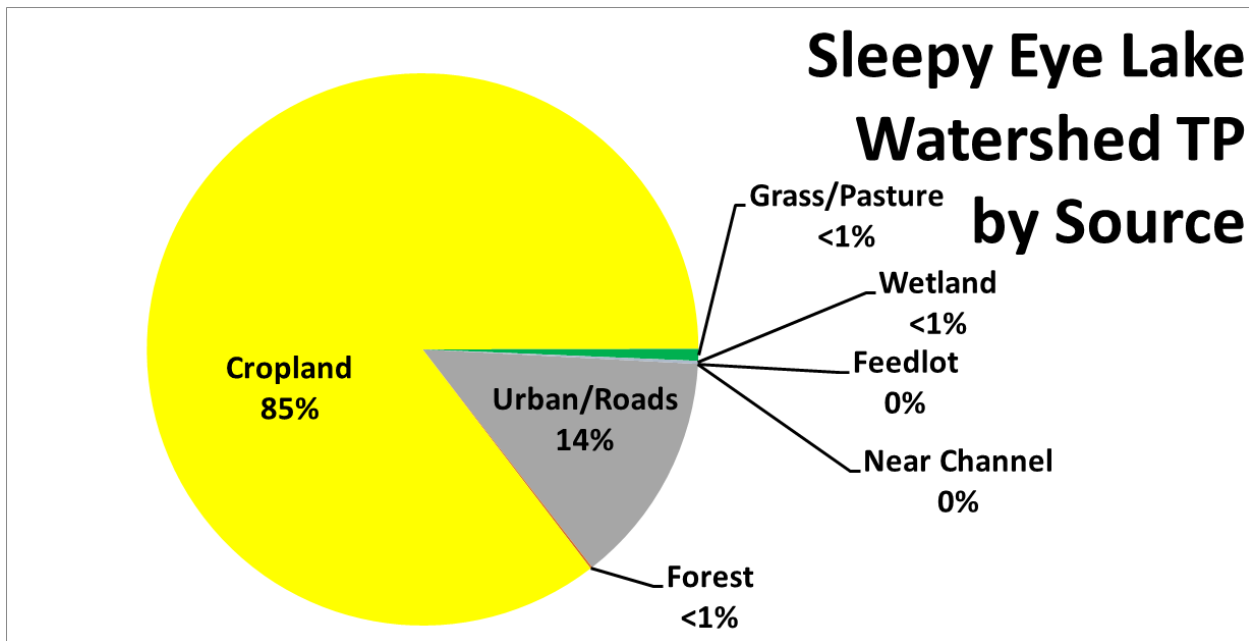


Figure C-21. Sleepy Eye Lake watershed TP load contribution by source predicted by HSPF.

Table C-9. Sleepy Eye Lake Current Condition Lake Response Model.

Average Loading Summary for Sleepy Eye						
Water Budgets				Phosphorus Loading		
Inflow from Drainage Areas						
Name	Drainage Area [acre]	Runoff Depth [in/yr]	Discharge [ac-ft/yr]	Phosphorus Concentration [ug/L]	Loading Calibration Factor (CF) ¹ [--]	Load [lb/yr]
1 Direct Watershed (434)	747	10.4	650	304	1.0	538
2						
3						
4						
5						
6						
Summation		747	10	649.88		538
Failing Septic Systems						
Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]		Load [lb/yr]
1	0	0	0	0%		0
2						
3						
4						
5						
Summation		0	0	0.0	#DIV/0!	0.0
Inflow from Upstream Lakes						
Name			Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]	Load [lb/yr]
1				-	1.0	
2				-	1.0	
3				-	1.0	
4				-	1.0	
5				-	1.0	
Summation			0.0	-		0.0
Atmosphere						
Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]
212	29.8	29.8	0.00	0.24	1.0	51
Dry-year total P deposition =				0.222		
Average-year total P deposition =				0.239		
Wet-year total P deposition =				0.259		
(Barr Engineering 2004)						
Internal						
Lake Area [km ²]	Anoxic Factor [days]			Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]
0.86	0		Oxic		1.0	0
0.86	14.4		Anoxic	4.3	1.0	118
Summation						118
Net Discharge [ac-ft/yr] =			650	Net Load [lb/yr] =		706

Average Lake Response Modeling for Sleepy Eye			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)		
		C _P =	1.05 [--]
		C _{CB} =	0.162 [--]
		b =	0.458 [--]
	W (total P load = inflow + atm.) =		320 [kg/yr]
	Q (lake outflow) =		0.8 [10 ⁶ m ³ /yr]
	V (modeled lake volume) =		2.4 [10 ⁶ m ³]
	T = V/Q =		2.99 [yr]
	P _i = W/Q =		400 [ug/l]
Model Predicted In-Lake [TP]			69.1 [ug/l]
Observed In-Lake [TP]			69.1 [ug/l]

Table C-10. Sleepy Eye Lake TMDL Condition Lake Response Model.

TMDL Loading Summary for Sleepy Eye							
Water Budgets				Phosphorus Loading			
Inflow from Drainage Areas							
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load	
Name	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]	
1 Direct Watershed (434)	747	10.4	650	267	0.9	472	
2							
3							
4							
5							
6							
Summation	747	10	649.88			472	
Failing Septic Systems							
Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]	Load [lb/yr]		
1	0	0	0	0%	0		
2							
3							
4							
5							
Summation	0	0	0.0	#DIV/0!	0.0		
Inflow from Upstream Lakes							
Name	Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]	Load [lb/yr]			
1		-	1.0				
2		-	1.0				
3		-	1.0				
4		-	1.0				
5		-	1.0				
Summation		0.0	-	0.0			
Atmosphere							
Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]	
212	29.8	29.8	0.00	0.24	1.0	51	
Dry-year total P deposition =				0.222			
Average-year total P deposition =				0.239			
Wet-year total P deposition =				0.259			
(Barr Engineering 2004)							
Internal							
Lake Area [km ²]	Anoxic Factor [days]	Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]			
0.86	0	Oxic	1.0	0			
0.86	14.4	Anoxic	1.0	118			
Summation				118			
Net Discharge [ac-ft/yr] =			650	Net Load [lb/yr] =		640	

TMDL Lake Response Modeling for Sleepy Eye				
Modeled Parameter	Equation	Parameters	Value	[Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION				
	$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)		
		C _P =	1.05	[--]
		C _{CB} =	0.162	[--]
		b =	0.458	[--]
		W (total P load = inflow + atm.) =	290	[kg/yr]
		Q (lake outflow) =	0.8	[10 ⁶ m ³ /yr]
		V (modeled lake volume) =	2.4	[10 ⁶ m ³]
		T = V/Q =	2.99	[yr]
		P _i = W/Q =	362	[ug/l]
Model Predicted In-Lake [TP]			65.0	[ug/l]
Observed In-Lake [TP]			69.1	[ug/l]

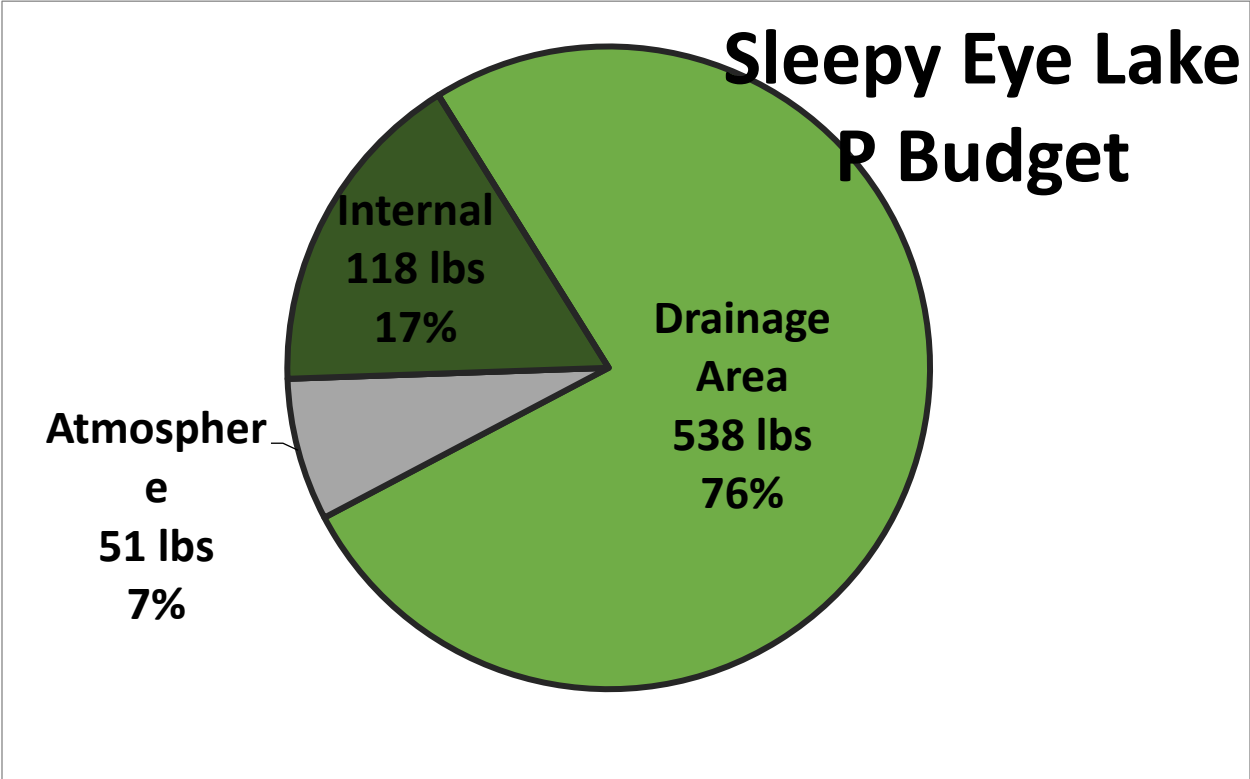


Table C-11. Sleepy Eye Lake average annual TP contributions by source based on HSPF and lake response modeling results.

Supporting Items for Clear Lake (08001100)

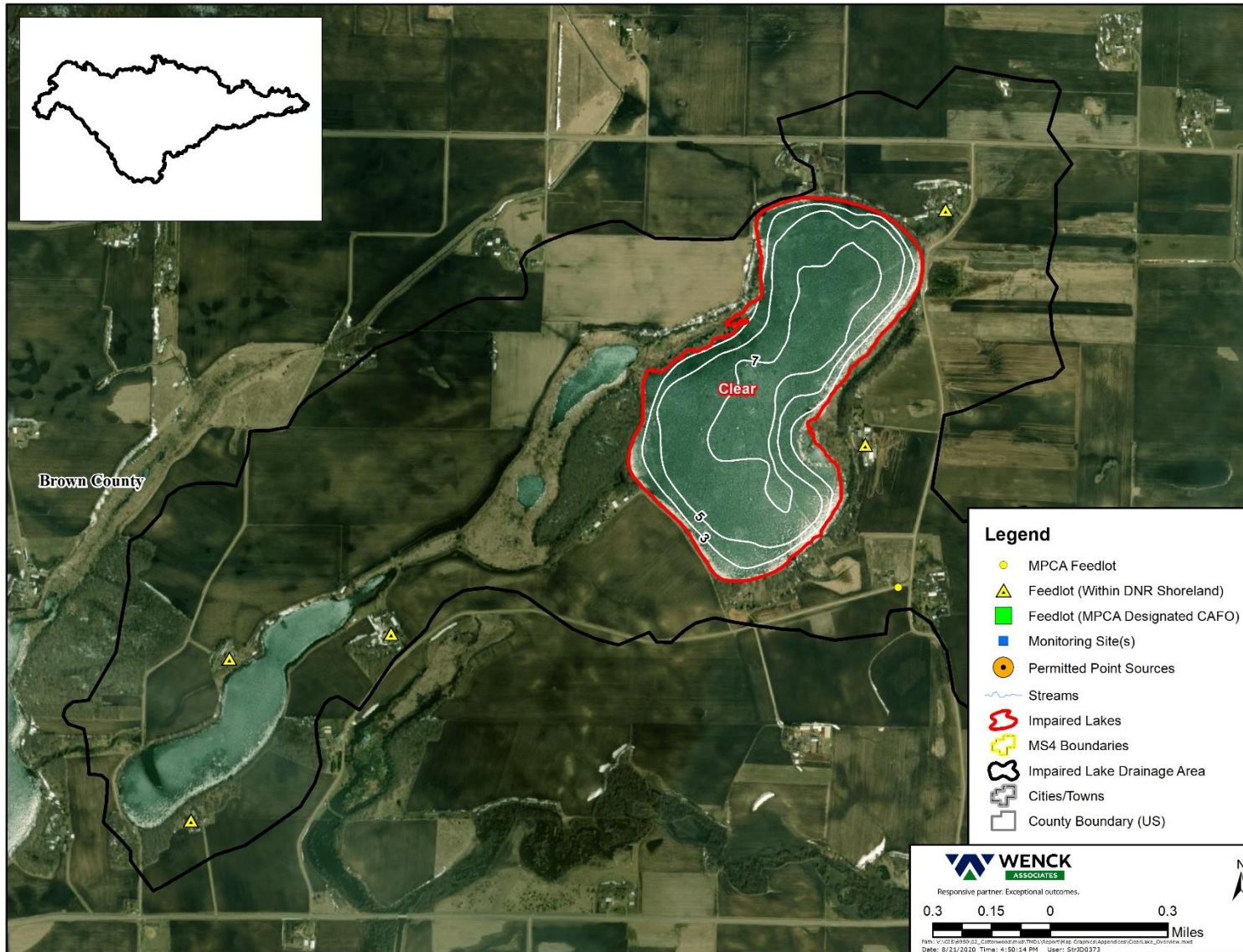


Figure C-22. Clear Lake Overview.

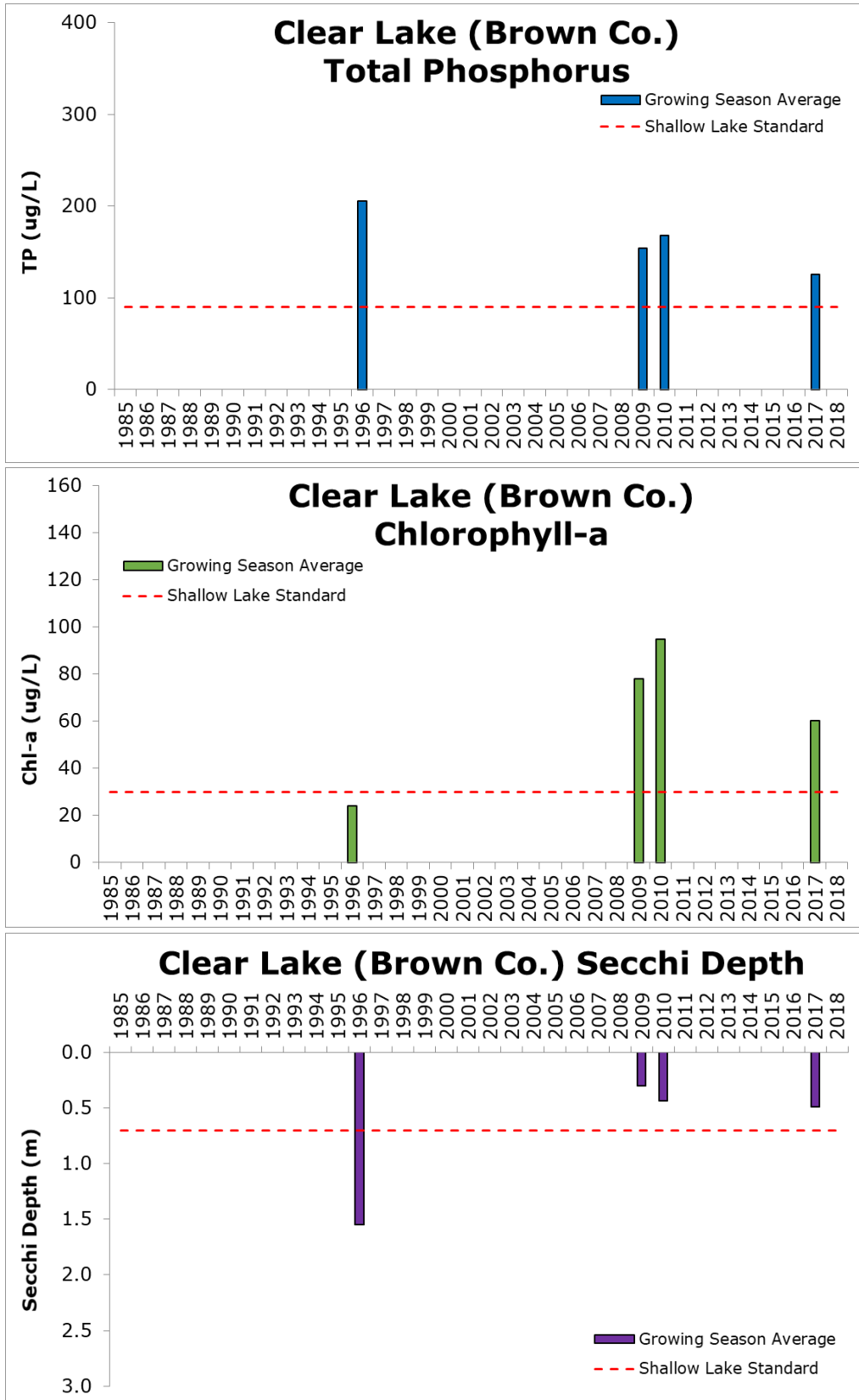


Figure C-23. Clear Lake Historic Water Quality.

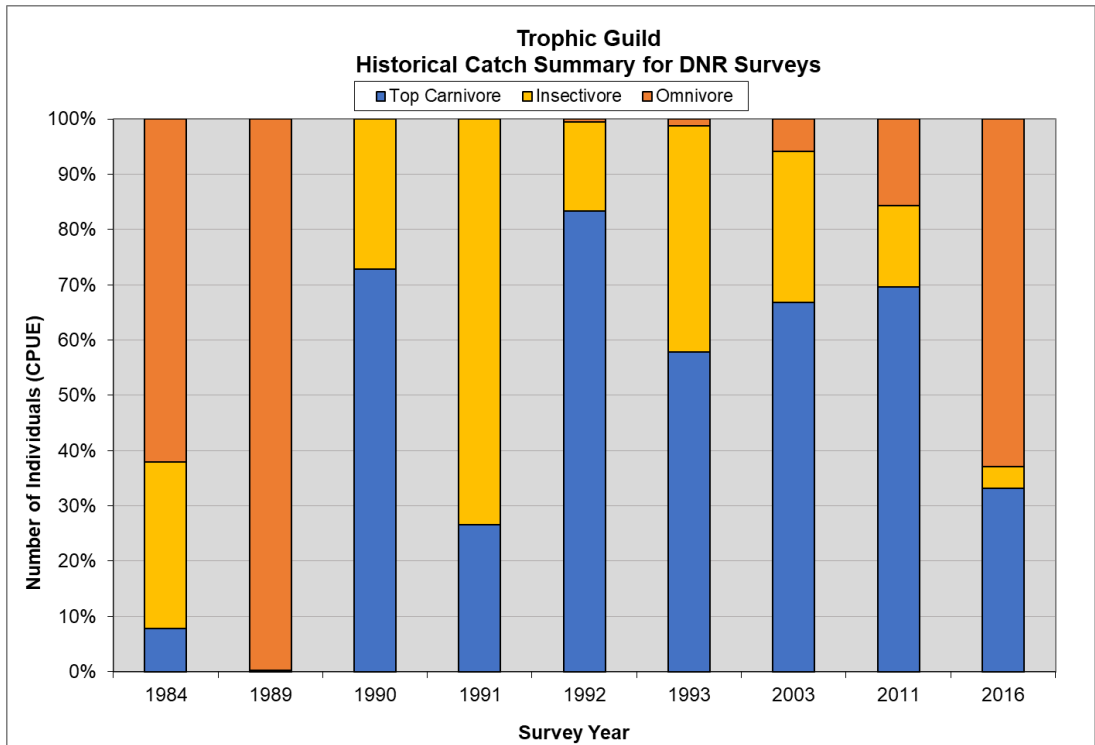


Figure C-24. Clear Lake DNR Fish Survey Historic Catch Summarized by Trophic Guild and Catch Per Unit Effort (CPUE).

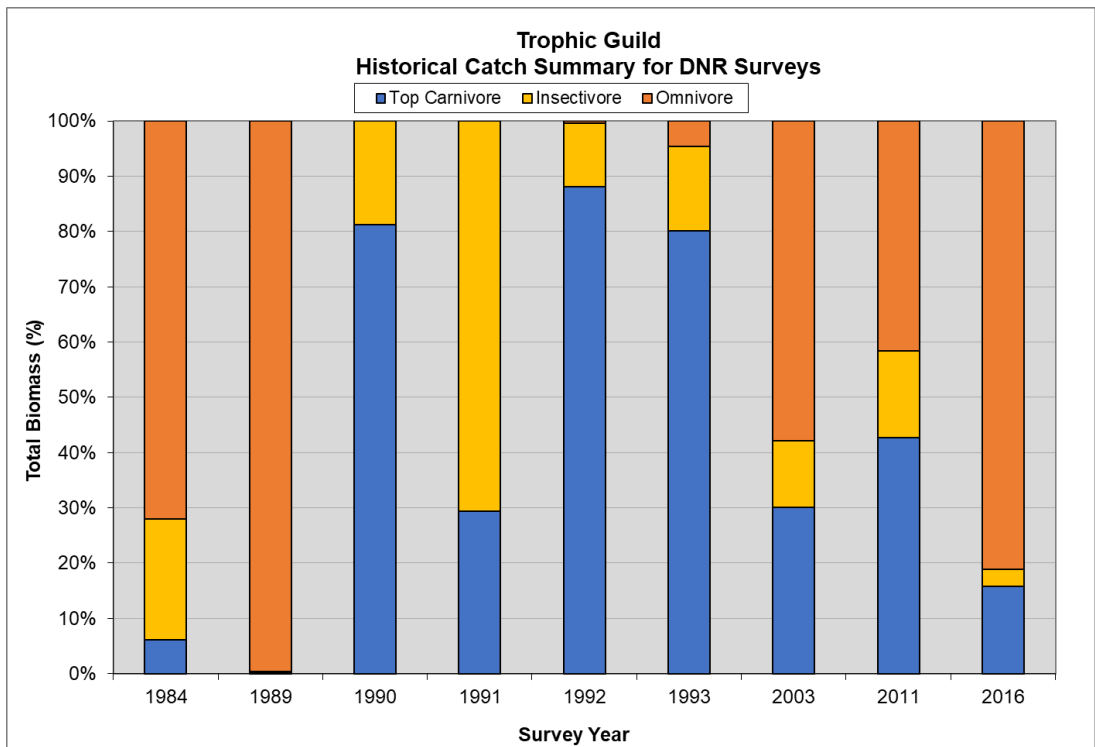


Figure C-25. Clear Lake DNR Fish Survey Historic Catch Summarized by Trophic Guild and Total Biomass.

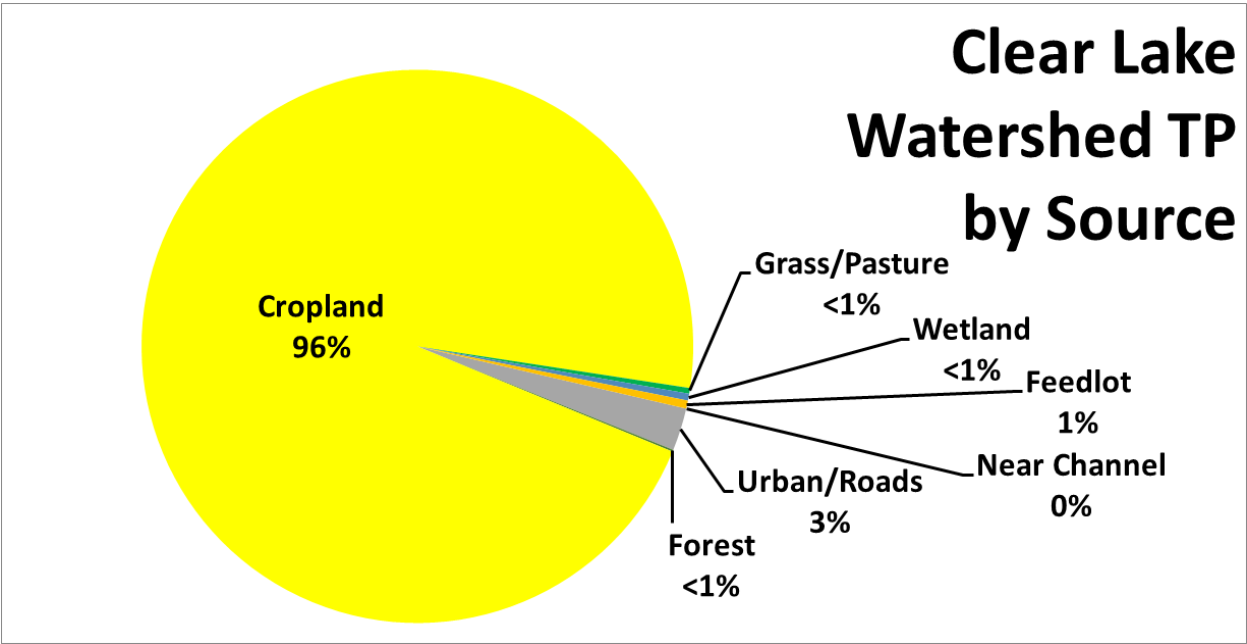


Figure C-26. Clear Lake watershed TP load contribution by source predicted by HSPF.

Table C-12. Clear Lake Current Condition Lake Response Model.

Average Loading Summary for Clear (Brown Co.)							
Water Budgets				Phosphorus Loading			
Inflow from Drainage Areas							
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load	
	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]	
1	Direct Watershed (HSPF 452)	1,426	13.6	1,613	241	1.0	1,057
2							
3							
4							
5							
6							
	<i>Summation</i>	1,426	14	1,612.95			1,057
Failing Septic Systems							
	Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]	Calibration Factor	Load [lb/yr]
1		13	1.74	0	13%		16
2							
3							
4							
5							
	<i>Summation</i>	13	2	0.0	13%		16
Inflow from Upstream Lakes							
	Name		Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]	Load [lb/yr]	
1				-	1.0		
2				-	1.0		
3				-	1.0		
4				-	1.0		
5				-	1.0		
	<i>Summation</i>		0.0	-		0.0	
Atmosphere							
	Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]
	277	32.0	32.0	0.00	0.24	1.0	66
				Dry-year total P deposition =	0.222		
				Average-year total P deposition =	0.239		
				Wet-year total P deposition =	0.259		
				(Barr Engineering 2004)			
Internal							
	Lake Area [km ²]	Anoxic Factor [days]		Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]	
	1.12	0	Oxic		1.0	0	
	1.12	37.0	Anoxic		1.0	1,289	
	<i>Summation</i>					1,289	
			Net Discharge [ac-ft/yr] =	1,613		Net Load [lb/yr] =	2,429

Average Lake Response Modeling for Clear (Brown Co.)			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
	$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)	
		C _P =	1.00 [--]
		C _{CB} =	0.162 [--]
		b =	0.458 [--]
		W (total P load = inflow + atm.) =	1,102 [kg/yr]
		Q (lake outflow) =	2.0 [10 ⁶ m ³ /yr]
		V (modeled lake volume) =	1.7 [10 ⁶ m ³]
		T = V/Q =	0.84 [yr]
		P _i = W/Q =	554 [ug/l]
Model Predicted In-Lake [TP]			151.0 [ug/l]
Observed In-Lake [TP]			151.0 [ug/l]

Table C-13. Clear Lake TMDL Condition Lake Response Model.

TMDL Loading Summary for Clear (Brown Co.)						
Water Budgets				Phosphorus Loading		
Inflow from Drainage Areas						
Name	Drainage Area [acre]	Runoff Depth [in/yr]	Discharge [ac-ft/yr]	Phosphorus Concentration [ug/L]	Loading Calibration Factor (CF) ¹ [--]	Load [lb/yr]
1 Direct Watershed (HSPF 452)	1,426	13.6	1,613	150	0.6	658
2						
3						
4						
5						
6						
Summation		1,426	14	1,612.95		658
Failing Septic Systems						
Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]	Calibration Factor	Load [lb/yr]
1	0	13	0	0%		8
2						
3						
4						
5						
Summation		13	0	0.0	0%	8
Inflow from Upstream Lakes						
Name	Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]	Load [lb/yr]		
1		-	1.0			
2		-	1.0			
3		-	1.0			
4		-	1.0			
5		-	1.0			
Summation		0.0	-	0.0		
Atmosphere						
Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]
277	32.0	32.0	0.00	0.24	1.0	66
Dry-year total P deposition =				0.222		
Average-year total P deposition =				0.239		
Wet-year total P deposition =				0.259		
(Barr Engineering 2004)						
Internal						
Lake Area [km ²]	Anoxic Factor [days]	Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]		
1.12	0	Oxic	1.0	0		
1.12	37.0	Anoxic	1.0	407		
Summation				407		
Net Discharge [ac-ft/yr] =			1,613	Net Load [lb/yr] =		1,139

TMDL Lake Response Modeling for Clear (Brown Co.)			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
$P = \frac{P_i}{\left(1 + C_p \times C_{CB} \times \left(\frac{W_p}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)		
		C _p =	1.00 [--]
		C _{CB} =	0.162 [--]
		b =	0.458 [--]
	W (total P load = inflow + atm.) =		517 [kg/yr]
	Q (lake outflow) =		2.0 [10 ⁶ m ³ /yr]
	V (modeled lake volume) =		1.7 [10 ⁶ m ³]
	T = W/Q =		0.84 [yr]
	P _i = W/Q =		260 [µg/l]
Model Predicted In-Lake [TP]			90.0 [ug/l]
Observed In-Lake [TP]			151.0 [ug/l]

Supporting Items for Altermatt Lake (08005400)

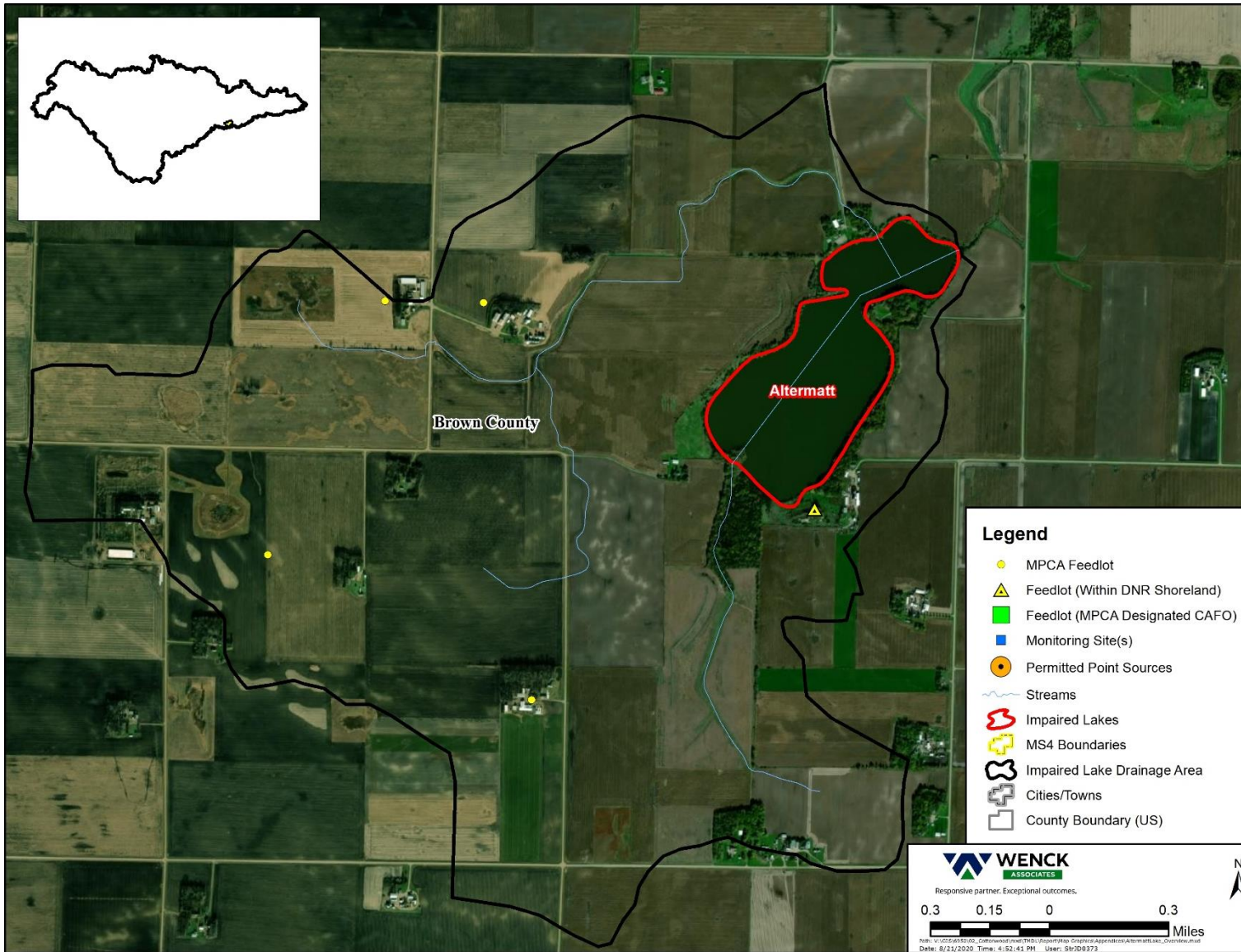


Figure C-27. Altermatt Lake Overview.

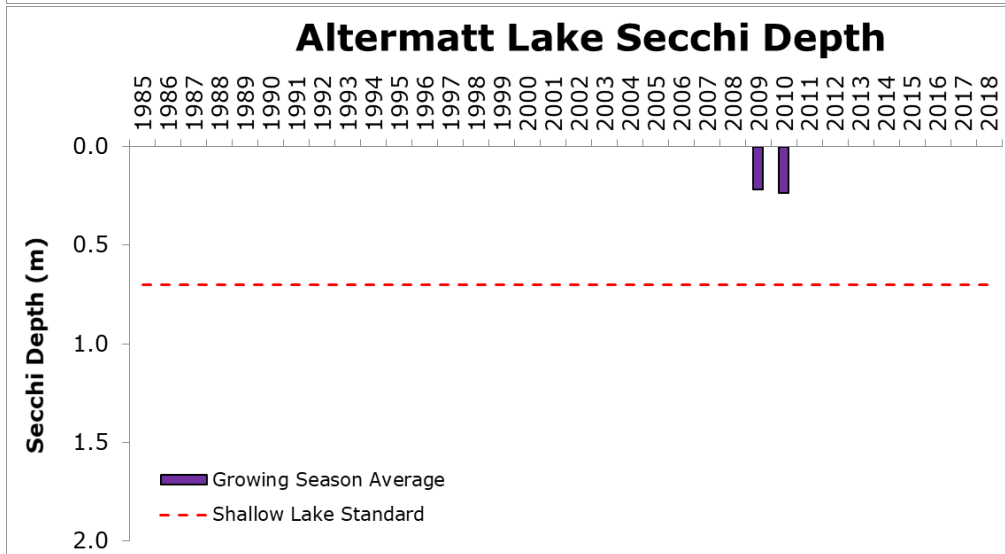
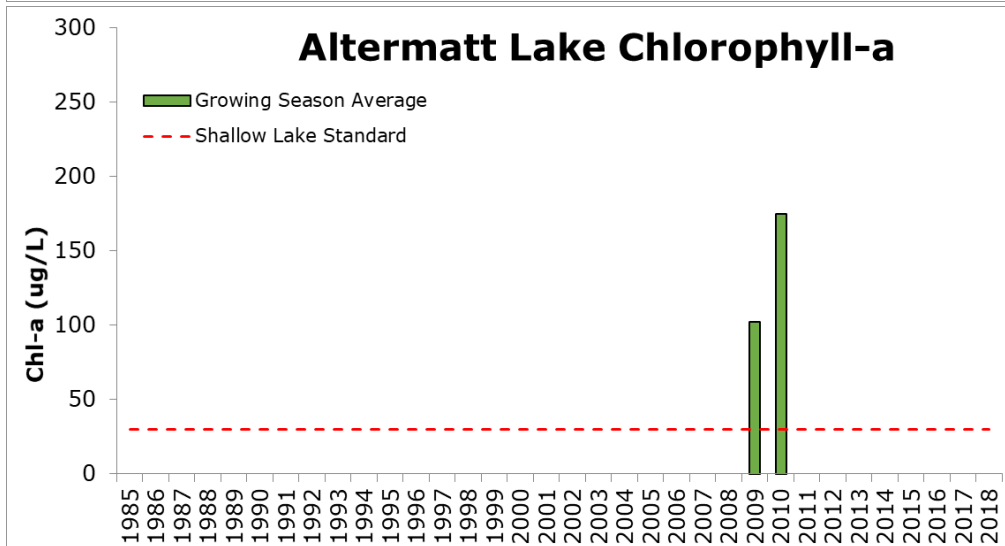
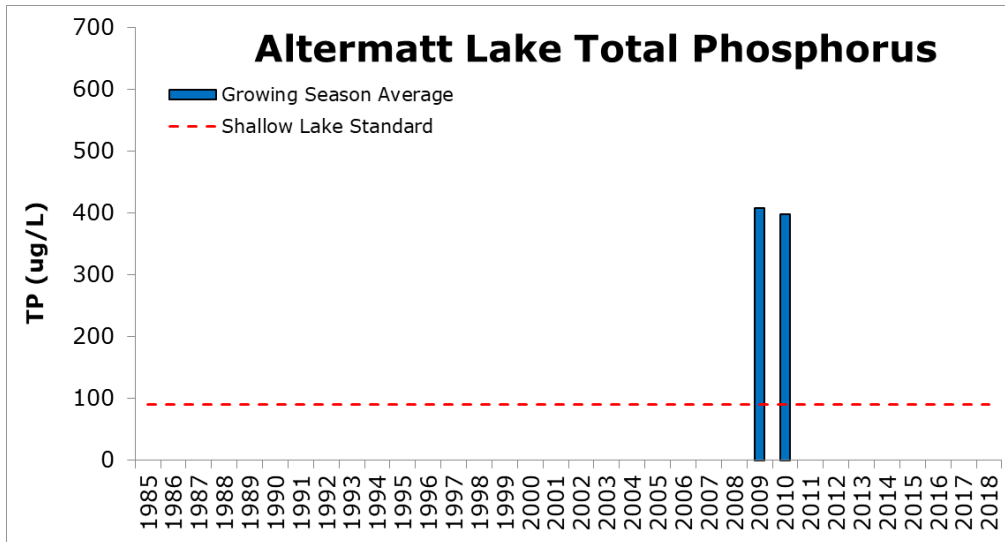


Figure C-28. Altermatt Lake Historic Water Quality.

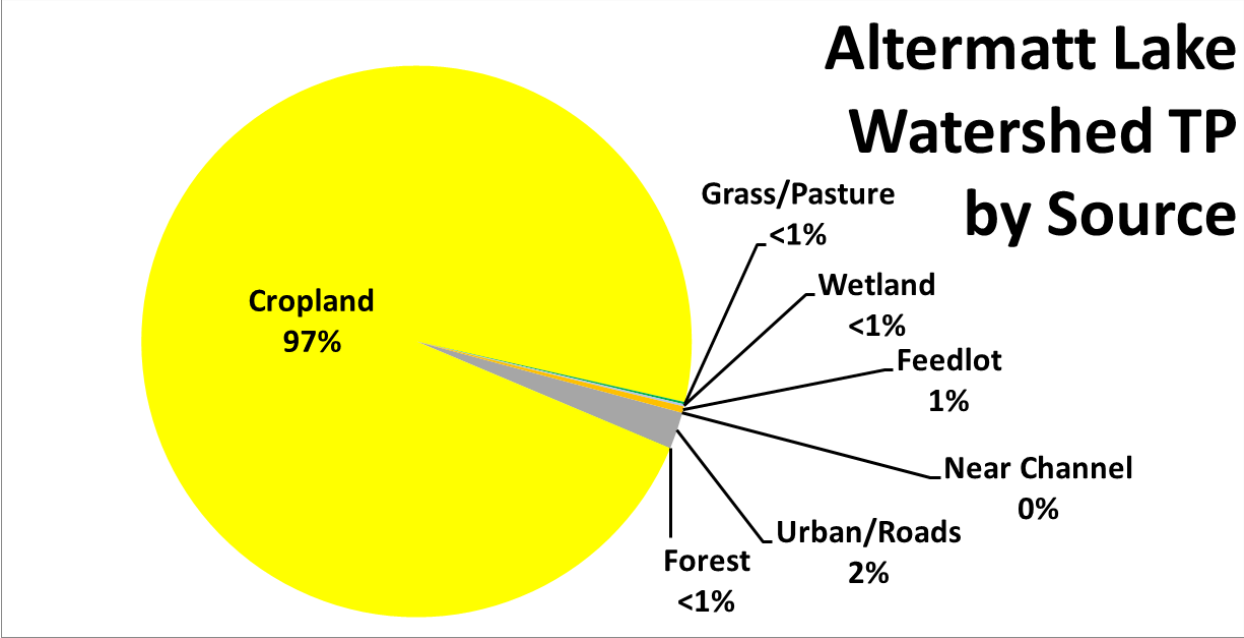


Figure C-29. Altermatt Lake watershed TP load contribution by source predicted by HSPF.

Table C-14. Altermatt Lake Current Condition Lake Response Model.

Average Loading Summary for Altermatt						
Water Budgets				Phosphorus Loading		
Inflow from Drainage Areas						
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load
Name	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]
1 All	1,865	6.5	1,012	356	1.0	980
2						
3						
4						
5						
6						
Summation	1,865	7	1,012.10			980
Failing Septic Systems						
Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]		Load [lb/yr]
1	9	2		25%		9
2						
3						
4						
5						
Summation	9	2	0.0	25%		9
Inflow from Upstream Lakes						
Name		Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]		Load [lb/yr]
1			-	1.0		
2			-	1.0		
3			-	1.0		
4			-	1.0		
5			-	1.0		
Summation		0.0	-			0.0
Atmosphere						
Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]
122	34.6	34.6	0.00	0.24	1.0	29
Dry-year total P deposition =				0.222		
Average-year total P deposition =				0.239		
Wet-year total P deposition =				0.259		
(Barr Engineering 2004)						
Internal						
Lake Area [km ²]	Anoxic Factor [days]		Release Rate [mg/m ² -day]	Calibration Factor [--]		Load [lb/yr]
0.49	0	Oxic		1.0		0
0.49	81.5	Anoxic	35.7	1.0		3,169
Summation						3,169
Net Discharge [ac-ft/yr] =			1,012	Net Load [lb/yr] =		4,188

Average Lake Response Modeling for Altermatt			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)		
	$C_P =$	1.00	[--]
	$C_{CB} =$	0.162	[--]
	$b =$	0.458	[--]
	W (total P load = inflow + atm.) =	1,900	[kg/yr]
	Q (lake outflow) =	1.2	[10 ⁶ m ³ /yr]
	V (modeled lake volume) =	0.5	[10 ⁶ m ³]
	$T = V/Q =$	0.39	[yr]
$P_i = W/Q =$	1521	[ug/l]	
Model Predicted In-Lake [TP]			402.8 [ug/l]
Observed In-Lake [TP]			402.8 [ug/l]

Table C-15. Altermatt Lake TMDL Condition Lake Response Model.

TMDL Loading Summary for Altermatt						
Water Budgets				Phosphorus Loading		
Inflow from Drainage Areas						
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load
Name	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]
1 All	1,865	6.5	1,012	141	0.4	388
2						
3						
4						
5						
6						
Summation	1,865	7	1,012.10			388
Failing Septic Systems						
Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]		Load [lb/yr]
1	9	2.25	0	25%		4
2						
3						
4						
5						
Summation	9	2	0.0	25%		4
Inflow from Upstream Lakes						
Name		Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]		Load [lb/yr]
1			-	1.0		
2			-	1.0		
3			-	1.0		
4			-	1.0		
5			-	1.0		
Summation			0.0	-		0.0
Atmosphere						
Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]
122	34.6	34.6	0.00	0.24	1.0	29.2
Dry-year total P deposition =				0.222		
Average-year total P deposition =				0.239		
Wet-year total P deposition =				0.259		
(Barr Engineering 2004)						
Internal						
Lake Area [km ²]	Anoxic Factor [days]			Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]
0.49	0		Oxic		1.0	0
0.49	81.5		Anoxic	35.7	1.0	89
Summation						89
Net Discharge [ac-ft/yr] =			1,012	Net Load [lb/yr] =		510

TMDL Lake Response Modeling for Altermatt			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)		
	$C_P =$	1.00	[--]
	$C_{CB} =$	0.162	[--]
	$b =$	0.458	[--]
	W (total P load = inflow + atm.) =	231	[kg/yr]
	Q (lake outflow) =	1.2	[10 ⁶ m ³ /yr]
	V (modeled lake volume) =	0.5	[10 ⁶ m ³]
	$T = V/Q =$	0.39	[yr]
$P_i = W/Q =$	185	[ug/l]	
Model Predicted In-Lake [TP]			90.0 [ug/l]
Observed In-Lake [TP]			402.8 [ug/l]

Supporting Items for Boise Lake (08009600)

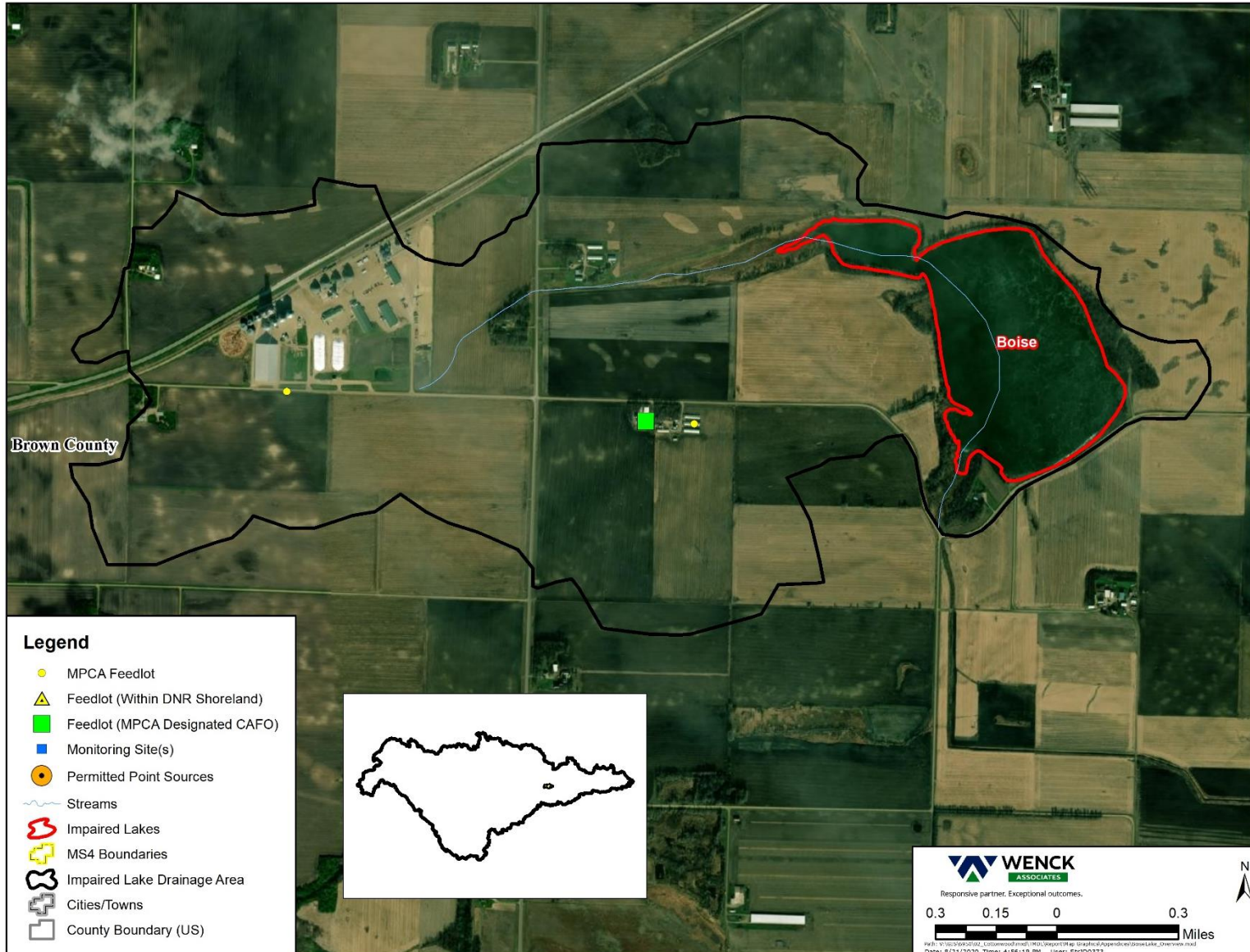


Figure C-30. Boise Lake Overview.

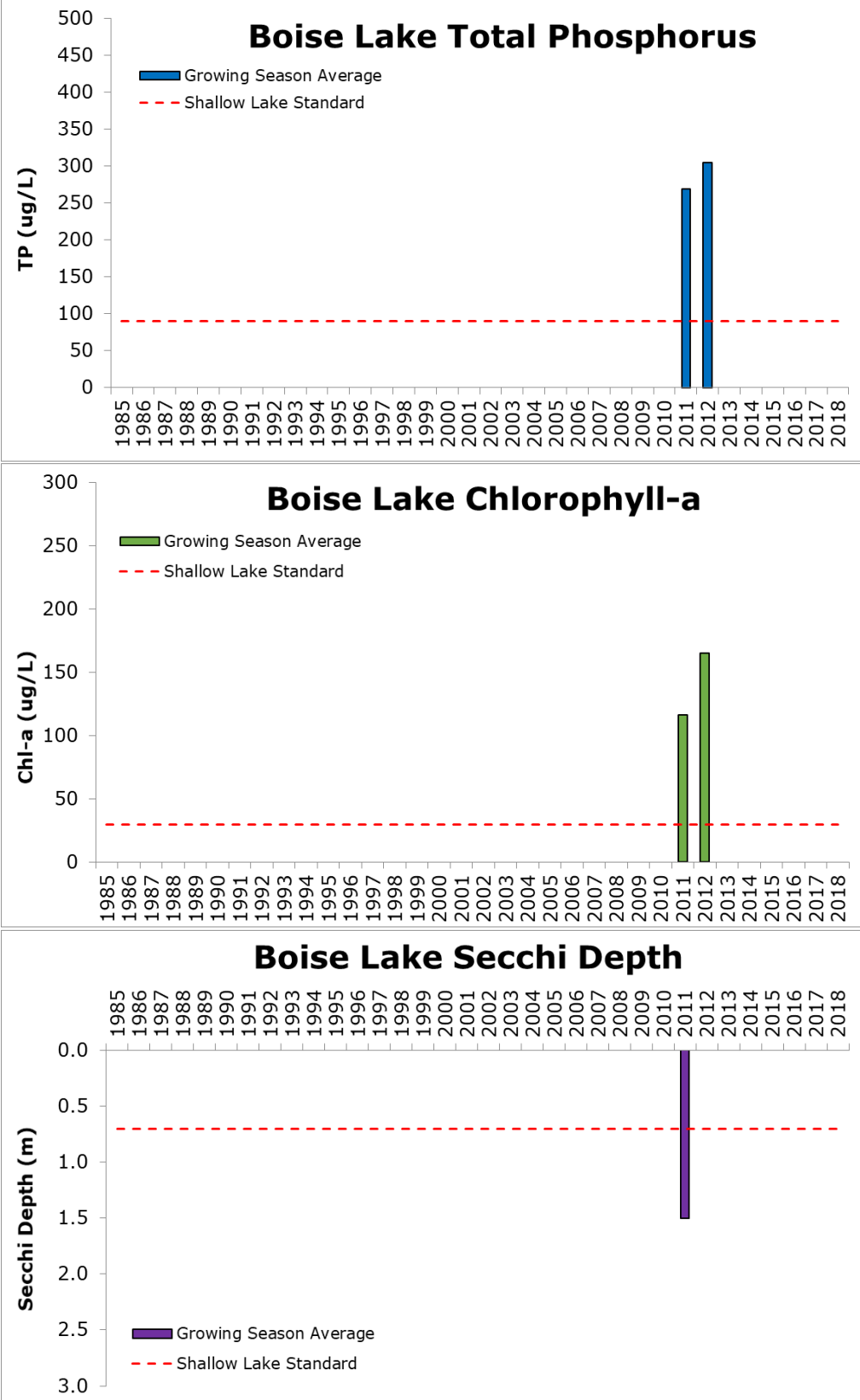


Figure C-31. Boise Lake Historic Water Quality.

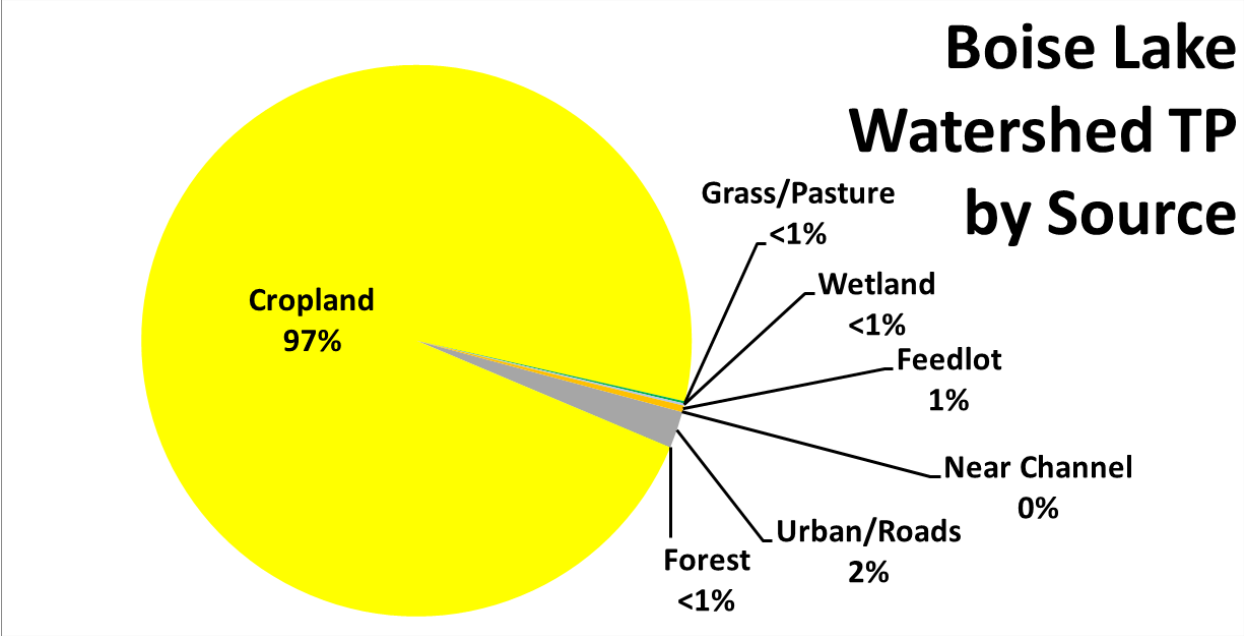


Figure C-32. Boise Lake watershed TP load contribution by source predicted by HSPF.

Table C-16. Boise Lake Current Condition Lake Response Model.

Average Loading Summary for Boise							
Water Budgets				Phosphorus Loading			
Inflow from Drainage Areas							
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load	
Name	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]	
1 All	1,376	7.9	901	329	1.0	805	
2			0	0		0	
3			0	0		0	
4			0	0		0	
5			0	0		0	
6			0	0		0	
Summation	1,376	8	900.61			805	
Failing Septic Systems							
Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]	Load [lb/yr]		
1	7	1.75		25%	8		
2							
3							
4							
5							
Summation			0.0		8		
Inflow from Upstream Lakes							
Name	Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]	Load [lb/yr]			
1		-	1.0				
2		-	1.0				
3		-	1.0				
4		-	1.0				
5		-	1.0				
Summation		0.0	-	0.0			
Atmosphere							
Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]	
187	23.9	23.9	0.00	0.22	1.0	42	
Dry-year total P deposition =				0.222			
Average-year total P deposition =				0.239			
Wet-year total P deposition =				0.259			
(Barr Engineering 2004)							
Internal							
Lake Area [km ²]	Anoxic Factor [days]			Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]	
0.76	0		Oxic		1.0	0	
0.76	74.4		Anoxic	10.7	1.0	1,333	
Summation						1,333	
Net Discharge [ac-ft/yr] =			901	Net Load [lb/yr] =		2,188	

Average Lake Response Modeling for Boise			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)		
	$C_P =$	1.00	[--]
	$C_{CB} =$	0.162	[--]
	$b =$	0.458	[--]
	W (total P load = inflow + atm.) =	992	[kg/yr]
	Q (lake outflow) =	1.1	[10 ⁶ m ³ /yr]
	V (modeled lake volume) =	0.4	[10 ⁶ m ³]
	$T = V/Q =$	0.37	[yr]
$P_i = W/Q =$	893	[ug/l]	
Model Predicted In-Lake [TP]		287.0	[ug/l]
Observed In-Lake [TP]		287.0	[ug/l]

Table C-17. Boise Lake TMDL Condition Lake Response Model.

TMDL Loading Summary for Boise						
Water Budgets				Phosphorus Loading		
Inflow from Drainage Areas						
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load
Name	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[-]	[lb/yr]
1 All	1,376	7.9	901	113	0.3	276
2			0	0		0
3			0	0		0
4			0	0		0
5			0	0		0
6			0	0		0
Summation	1,376	8	900.61			276
Failing Septic Systems						
Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]		Load [lb/yr]
1	7	0		0%		4
2						
3						
4						
5						
Summation			0.0			4
Inflow from Upstream Lakes						
Name		Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [-]		Load [lb/yr]
1			-	1.0		
2			-	1.0		
3			-	1.0		
4			-	1.0		
5			-	1.0		
Summation		0.0	-			0.0
Atmosphere						
Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [-]	Load [lb/yr]
187	23.9	23.9	0.00	0.22	1.0	42
Dry-year total P deposition =				0.222		
Average-year total P deposition =				0.239		
Wet-year total P deposition =				0.259		
(Barr Engineering 2004)						
Internal						
Lake Area [km ²]	Anoxic Factor [days]			Release Rate [mg/m ² -day]	Calibration Factor [-]	Load [lb/yr]
0.76	0		Oxic		1.0	0
0.76	74.4		Anoxic	10.7	1.0	124
Summation						124
Net Discharge [ac-ft/yr] =			901	Net Load [lb/yr] =		445

TMDL Lake Response Modeling for Boise			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)		
		C _P =	1.00 [-]
		C _{CB} =	0.162 [-]
		b =	0.458 [-]
	W (total P load = inflow + atm.) =		202 [kg/yr]
	Q (lake outflow) =		1.1 [10 ⁶ m ³ /yr]
	V (modeled lake volume) =		0.4 [10 ⁶ m ³]
	T = V/Q =		0.37 [yr]
	P _i = W/Q =		182 [ug/l]
Model Predicted In-Lake [TP]			90.0 [ug/l]
Observed In-Lake [TP]			287.0 [ug/l]

Supporting Items for Bachelor Lake (08002900)

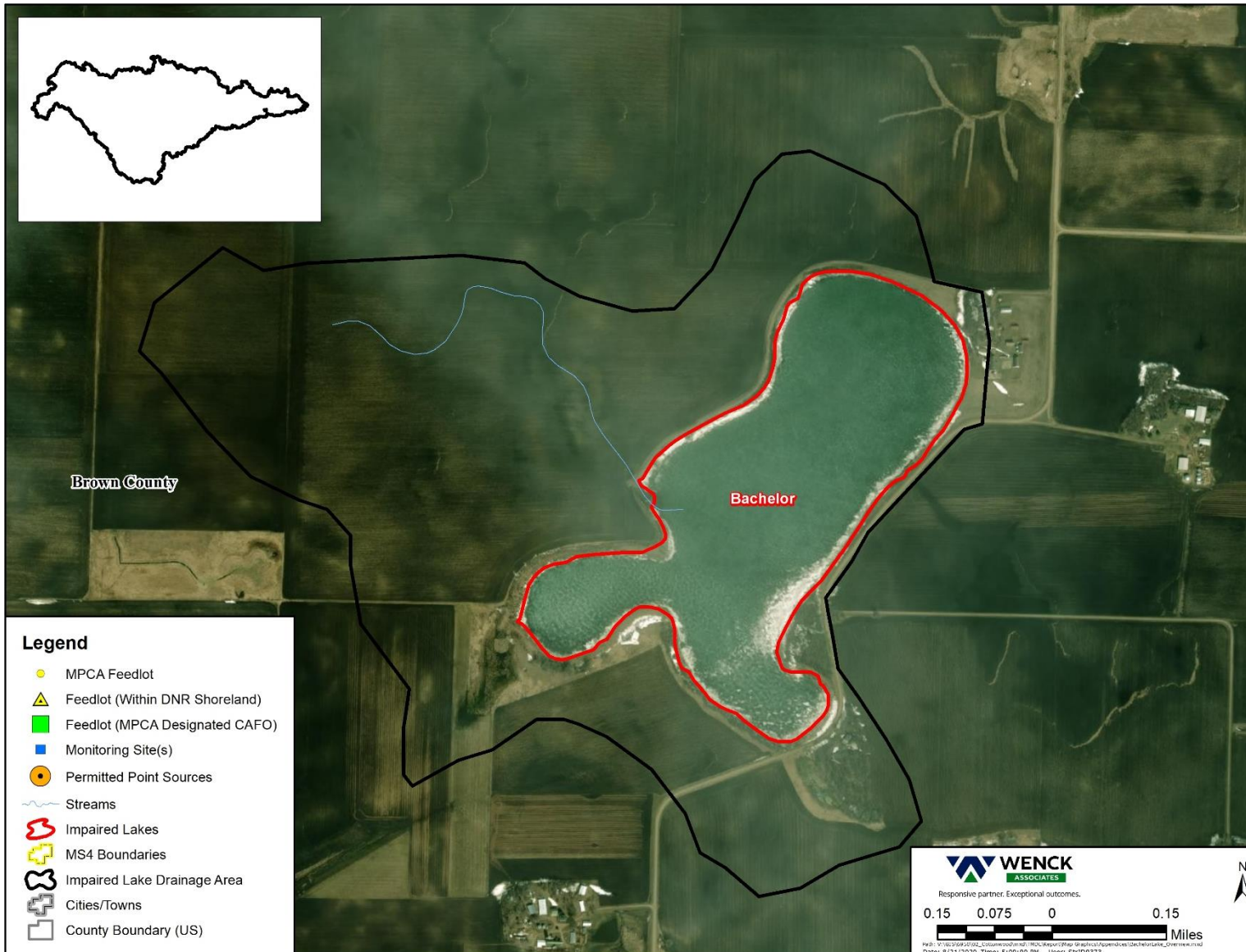


Figure C-33. Bachelor Lake Overview.

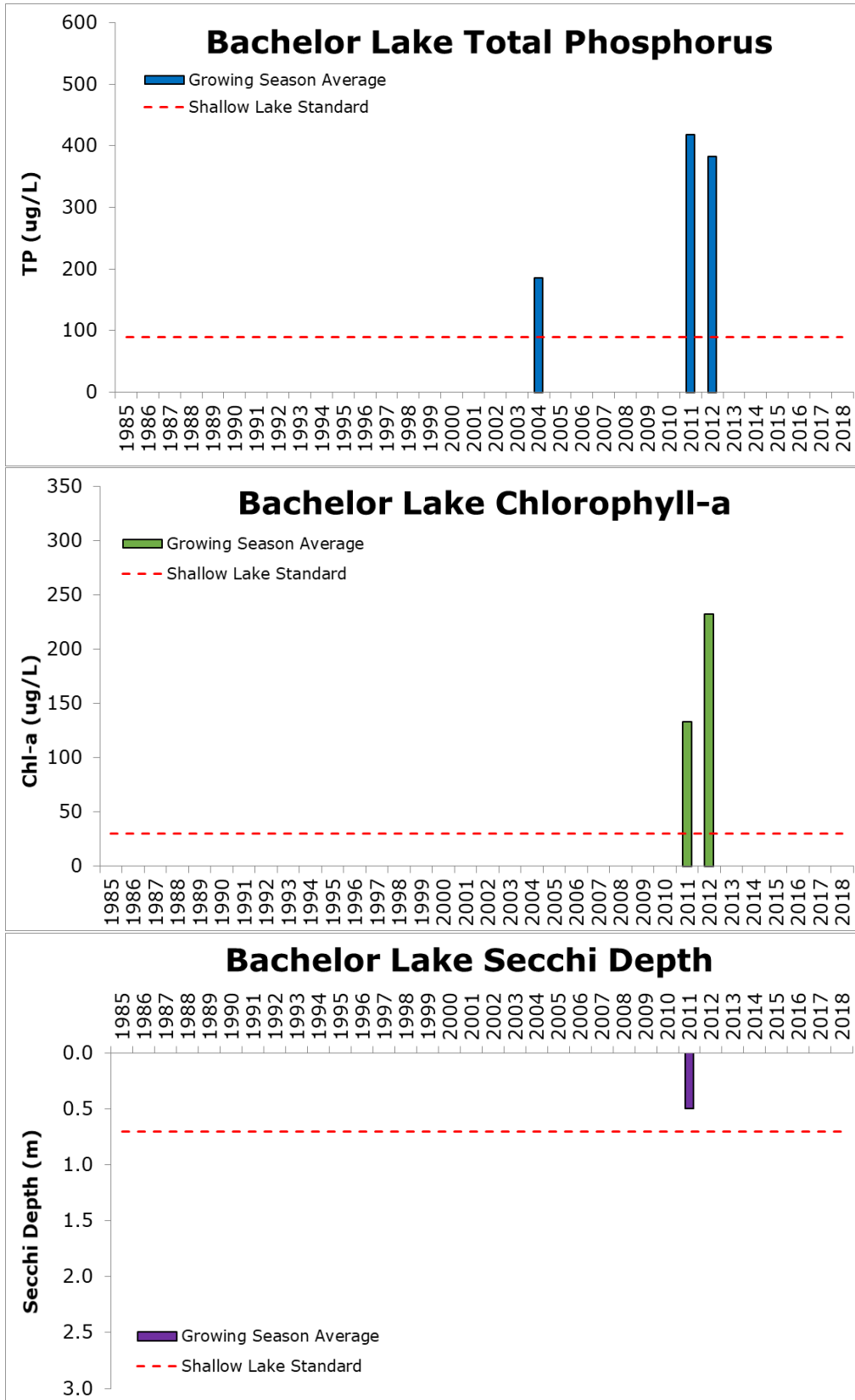


Figure C-34. Bachelor Lake Historic Water Quality.

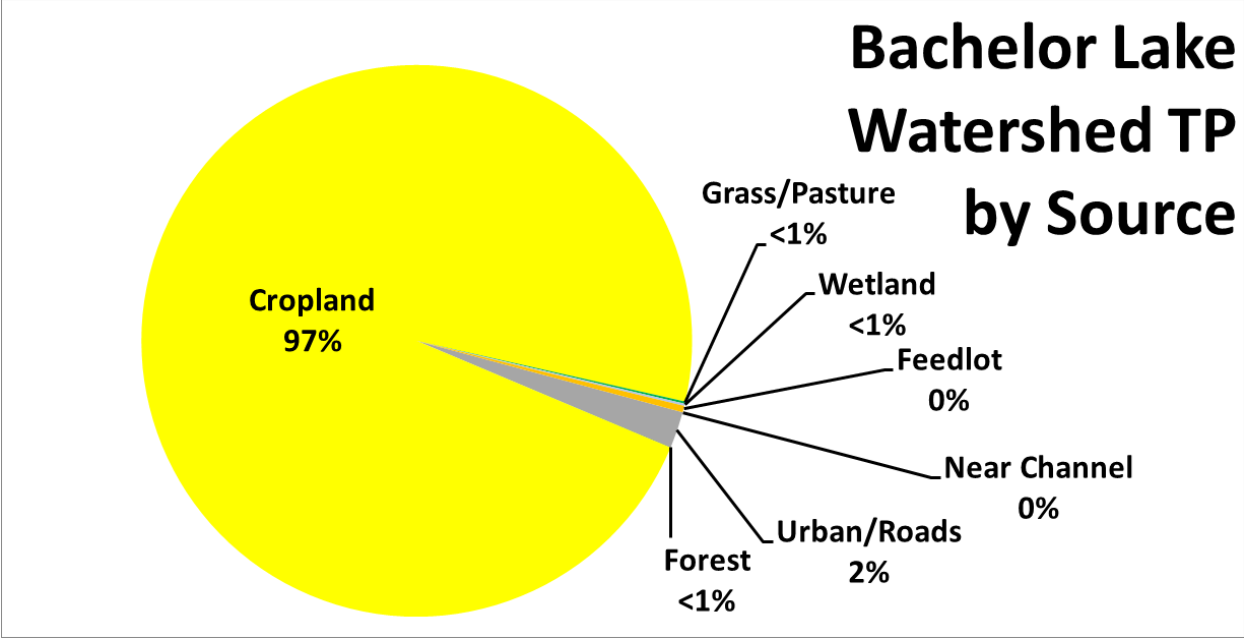


Figure C-35. Bachelor Lake watershed TP load contribution by source predicted by HSPF.

Table C-18. Bachelor Lake Current Condition Lake Response Model.

Average Loading Summary for Bachelor							
Water Budgets				Phosphorus Loading			
Inflow from Drainage Areas							
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load	
	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]	
1	All	377	297	349	1.0	283	
2							
3							
4							
5							
6							
	Summation	377	297.48			283	
Failing Septic Systems							
	Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]	Load [lb/yr]	
1		1	0		49%	1	
2							
3							
4							
5							
	Summation			0.0		1	
Inflow from Upstream Lakes							
	Name		Discharge [ac-ft/yr]	Estimated P Concentration [ug/L]	Calibration Factor [--]	Load [lb/yr]	
1				-	1.0		
2				-	1.0		
3				-	1.0		
4				-	1.0		
5				-	1.0		
	Summation		0.0	-		0.0	
Atmosphere							
	Lake Area [acre]	Precipitation [in/yr]	Evaporation [in/yr]	Net Inflow [ac-ft/yr]	Aerial Loading Rate [lb/ac-yr]	Calibration Factor [--]	Load [lb/yr]
	105	23.9	23.9	0.00	0.22	1.0	23.3
					Dry-year total P deposition = 0.222		
					Average-year total P deposition = 0.239		
					Wet-year total P deposition = 0.259		
					(Barr Engineering 2004)		
Internal							
	Lake Area [km ²]	Anoxic Factor [days]		Release Rate [mg/m ² -day]	Calibration Factor [--]	Load [lb/yr]	
	0.42	0	Oxic		1.0	0	
	0.42	80.6	Anoxic	12.7	1.0	963	
	Summation					963	
			Net Discharge [ac-ft/yr] =	297		Net Load [lb/yr] =	1,269

Average Lake Response Modeling for Bachelor			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
	$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)	
		C _P =	1.00 [--]
		C _{CB} =	0.162 [--]
		b =	0.458 [--]
		W (total P load = inflow + atm.) =	576 [kg/yr]
		Q (lake outflow) =	0.4 [10 ⁶ m ³ /yr]
		V (modeled lake volume) =	0.2 [10 ⁶ m ³]
		T = V/Q =	0.41 [yr]
		P _i = W/Q =	1568 [ug/l]
Model Predicted In-Lake [TP]			400.4 [ug/l]
Observed In-Lake [TP]			400.4 [ug/l]

Table C-19. Bachelor Lake TMDL Condition Lake Response Model.

TMDL Loading Summary for Bachelor						
Water Budgets				Phosphorus Loading		
Inflow from Drainage Areas						
	Drainage Area	Runoff Depth	Discharge	Phosphorus Concentration	Loading Calibration Factor (CF) ¹	Load
Name	[acre]	[in/yr]	[ac-ft/yr]	[ug/L]	[--]	[lb/yr]
1 All	377	9.5	297	67	0.2	54
2						
3						
4						
5						
6						
Summation	377	9	297.48			54
Failing Septic Systems						
Name	Total Systems	Failing Systems	Discharge [ac-ft/yr]	Failure [%]		Load [lb/yr]
1	1	0		0%		0
2						
3						
4						
5						
Summation			0.0			0
Inflow from Upstream Lakes						
			Discharge	Estimated P Concentration	Calibration Factor	Load
Name			[ac-ft/yr]	[ug/L]	[--]	[lb/yr]
1				-	1.0	
2				-	1.0	
3				-	1.0	
4				-	1.0	
5				-	1.0	
Summation			0.0	-		0.0
Atmosphere						
Lake Area	Precipitation	Evaporation	Net Inflow	Aerial Loading Rate	Calibration Factor	Load
[acre]	[in/yr]	[in/yr]	[ac-ft/yr]	[lb/ac-yr]	[--]	[lb/yr]
105	23.9	23.9	0.00	0.22	1.0	23
				Dry-year total P deposition = 0.222		
				Average-year total P deposition = 0.239		
				Wet-year total P deposition = 0.259		
				(Barr Engineering 2004)		
Internal						
Lake Area	Anoxic Factor			Release Rate	Calibration Factor	Load
[km ²]	[days]			[mg/m ² -day]	[--]	[lb/yr]
0.42	0		Oxic		1.0	0
0.42	80.6		Anoxic	12.7	1.0	76
Summation						76
			Net Discharge [ac-ft/yr] =	297		Net Load [lb/yr] =
						154

TMDL Lake Response Modeling for Bachelor			
Modeled Parameter	Equation	Parameters	Value [Units]
TOTAL IN-LAKE PHOSPHORUS CONCENTRATION			
$P = \frac{P_i}{\left(1 + C_P \times C_{CB} \times \left(\frac{W_P}{V}\right)^b \times T\right)}$	as f(W,Q,V) from Canfield & Bachmann (1981)		
		C _P =	1.00 [--]
		C _{CB} =	0.162 [--]
		b =	0.458 [--]
		W (total P load = inflow + atm.) =	70 [kg/yr]
		Q (lake outflow) =	0.4 [10 ⁶ m ³ /yr]
		V (modeled lake volume) =	0.2 [10 ⁶ m ³]
		T = V/Q =	0.41 [yr]
		P _i = W/Q =	190 [ug/l]
Model Predicted In-Lake [TP]			90.0 [ug/l]
Observed In-Lake [TP]			400.4 [ug/l]

Additional Supporting Items for Impaired Lakes

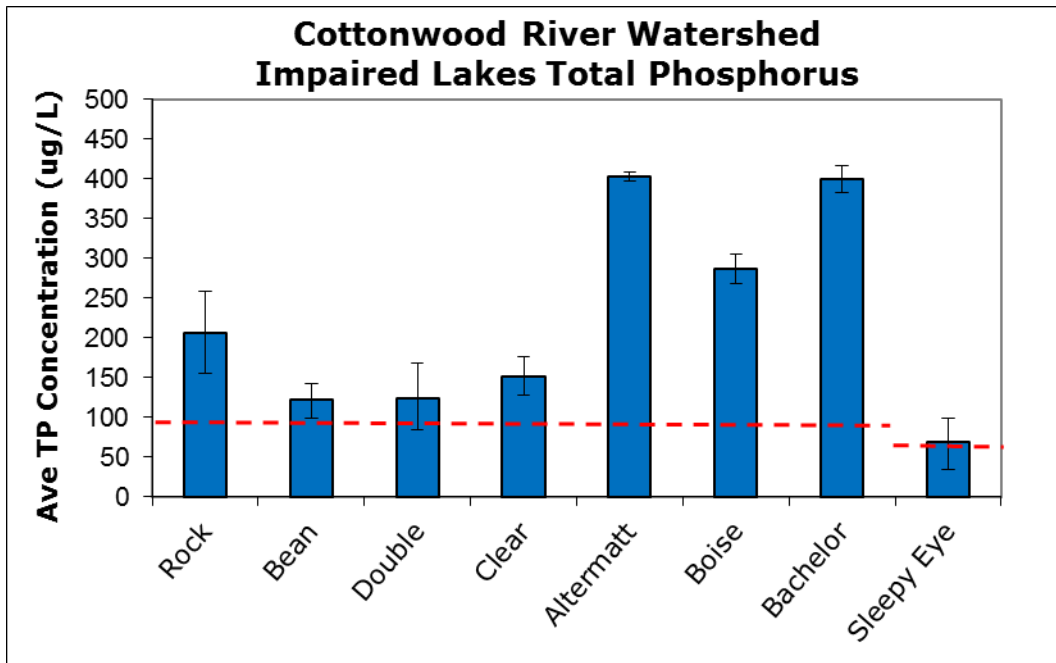


Figure C-36. Average summer growing season TP concentrations for each impaired lake, including Sleepy Eye (delisted 2020).

To: Redwood Cottonwood Rivers Control Area
Minnesota Pollution Control Agency

From: Tom Langer, Wenck Associates, Inc.
Jeff Strom, Wenck Associates, Inc.

Date: February 4, 2019

Memo Subject: Redwood and Cottonwood River Watershed Lake Common Carp Assessments

Wenck Associates conducted common carp (*Cyprinus carpio*) population assessments on School Grove, Double and Sleepy Eye Lakes on June 27- 28, 2018. These were the first common carp population assessment conducted on these systems. The survey efforts were intended to better inform lake managers of the abundance and density of carp within the system and to inform of possible water quality degradation occurring from an overabundance of common carp. This technical memo summarizes the methods and results of the June 27- 28, 2018 assessment and provides management recommendations.

Methods

Biologists and scientists from Wenck Associates conducted common carp population assessments using standard research methods described in (Bajer and Sorensen 2012). Boat electrofishing was implemented to sample three shoreline transects per lake for approximately 20 minutes each under MnDNR permit approval.

All common carp were netted (some carp are inevitably missed), counted and measured for total length (weight was extrapolated from length using a regression model) prior to being released. This information, along with the amount of time spent electrofishing, were used in linear regression models developed by (Bajer and Sorensen 2012) to estimate the current population size and density within each lake.

Results

The total number of carp captured, average total length, and average weight varied across the three lakes. School Grove observed the greatest catch per unit effort (CPUE) and had the 2nd highest total length and weight of the three lakes surveyed. Sleepy Eye observed the lowest CPUE and the smallest and shortest carp, while Double had the 2nd highest CPUE but the largest and longest carp on average.

Using results of this assessment and the regression equation described above, the estimated common carp densities varied across the three lakes. School Grove Lake observed a biomass density of 331 kg/ha (295 lbs/acre). Extrapolating this density across the entire basin suggests that there are ~15,447 individual carp within the lake. Using this population estimate and the average weight of the fish capture suggests that there are currently ~102,631 pounds of carp in School Grove Lake. Double Lake observed a biomass density of 234 kg/ha (208 lbs/acre). Extrapolating this density across the entire basin suggests that there are ~3,109 individual carp and ~26,858 pounds of carp in Double Lake. Sleepy Eye Lake observed a biomass density of 19 kg/ha (17 lbs/acre). Extrapolating this density across the entire basin suggests that there are ~1,215 individual carp and ~4,105 pounds of carp in Sleepy Eye Lake.

Table 1: Summary of common carp assessments.

Lake	Carp Collected	Shock Time (hour)	Average Length (cm)	Average Weight (kg)	Biomass Mean (kg/ha)	Estimated Population Size
School Grove	24	1.06	59.6	3.02	331.0	15,447
Double	12	1	65.4	3.92	233.7	3,109
Sleepy Eye	2	1	55.3	1.53	19.1	1,215

Discussion

Common carp (*Cyprinus carpio*) are among the most widespread aquatic invasive species in North America. Common Carp can rapidly colonize a waterbody and significantly alter habitat, water quality conditions and nutrient dynamics within a lake. High densities of common carp can have specific impacts within a system, including reduced vegetation coverage, lower water fowl populations and increased water turbidity. Research suggests that these impacts begin to occur at densities of ~100 kg of carp biomass/hectare (89 lbs/acre) (Bajer *et al.* 2009). Populations observed at or above this density threshold would benefit from population reductions below 100 kg/ha as a strategy to improve water quality and restore a healthy functioning ecosystem.

Results of the common carp assessments indicate that School Grove and Double Lakes currently have carp biomass densities more than double the critical threshold (100kg/ ha). Sleepy Eye Lake was observed to be well below the critical threshold.

These results suggest common carp are a contributing factor to water quality impairments and habitat degradation within School Grove and Double Lakes, but not in Sleepy Eye Lake. To achieve density levels right at the 100 kg/ha threshold would require the removal of ~4,667 carp or ~10,780 kg in School Grove Lake and ~1,331 carp or ~1,779 kg in Double Lake. We recommend establishing removal goals below the critical threshold to 50 kg/ha to allow for potential growth of individuals that are not removed from the system.

References

Bajer, P.G, G. Sullivan, and P.W. Sorensen. 2009. Effects of a rapidly increasing population of common carp on vegetative cover and waterfowl in a recently restored Midwestern shallow lake. *Hydrobiologia* 632: 235-245.

Bajer, P.G. and P.W. Sorensen. 2012. Using Boat Electrofishing to Estimate the Abundance of Invasive Common Carp in Small Midwestern Lakes. *North American Journal of Fisheries Management* 32: 817-822.

Photos



Photo 1: Common carp.



Photo 2: Holding tanks filled with common carp during the assessment.

To: Redwood Cottonwood Rivers Control Area
Minnesota Pollution Control Agency

From: Anne Wilkinson, Wenck Associates, Inc.
Jeff Strom, Wenck Associates, Inc.

Date: February 5, 2019

Memo Subject: Redwood and Cottonwood River Watershed Lake Sediment Phosphorus Release Analysis

The Redwood Cottonwood Rivers Control Area (RCRCA) contracted with Wenck Associates, Inc. (Wenck) for the Redwood and Cottonwood River Watershed-wide total maximum daily load (TMDL) studies. As part of this contract, Wenck Associates collected sediment cores on four of the impaired lakes (Benton, Double School Grove and Sleepy Eye Lakes) included in the TMDL studies to better characterize potential drivers of internal load. This memo presents the results of the sediment phosphorus release analysis which includes the following components:

- ▲ Review of temperature and dissolved oxygen (DO) profile data
- ▲ Anoxic Factor (AF) calculations
- ▲ Sediment core collection and laboratory analysis
- ▲ Sediment phosphorus release estimates

Water Column Profile Results

Water column stability can have a significant impact on phosphorus loading and lake nutrient cycling. Lake stratification, mixing, and absence of DO can all affect whether a lake releases phosphorus from benthic sediments. Temperature and DO profiles have been recorded for each lake over the past 20 years, most recently in 2017. These profiles show lake stratification occasionally occurs during the summer growing season in all the lakes in this study. Low oxygen ($DO < 5.0$ mg/L) and anoxic ($DO < 2.0$ mg/L) conditions have been observed in the hypolimnion in Benton and Sleepy Eye. Stratification establishes anywhere from 5-9 feet below the surface during the summer season. The profiles also showed that large storm events, high winds and changes in air temperatures can cause stratification to weaken and breakdown during the summer growing season which results in mixing and re-oxygenation throughout the water column. Table 1 summarizes observed stratification and DO conditions for the four lakes in which sediment cores were collected for the Redwood and Cottonwood TMDL studies (Benton, School Grove, Double and Sleepy Eye). Table 2 summarizes observed stratification and DO conditions for the six other impaired lakes in the Redwood and Cottonwood River watersheds which sediment cores were not collected.

Table 1. Stratification and DO profile summary for the sediment cored lakes.

Parameter	Unit	Benton	School Grove	Double	Sleepy Eye
Year(s)		4	4	2	5
Summer Growing Season Profiles	[Count]	13	10	9	18
Profiles Demonstrating Stratification	[Count]	2	4	2	4
Profiles Demonstrating DO < 5.0 mg/L	[Count]	2	-	-	3
Profiles Demonstrating DO < 2.0 mg/L	[Count]	1	-	-	13
Ave Depth of Stratification	[ft]	5.1	5.7	6.6	9.4
Ave Depth of DO <5.0 mg/L	[ft]	4.5	-	-	14.9
Ave Depth of DO <2.0 mg/L	[ft]	6.6	-	-	15.5

Table 2. Stratification and DO profile summary for other impaired lakes in the Redwood and Cottonwood River watersheds.

Parameter	Unit	Dead Coon	Goose	Clear (Lyon Co.)	Bean	Rock	Clear (Brown Co.)
Year(s)		4	3	1	2	4	2
Summer Growing Season Profiles	[Count]	13	11	0	10	14	4
Profiles Demonstrating Stratification	[Count]	2	1	-	5	2	1
Profiles Demonstrating DO < 5.0 mg/L	[Count]	2	3	-	1	1	3
Profiles Demonstrating DO < 2.0 mg/L	[Count]	-	-	-	3	-	2
Ave Depth of Stratification	[ft]	1.5	2.15	-	2.1	1.5	1.5
Ave Depth of DO <5.0 mg/L	[ft]	2.1	2.3	-	3.4	2.5	-
Ave Depth of DO <2.0 mg/L	[ft]	-	-	-	3.2	-	2.4

Anoxic Factor Estimates

Shallow lakes, like the lakes presented here, often demonstrate short periods of anoxia due to instability of stratification, which can last a few days or even a few hours, that are often missed by periodic field measurements. Thus, the following equation was used to estimate the anoxic factor for all shallow lakes in this TMDL study (Nürnberg 2005):

$$AF_{\text{shallow}} = -35.4 + 44.2 \log(\text{TP}) + 0.95 z/A^{0.5}$$

Where TP is the average summer phosphorus concentration of the lake, z is the mean depth (m) and A is the lake surface area (km²).

The shallow lakes equation provides an AF estimate based on an empirical relationship with AF being a function of lake bathymetry and TP concentration, however, when DO oxygen data is available, the AF can be estimated directly, by calculating the number of days in which there is observed anoxia above the sediments. The anoxic factor is expressed in days but is normalized by the area of the lake. The anoxic factor is then used along with a sediment release rate to estimate the total phosphorus load from the sediments.

Anoxic factors were estimated using both the shallow lakes equation and the DO profiles collected at the four lakes in which sediment cores were collected and the other impaired lakes in the Redwood and Cottonwood River watershed (Table 3).

Table 3. Anoxic Factor Estimates for the sediment cored lakes.

Lake	Anoxic Factor Estimation		
	Shallow Lake Eq (days)	DO Profiles (days)	Average (days)
Benton	58.9	19.7	39.3
School Grove	55	-	55
Double	62.2	-	62.2
Sleepy Eye	49.8	14.4	32.1

NOTE: section 2 of the table compares AF estimates for lakes without sediment core data
¹average of two years (2007 and 2008)

Table 4. Anoxic Factor Estimates other impaired lakes in the Redwood and Cottonwood River watersheds.

Lake	Anoxic Factor Estimation		
	Shallow Lake Eq (days)	DO Profiles (days)	Average (days)
Dead Coon	64.42	56.7	60.6
Goose	61.4	128.2	94.8
Clear (Lyon Co.)	61.5	-	61.5
Bean	61.3	30.7	46
Rock	68.5	-	68.5
Clear (Brown County)	49.8	14.43	35.1

Sediment Core Results

Three intact sediment cores were collected at one location in Benton, School Grove and Double Lakes on June 27th and 28th, 2018. For Sleepy Eye Lake, three cores were collected at two locations (one dredged location and one un-dredged location) on June 28th to assess potential impacts of dredging on phosphorus release from the sediment. Sediment cores were collected using a gravity sediment coring device (Aquatic Research Instruments, Hope ID) equipped with an acrylic core liner (6.5-cm ID and 50-cm length). In general, the sediment core locations coincide with the long-term water quality monitoring site for each lake. The sediment cores were transported to the University of Wisconsin - Stout Discovery Center Laboratory where they were analyzed for phosphorus release under anoxic conditions.

Anaerobic phosphorus release rates for Redwood/Cottonwood lakes are range from 3.8-9.2 mg/m²/day (Table 3). Sleepy Eye Lake had the lowest rates of of phosphorus release (3.8-4.8 mg/m²/day) which are near the 25th percentile for release rates measured in lakes throughout Minnesota. Benton and Double show the highest release rates, 9.1 and 9.2 mg/m²/day, respectively. These rates are considered high and near the 75th percentile for release rates measured in Minnesota lakes. Sleepy Eye and School Grove are both near the 50th percentile for release rates measured in Minnesota lakes.

Table 3. Anaerobic phosphorus release rates.

Lake	Anaerobic Release Rate (mg/m ² /day)	Other MN Lakes		
		25 th Percentile	Median	75 th Percentile
Lake Benton (Lincoln Co.; Redwood River)	9.1	2.7	5.1	9.3
School Grove Lake (Lyon Co.; Redwood River)	5.9			
Double Lake (Cottonwood Co.; Cottonwood River)	9.2			
Sleepy Eye Lake (Un-dredged; Brown Co.; Cottonwood River)	3.8			
Sleepy Eye Lake (Dredged; Brown Co.; Cottonwood River)	4.8			

References

Nürnberg, G. 2005. Quantification of Internal Phosphorus Loading in Polymictic Lakes. Verhandlungen Internationalen Vereinigung Limnologie (SIL). Vol. 29.

Appendix C – WWTF DMR Data Summary

Table C-1. WWTF Effluent TSS Summary (2008-2017).

Facility	Number of Samples	TSS (ave; mg/L)	TSS (min; mg/L)	TSS (max; mg/L)	Samples exceeding 65mg/L	Facility Monthly Limit
ACME Brick Great Lakes Plant	24	8	2	19	0	45
August Schell Brewing Co	34	3	1	9	0	30
Balaton WWTP	45	15	2	68	1	45
Clements WWTP	25	12	2	50	0	45
Del Monte Foods Inc - Sleepy Eye Plant 114	88	23	2	170	3	30; 45
Garvin WWTP	43	8	1	24	0	45
Highwater Ethanol LLC	4	9	7	10	0	30
Lamberton WWTP	29	14	4	45	0	45
Lucan WWTP	47	32	6	89	4	45
New Ulm WWTP	5	4	3	6	0	30
Revere WWTP	25	41	7	124	3	45
Sanborn WWTP	24	12	3	51	0	45
Sleepy Eye WWTP	49	8	0	22	0	45
Springfield WWTP	120	5	2	11	0	30
Storden WWTP	32	30	2	97	1	45
Tracy WWTP	104	14	2	54	0	45
Wabasso WWTP	120	9	1	21	0	30
Walnut Grove WWTP	120	9	1	26	0	30
Wanda WWTP	28	7	2	18	0	45
Westbrook WWTP	40	24	3	309	2	45

Note: Samples refer to single monthly reported value

Table C-2. WWTF Effluent Fecal Coliform Summary (2005-2019).

Facility	count	min	max	Geomean (#/100ml)	samples >200/ml	% >200/ml
Sleepy Eye WWTP	44	10	464	33	6	14%
Westbrook WWTP	41	10	530,000	36	5	12%
Balaton WWTP	47	1	292	5	1	2%
Garvin WWTP	45	1	2,420	5	2	4%
Walnut Grove WWTP	89	1	630	13	2	2%
Revere WWTP	21	1	2,420	22	2	10%
Storden WWTP	37	1	2,420	5	1	3%

Appendix E – CAFO List and Watershed Summary

Table E- 1. List of CAFOs by HUC-10 subwatershed in the Cottonwood River Watershed.

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
Headwaters – Cottonwood River	083-50002	973	N
	083-50003	1440	N
	083-50015	300	N
	083-60847	140	N
	083-62344	400	N
	083-62428	473.5	N
	083-62444	650	N
	083-62543	285	N
	083-62553	693	N
	083-62704	57.8	N
	083-62734	150	N
	083-62825	1080	N
	083-62848	602.5	Y
	083-62856	490	N
	083-62862	386	N
	083-62863	300	N
	083-62926	999	N
	083-62928	660	N
	083-63509	138	N
	083-63783	169	N
	083-65527	297.5	N
	083-80220	980	N
	083-83840	711	N
	083-89079	600	N
	083-98301	1248	N
	083-100060	600	N
	083-104800	210	N
	083-105640	66	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	083-109880	2700	N
	083-113093	980	N
	083-113278	720	N
	083-119803	820	N
	083-121082	720	N
	083-121083	60	N
	083-124355	600	N
	083-125550	299	N
Meadow Creek	083-50012	700	N
	083-50014	840	N
	083-50024	1248	N
	083-60844	500	N
	083-61769	88	N
	083-61770	540	Y
	083-61803	373	N
	083-62112	177	N
	083-62170	500	N
	083-62425	395	N
	083-62427	500	N
	083-62441	165	N
	083-62541	210	Y
	083-62542	210	Y
	083-62563	525	N
	083-62691	200	N
	083-62709	720	N
	083-62737	238.6	N
	083-62842	880	N
	083-65081	397	N
	083-68166	485	N
	083-87104	4500	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	083-106440	72	N
	083-111440	285	N
	083-121434	202.5	N
	083-121438	190	N
	083-125701	720	
	083-125800	1440	
	083-125999	720	
	083-126540	720	N
Plum Creek	083-50007	2520	
	101-68937	590	N
	101-68950	54	N
	101-77051	50	N
	101-77080	270	N
	101-77154	160.2	N
	101-77185	74	N
	101-77400	231	N
	101-88975	171	N
	101-88981	660	N
	101-88985	120	N
	101-88990	133	N
	101-89012	132	Y
	101-89021	420	N
	101-89037	340	N
	101-107508	85	N
	101-107847	110	N
	101-107848	30	Y
	101-107849	56	N
	101-107853	75.9	N
	101-119167	150	N
	101-121921	200	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	101-126420	720	N
	127-50083	240	N
	127-50084	845	N
	127-50085	620	N
	127-62486	95	N
	127-62506	60	N
	127-62745	158	N
	127-62750	222	N
	127-63074	999	N
	127-63123	84	N
	127-63790	268	N
	127-105560	390	N
	127-114503	97.5	N
Pell Creek – Cottonwood River	033-97854	23.5	Y
	033-97989	60	N
	083-50010	20	Y
	083-50011	48	Y
	083-50029	1200	N
	083-50030	750	N
	083-62706	195	N
	083-62836	20.6	Y
	083-63796	50	N
	083-65618	71	N
	083-119884	1440	N
	101-107850	1470.5	N
	127-50031	888.5	N
	127-50056	295	N
	127-50061	698.4	N
	127-50063	1728	Y
	127-50066	166	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	127-50080	632.5	N
	127-50097	90	N
	127-60086	95	N
	127-62328	141	N
	127-62472	180	N
	127-62507	321.5	N
	127-62694	350	N
	127-62954	154	N
	127-62959	62	N
	127-62969	162	N
	127-65083	346	N
	127-65084	142.5	N
	127-65520	270	N
	127-80028	131	N
	127-80102	1200	N
	127-98160	990	N
	127-99980	936	N
	127-105720	600	N
	127-117681	735	N
	127-125907	375	
Dutch Charley Creek	033-50001	1177	N
	033-50006	4480	Y
	033-60187	1715	N
	033-97860	720	N
	033-97879	265	N
	033-97881	845	N
	033-97882	210	N
	033-97908	600	N
	033-97910	291	Y
	033-97912	80	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	033-97914	200	N
	033-97915	140	N
	033-97918	82	N
	033-97919	80	N
	033-97929	139	N
	033-97935	60	N
	033-97938	60	N
	033-97939	135	N
	033-97940	90	N
	033-97965	42	Y
	033-97970	150	N
	033-97974	980	N
	033-97976	220	N
	033-97978	122.765	N
	033-97981	290.5	N
	033-97992	139.25	N
	033-97993	150	N
	033-97997	990	N
	033-97999	150	N
	033-98002	38	Y
	033-98005	280	N
	033-98032	705	N
	033-98033	570	N
	033-98035	310.5	N
	033-98047	183	N
	033-98061	89	N
	033-98063	150	N
	033-98065	84	N
	033-98078	150	N
	033-98080	150	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	033-98081	990	N
	033-98088	200	N
	033-98095	588	N
	033-98102	141	N
	033-98107	90	N
	033-102342	990	N
	033-102566	250.3	N
	033-102577	530	N
	033-103543	60	N
	033-103552	960	N
	033-104200	1342.5	
	033-104201	990	N
	033-107458	56	N
	033-108225	250	N
	033-108322	120	N
	033-110360	1342.5	N
	033-117658	930	N
	033-120691	750	N
	033-125533	60	N
	033-125751	1290	N
	033-125896	360	N
	033-126396	720	
	101-50005	2126.4	
	101-68939	50	Y
	101-77068	399	N
	101-77069	119	N
	101-77135	120	N
	101-77141	16.3	Y
	101-77169	95	N
	101-77170	53.5	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	101-77388	180	N
	101-77389	100	N
	101-88997	50	N
	101-89033	193	Y
	101-108062	128	N
	101-108064	325	N
	101-108066	16	Y
	101-108076	60	
	101-114832	480	N
	127-50034	180.7	N
	127-62710	110	N
	127-122138	100	N
Mound Creek – Cottonwood River	015-50005	1872	N
	015-71652	33	Y
	015-71655	450	N
	015-71671	1125	N
	015-71702	497.4	Y
	015-71716	350	N
	015-71727	2936.3	N
	015-71740	171	N
	015-71744	160	N
	015-71757	120	N
	015-71787	90	N
	015-71794	195	N
	015-71810	195	N
	015-71824	192.5	N
	015-71856	285	N
	015-71872	160	N
	015-71876	78	N
	015-71889	90	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	015-71921	295	N
	015-71933	590	N
	015-71966	125.5	N
	015-72003	216	N
	015-72024	115	N
	015-72032	160	N
	015-72035	182	Y
	015-72041	900	N
	015-72075	624	N
	015-72094	91	N
	015-72098	735	N
	015-72107	900	N
	015-72127	163	N
	015-72138	225	N
	015-72147	400	N
	015-72162	990	N
	015-72168	242	N
	015-72171	55	Y
	015-72178	110	N
	015-72200	325	N
	015-72204	300	N
	015-72210	138.07	Y
	015-72217	112	Y
	015-72218	180	Y
	015-72223	315	N
	015-72233	50	N
	015-72244	840	N
	015-72246	90	Y
	015-72273	992	N
	015-72285	96.12	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	015-72315	213.6	N
	015-72317	500	N
	015-72324	50	N
	015-72328	1106	
	015-72332	160	N
	015-80242	258	N
	015-82445	85	N
	015-82469	102	Y
	015-82477	300	N
	015-93741	360	N
	015-95050	144	N
	015-95133	84	Y
	015-95136	125	N
	015-95141	300	N
	015-95145	565.5	Y
	015-95148	1106	
	015-105820	900	N
	015-105961	900	N
	015-107460	1600	N
	015-107461	295	N
	015-108312	620	N
	015-109414	810	N
	015-115876	595	N
	015-117075	421	N
	015-119172	250	Y
	015-125529	900	
	015-126342	748.5	N
	015-127146	270	N
	015-127195	990	N
	033-50011	1682	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	033-97856	480	N
	033-97885	73.126	N
	033-97894	100	N
	033-97909	210	N
	033-97922	94	N
	033-97925	56	N
	033-97926	60	N
	033-97932	217	N
	033-97933	789	N
	033-97934	60.3	N
	033-97944	72	N
	033-97948	250	N
	033-97952	343.5	N
	033-97954	265.4	N
	033-97959	211	N
	033-97962	133	N
	033-97968	950	N
	033-97975	180	N
	033-97998	300	N
	033-98016	900	N
	033-98024	55.725	N
	033-98025	209	N
	033-98038	450	N
	033-98048	482.5	N
	033-98051	61.4	N
	033-98068	780	N
	033-98069	75	N
	033-98076	930	N
	033-98089	117	N
	033-98098	998.9	Y

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	033-98099	900	N
	033-98103	999	N
	033-103542	50	N
	033-103546	240	N
	033-103548	500	N
	033-105840	900	N
	033-108226	57.7	N
	033-110813	600	N
	033-112558	900	N
	033-121655	84	Y
	127-50079	128	N
	127-62535	78.53	N
	127-62536	102	N
	127-63134	225	N
	127-98660	900	N
	127-111220	750	N
	127-125865	720	
	127-126355	990	N
Sleepy Eye Creek	015-50009	2092	N
	015-50013	1200	N
	015-60703	1640	N
	015-71726	900	N
	015-71769	390	N
	015-71982	325	N
	015-72159	315	N
	015-72207	290	N
	015-72278	65.3	N
	015-82450	70	N
	015-82459	608	N
	015-82459	608	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	015-82460	750	N
	015-82476	750	N
	015-82840	612	N
	015-125789	744	N
	015-126350	30.66	Y
	127-50001	576	N
	127-50009	120	N
	127-50010	77	N
	127-50014	427	N
	127-50023	150	N
	127-50027	1420	N
	127-50029	500	N
	127-50032	600	N
	127-50033	54.08	N
	127-50036	198	N
	127-50042	902.5	N
	127-50046	499	N
	127-50047	912.5	N
	127-50049	80	N
	127-50051	1872	N
	127-50058	553	N
	127-50059	420.1	N
	127-50060	52	N
	127-50074	290	N
	127-50086	173.5	N
	127-60040	110.4	N
	127-60085	120.5	N
	127-60520	104	N
	127-60564	57.5	N
	127-60848	350	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	127-61729	177.5	N
	127-61738	660	N
	127-61742	180	N
	127-61761	54	N
	127-62182	97.5	N
	127-62466	200	N
	127-62475	226.5	N
	127-62523	92.5	N
	127-62695	480	N
	127-62697	165	N
	127-62699	390	N
	127-62872	272.8	N
	127-62875	14.4	Y
	127-62886	312.5	N
	127-62891	150	N
	127-62899	50	N
	127-62904	268	N
	127-63122	480	N
	127-63124	83	N
	127-63151	87.5	N
	127-63155	60	N
	127-63190	96.7	N
	127-63529	299	N
	127-63758	401.4	N
	127-63781	515	N
	127-64986	90	N
	127-65613	135	N
	127-65616	660	N
	127-101040	624	N
	127-105900	900	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	127-106300	936	N
	127-106840	177.1	N
	127-107260	760	N
	127-109480	270	N
	127-109820	432	N
	127-110620	936	N
	127-112698	360	N
	127-120771	720	N
	127-124541	1440	N
	127-125564	840	N
	127-125590	744	N
	127-125731	720	N
	127-126807	133.9	N
	127-127020	990	N
Cottonwood River	015-50002	1575	N
	015-50008	1200	
	015-71647	600	N
	015-71650	93.5	Y
	015-71654	153	N
	015-71673	70.6	N
	015-71675	624	N
	015-71678	41	Y
	015-71698	78.1	N
	015-71703	495.5	N
	015-71720	306	N
	015-71737	125	N
	015-71745	59.5	N
	015-71816	120	N
	015-71852	97.9	Y
	015-71853	17	Y

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	015-71857	295	N
	015-71866	101.5	N
	015-71880	68.6	N
	015-71890	147	N
	015-71892	36	Y
	015-71905	311.8	Y
	015-71919	510	N
	015-71948	108	N
	015-71949	129.6	N
	015-71964	50	Y
	015-71968	70	N
	015-71973	57.425	N
	015-71987	98.2	N
	015-71999	60	N
	015-72029	194	N
	015-72049	108	N
	015-72059	465	N
	015-72066	163.9	N
	015-72068	80	N
	015-72074	645	N
	015-72139	1690	N
	015-72155	294	N
	015-72165	832	N
	015-72175	60	N
	015-72197	247.9	Y
	015-72226	61.075	N
	015-72236	75	N
	015-72238	675	N
	015-72282	75	N
	015-72283	60	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	015-72304	50.05	N
	015-72331	149	N
	015-72336	10.2	Y
	015-72353	95	N
	015-72357	81	N
	015-72369	128.6	N
	015-72375	196	N
	015-72395	62	N
	015-95056	318.5	N
	015-95134	72	Y
	015-95138	22.8	Y
	015-95147	247.1	N
	015-100000	1440	N
	015-107462	1200	N
	015-107843	170	N
	015-107846	123	N
	015-109481	936	N
	015-115641	80	N
	015-120278	97	N
	015-126352	102	N
	015-126800	100	N
	015--126427	85	N
	127-50088	2053	N
	127-50092	180	N
	127-50093	576	N
	127-60702	70	N
	127-61745	350	N
	127-61762	1895	
	127-62180	330	N
	127-63144	735	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	127-65511	660	N
	127-112251	800	N
	127-112801	720	N
	127-117156	945	N
	127-124992	412	

Table E- 2. Cottonwood River Watershed CAFO Summary.

General	
Total Feedlots	513
Total Permitted CAFO's	64
Total Animal Units (AUs)	228,065
Primary Animal Type ¹	Swine (53%)
	Cattle (45%)
Sensitive Areas	
Open Lot Feedlots	322
Feedlots in Shoreland	46
Open Lot Feedlots in Shoreland	37

¹Percentages are based on animal units.

Appendix D – HSPF Model Documentation



Memorandum

To: Dr. Chuck Regan, Tim Larson (MPCA) **Date:** 03/17/2016 (Revised)
From: J. Wyss, H.I.T; J. Butcher, Ph.D., P.H. **Subject:** **Minnesota River Basin HSPF Model Sediment Recalibration**
Cc: Jennifer Olson **Includes:** Electronic supplement

1 Introduction

The Minnesota River basin HSPF models have a long history. Models for six of the 8-digit Hydrologic Unit Code (HUC8) basins were originally developed by MPCA in the 1990s and subsequently expanded and calibrated to include the entire basin from Lac qui Parle to Jordan, MN by Tetra Tech in 2002. Those models were used to support the development of a nutrient/dissolved oxygen TMDL and associated wasteload allocations. Tetra Tech (2008) subsequently refined these models for sediment simulation. These models were discretized at approximately the HUC10 scale. Tetra Tech later developed finer-resolution (HUC12-scale) models of the Chippewa and Hawk-Yellow Medicine HUC8 sub-models. MPCA then contracted with RESPEC to develop HUC12-scale models of the entire basin downstream of Lac qui Parle, as well as to extend the models in time through 2012. That effort was completed in 2014.

In 2015, MPCA contracted with Tetra Tech to refine the hydrologic and sediment calibrations for the Basin. The initial review of the RESPEC models provided to MPCA by Tetra Tech suggested that hydrology was fit reasonably well; however, sediment source attribution did not match up well with the evidence available from radiometric data (e.g., Schottler et al., 2010). Subsequent analysis revealed other aspects of the hydrologic calibration that potentially affect sediment calibration. Accordingly, MPCA requested review and revisions to the hydrologic calibration as part of the sediment recalibration effort. Tetra Tech completed the hydrology recalibration in November, 2015 and then used those models to complete the sediment recalibration.

The hydrologic recalibration is summarized in *Minnesota River Basin HSPF Model Hydrology Recalibration*, submitted to MPCA on November 3, 2015. This memorandum, along with accompanying electronic files, specifically documents the sediment recalibration and validation of the Minnesota River Basin HSPF modeling system, including linked models for the following HUC8 watersheds:

- Hawk-Yellow Medicine (07020004)
- Chippewa (07020005)
- Redwood (07020006)

- Middle Minnesota (07020007)
- Cottonwood (07020008)
- Blue Earth (07020009)
- Watonwan (07020010)
- Le Sueur (07020011)
- Lower Minnesota (07020012).

2 Approach

2.1 GOALS AND OBJECTIVES FOR RECALIBRATION

The goal of this effort is to update the sediment calibration of the Minnesota River HSPF models using all relevant available sources of information including evidence on source attribution. Model performance was adjusted at all calibration gages in the watershed to meet the following objectives:

- **Formulation of sediment source attribution targets.** The MPCA was responsible for generating the first set of sediment apportionment calibration targets for Minnesota River HSPF models. The greatest amount of data is available from the detailed sediment budget study of the Le Sueur River, where estimates have been developed for sediment load deriving from upland sheet and rill erosion, ravines, channel degradation, and bluff collapse. Sediment apportionment calibration targets in the Le Sueur are based on flow and sediment measurements above and below the nick zones of active headcuts in the Le Sueur mainstem, Big Cobb River, and Maple River. Radiometric information aided in the partitioning of the field derived and channel derived sediment contributions based primarily on analysis of cores from depositional “integrator sites” (Schottler et al., 2010 plus additional ongoing work to further refine the interpretation by Schottler, as presented to Chuck Regan of MPCA, with additional information from the Le Sueur and Greater Blue Earth sediment mass balance studies of Gran et al., 2011 and Bevis, 2015).. Information from the Le Sueur Sediment Budget and other on-going work in the Greater Blue Earth watershed (Greater Blue Earth Sediment Budget) and throughout the Minnesota Basin are used to partition sediment contributions among fields, ravines, bluff, and channel incision sources. The sediment apportionment target information is summarized below in Table 1, showing the range of attributed upland loads from all sources and the current best estimate for this source.
- **Implementation of the sediment apportionment calibration targets.** The 2014 Minnesota River Basin HSPF models parameters were modified so that the amount of sediment coming from the four source categories were consistent with the calibration targets formulated in the previous task. The models were adjusted as needed to maintain acceptable levels of calibration for sediment transport.
- **Tabulation of the simulated sediment source apportionment.** For each watershed, Excel™ workbooks were created that tabulate the simulated sediment source apportionment. Each workbook is currently set up to supply simulated sediment source apportionment at instream calibration and validation stations for each watershed. They have been created in such a way that the workbooks can easily be modified to provide simulated sediment source apportionment at any pour point in each model. Each workbook uses standard model output from the HBN file so the

structure of the 2014 Minnesota River Basin HSPF models did not need to be modified to generate these results.

- **Assess the per-acre sediment loading rates for all of the pervious and impervious land classes in each model.** The 2014 Minnesota River Basin HSPF models generated per-acre upland sediment loading rates that are inconsistent with current constraining information. The models were adjusted as needed to make the sediment loading rates consistent with current constraining information.
- **Maintain acceptable fit between observed and simulated loads and concentrations** as recommended by MPCA’s modeling guidance (AQUA TERRA, 2012). The existing calibration for sediment in the 2014 models appears to provide a decent fit to observations of suspended sediment concentrations, but the source apportionment is not consistent with available evidence and statistical analysis of model fit was not presented in RESPEC (2014). The objective of this work is to develop models that conform to constraining information on sediment source apportionment and annual loads while maintaining a high quality fit to instream observations of suspended sediment concentrations. The multi-objective calibration helps ensure a robust model; however, assuring an appropriate fit to source attribution information does appear to make it more difficult to match instream observations.

Table 1. Sediment Apportionment Calibration Targets

HUC8	Upland Best Estimate	Upland Range	Ravine	Bluff	Stream
Chippewa	31%	30-31%	ND	ND	ND
Redwood	23%	21-25%	ND	ND	ND
Yellow Medicine	ND	ND	ND	ND	ND
Cottonwood	21%	21-41%	ND	ND	ND
Watonwan	27%	27-41%	7%	43%	21%
Le Sueur	27%	12-27%	9%	57%	8%
Blue Earth	26%	19-28%	5%	55%	18%
Middle	27%	16-27%	ND	ND	ND
Lower/Metro	23%	14-31%	ND	ND	ND

2.2 SEDIMENT PERFORMANCE METRICS

Sediment is one of the more difficult water quality constituents to represent accurately in watershed and stream models. Important aspects of sediment behavior within a watershed system include loading and erosion sources, delivery of these eroded sediment sources to streams, drains and other pathways, and subsequent instream transport, scour and deposition processes (USEPA, 2006).

Sediment calibration for watershed models involves numerous steps in estimating model parameters and determining appropriate adjustments needed to insure a reasonable simulation of the sediment sources on the watershed, delivery to the waterbody, and transport behavior within the channel system. Rarely is there sufficient observed local data at sufficient spatial detail to obtain a unique calibration for all

parameters for all land uses and each stream and waterbody reach. Consequently, model users focus the calibration on sites with observed data and review simulations in all parts of the watershed to ensure that the model results are consistent with field observations, historical reports, and expected behavior from past experience (Donigian and Love, 2003, AQUA TERRA, 2012).

The level of performance and overall quality of sediment calibration is evaluated in a weight of evidence approach that includes both visual comparisons and quantitative statistical measures. For this effort, the models were already stated to be calibrated for sediment, but did not match evidence on source attribution. Therefore, the primary focus of the model re-calibration was on approximating the source attribution evidence. We also adopted a philosophy, consistent with the RESPEC model representation, of using a parsimonious parameter set in which the parameter KSER, which controls washoff of upland sediment, were generally held constant for a given land use within a HUC8 basin. Similarly, the instream critical shear stresses for scour and deposition were held to narrow and consistent ranges. This approach leads to a robust model that is not over-fit to uncertain data and the fine-scale factors that may skew observations at individual stations; however, it also can reduce the apparent quality of fit in comparing model predictions to observations at individual stations.

The standard approach to sediment calibration focuses on the comparison of model predictions and observed total suspended solids or suspended sediment concentration data. Given the inherent errors in input and observed data and the approximate nature of model formulations, absolute criteria for watershed model performance are not generally considered appropriate by most modeling professionals. Yet, most decision makers want definitive answers to the questions—“How accurate is the model?” and “Is the model good enough for this evaluation?” Consequently, the current state of the art for model evaluation is to express model results in terms of ranges that correspond to “very good”, “good”, “fair”, or “poor” quality of simulation fit to observed behavior. These characterizations inform appropriate uses of the model: for example, where a model achieves a good to very good fit, decision-makers often have greater confidence in having the model assume a strong role in evaluating management options. Conversely, where a model achieves only a fair or poor fit, decision makers may assign a less prominent role for the model results in the overall weight-of-evidence evaluation of management options.

For HSPF and similar watershed models, a variety of performance targets for comparison to observed suspended sediment concentrations have been documented in the literature, including Donigian et al. (1984), Lumb et al. (1994), Donigian (2000), and Moriasi et al. (2007). Based on these references and past experience, HSPF performance targets for sediment are summarized in Table 2.

Table 2. Performance Targets for HSPF Suspended Sediment Simulation (Magnitude of Annual and Seasonal Relative Mean Error (RE); daily and monthly NSE)

Model Component	Very Good	Good	Fair	Poor
Sediment	≤ 20%	20 - 30%	30 - 45%	> 45%

It is important to clarify that the tolerance ranges are intended to be applied to mean values, and that individual events or observations may show larger differences and still be acceptable (Donigian, 2000).

Where model fit to observations is rated less than “good” this can be due to deficiencies in the model simulation of sediment, deficiencies in the model simulation of hydrology, deficiencies in the flow gage and water quality monitoring records, or a combination of the three. Model calibration typically assumes that the observed records are “correct” and maximizes the fit of the model to those records. It is clear in some cases, however, that uncertainty in the monitoring record itself is a major contributor to poor predictability. This is most likely to be true for stations that have short periods of record, locations that are impacted by backwater effects, and sites with unstable channels at which rating curve adjustments (which are essential to the simulation of shear stress and sediment scour and deposition) have not been

frequently revised. In addition, most of the observed data consist of grab samples that represent a specific point in space and time. These are compared to model predictions that represent a daily average over a whole model reach (typically several miles in length) that is assumed to be completely mixed. An instantaneous grab sample may not be representative of an average concentration over the course of a day, and small errors in the timing of storm flows will propagate into apparent error in the fit to suspended sediment concentration. Further, observations at a specific spatial location may be affected by local conditions, such as bridge scour, that deviate from the average over the whole reach. As a result, calibration is an inexact science that must proceed by a weight-of-evidence approach.

2.3 CALIBRATION AND VALIDATION/CORROBORATION

Traditional model validation is intended to provide a test of the robustness of calibrated parameters through application to a second time period. In watershed models, this is, in practice, usually an iterative process in which evaluation of model application to a validation period leads to further adjustments in the calibration. A second, and perhaps more useful constraint on model specification and performance is a spatial calibration/corroboration approach in which the model is tested at multiple gages on the stream network to ensure that the model is not over parameterized to fit any one gage or collection of gages. In particular, obtaining model fit to numerous gages at multiple spatial scales from individual headwater streams to downstream stations that integrate across the entire Minnesota River basin helps to ensure that the model calibration is robust. This is especially appropriate for the present model recalibration effort in which the full set of available data has already been used to develop the initial model calibration.

The overall model application period is 1/1/1995 – 12/31/2012. Typical sediment sampling frequencies range from once a week to once a month, but often cover only a subset of years within the overall application period. All of the sediment samples at a gage were used as a full record for that gage and no split sample calibration/validation periods were adopted. Instead a spatial distribution of calibration and validation stations was selected in which initial efforts focused on the “calibration” stations, followed by additional testing and refinement using the corroboration stations. Generally, headwater and upstream gages are considered corroboration stations, which ensures that a corroboration station is not downstream of a calibration station and thus represents a semi-independent test of the model parameterization. Note, however, that model fit to observations is likely to decline for stations with smaller drainage areas because these stations are likely to have flashier responses that amplify the potential discrepancy between grab sample observations and model daily average predictions.

2.4 COMPONENTS NOT ADJUSTED

The adjustments to the sediment calibration are conditional on accepting several aspects of the RESPEC model development (RESPEC, 2014). Most of these were discussed in the hydrology recalibration memo:

- Development and assignment of meteorological forcing time series, including the calculation of potential evapotranspiration, was not adjusted. The models are forced by rainfall gauge records, which have in many instances have been shown not to be representative of areal average precipitation totals during large convective summer storm events.
- Point source discharges are accepted as specified by RESPEC.
- The RESPEC models use a degree-day method for the simulation of snow melt in which melt is estimated solely as a function of air temperature. This provided a good fit to the overall water balance at most stations, but is less adept at simulating rapid changes in the snow balance and does not account for sublimation from the snow pack.

- Hydraulic functional tables (FTables) are not altered from the RESPEC models. Lake simulation is also as set up by RESPEC. Most of the stream reach FTables appear to be specified based on regional hydraulic geometry information and do not incorporate measured channel cross section data¹. This can bias simulation of channel shear stresses, especially during large storm events.

Also significant to the sediment recalibration are the following:

- The RESPEC models represent sediment contributions from tile drains with surface inlets through the use of GENER statements. The methodology used to generate tile drain sediment loads in this application is unchanged; however, the area factors associated with the GENER statements were updated to properly represent the modifications made to separate agricultural lands by hydrologic soil group (HSG), as described in Section 4. Examination of the approach to simulating tile drain sediment in these models indicates a much more rapid response and quick recession of sediment loads compared to those represented through Special Actions in the Tetra Tech (2008) models.
- The setup of which land uses contribute mass scour (ravine erosion) from the uplands was unchanged. The RESPEC models assign ravine erosion to agricultural lands and to the special bluff and ravine land uses. With the exception of the bluff and ravine land uses (where scour rates were increased to generate considerably more sediment from the land), the setup for ravine erosion is unchanged from what RESPEC provided; however, the results will differ due to the revisions to model hydrology.
- The partitioning from upland total sediment yield to instream sand, silt, and clay fraction loads is not modified from what RESPEC provided.
- Initial stream bed composition of sand, silt, and clay is not modified from what RESPEC provided.
- The Chippewa model received from RESPEC and adapted from the earlier Tetra Tech model is set up with an additional general quality constituent simulating sediment load independent of sheet and rill or gully erosion. This was done because suspended solids concentrations at the upstream station on the Chippewa River at Cyrus have an atypical relationship to flow. That is, high concentrations of TSS often occur at relatively low flows, while the concentration tends to decrease for higher flows. This suggests the presence of an approximately constant load of solids that is independent of flow, such as could occur from extensive animal activity in the stream or sand mining operations. This approach was not modified for the sediment recalibration.

3 Calibration Gage Sites

A total of 63 in-stream water quality stations were used for the Minnesota River Basin HSPF model sediment recalibration. All selected in-stream stations have at least 100 TSS samples during the simulation period. Additionally, with the exception of Watonwan (Watonwan has only one station with more than 100 samples) at least three stations were included for each HUC8. As previously discussed the stations were split into calibration (31 stations) and corroboration (32 stations) based on spatial

¹ The RESPEC memoranda say that for reaches where Tetra Tech previously calculated FTables using results of HEC-RAS models, those FTables “will be scaled by reach length and applied to corresponding reaches in order to maximize the use of the best available data.” For reaches that did not have HEC-RAS models, the documentation implies that cross-sectional measurements at USGS gage sites will be used, and, when field information on a gage is not available, “The USGS maximum width, depth, and area data will be used to calculate cross-sections assuming a trapezoidal channel and a bank slope of 1/3.”

information. The in-stream water quality stations used for sediment calibration and corroboration are listed in Table 3.

Table 3. Sediment Calibration and Corroboration Stations

Site	HUC 8	HYDSTRA ID	STORET ID	Period of Record	Type
Chippewa R at 140th St, 7 mi N of Cyrus	7020005	276033	S002-190	5/1999 - 9/2012	Calibration
Chippewa R at CSAH-22, 1 mi E of Clontarf	7020005	276036	S002-193	5/1998 - 9/2012	Calibration
Shakopee Ck, at Unn Twnshp Rd, 1 mi W Mn-29, 8 mi*	7020005	276043	S002-201	5/1998 - 9/2012	Calibration
Chippewa R, at MN-40, 5.5 mi E of Milan	7020005	276045	S002-203	5/1998 - 12/2012	Calibration
Dry Weather Creek, at 85th Ave NW, 4 mi NE of Wat*	7020005	276046	S002-204	5/1998 - 9/2012	Corroboration
Shakopee Ck S Andrew Rd at Lk Andrew Otl 4.5 mi W*	7020005	276051	S002-209	6/1996 - 10/2007	Corroboration
Little Chippewa R at MN-28, 4 mi W of Starbuck	7020005	276146	S004-705	3/2007 - 9/2009	Corroboration
Chippewa R, EB, at 15th Ave Ne, 2.5 mi N of Benson	7020005	276156	S005-364	5/1998 - 9/2012	Corroboration
W Fk Beaver Ck at CSAH-4 6.5 mi S of Olivia	7020004	275971	S000-405	6/1999 - 9/2009	Corroboration
Beaver Ck at CSAH-2 2.5 mi NE of North Redwood	7020004	275976	S000-666	6/1999 - 9/2012	Calibration
Sacred Heart Ck at CSAH-15 Br, 5 mi NW of Delhi, *	7020004	275988	S001-341	4/1999 - 9/2012	Corroboration
Hawk Ck at Cr 52 Br, 6.5 mi SE of Granite Falls	7020004	276009	S002-012	6/1999 - 12/2012	Calibration
Palmer Ck at 15th Ave Se, 2 mi NW of Granite Falls	7020004	276010	S002-136	4/1999 - 9/2012	Corroboration
Hawk Ck, at Cr-116, 1.25 mi S of MN-40, 4.2 mi SW*	7020004	276014	S002-140	6/1999 - 9/2012	Corroboration
Hawk Ck, at MN-23, 2.2 mi SW of Maynard	7020004	276022	S002-148	6/1999 - 9/2012	Calibration
Chetomba Ck, at Unnamed Twp Rd, 5 mi SE of Maynard	7020004	276026	S002-152	6/1999 - 9/2012	Corroboration
Yellow Med R, 1 1/3 mi No CSAH-18, 5 1/4 mi NE Ha*	7020004	276068	S002-316	4/2001 - 10/2012	Calibration
So Br Yellow Medicine R On CSAH-26, 4 mi N Minneo*	7020004	276071	S002-320	4/2001 - 8/2012	Corroboration
Cd-119 at CSAH-15, 5.6 mi S of Sacred Heart, Minn*	7020004	276116	S003-866	4/2005 - 8/2012	Corroboration
Timms Ck at CSAH-15, 2.8 mi NNE of Delhi, Minneso*	7020004	276117	S003-867	4/2005 - 8/2012	Corroboration
MM R 500 Ft S CSAH-13 near USGS Gage House Dwnst *	7020004	276123	S004-649	3/2007 - 12/2012	Calibration
Minnesota R, Ethanol Facility Water Supply Intake*	7020004	276349	S007-748	2/2007 - 1/2008	Calibration
Redwood R at CSAH-15 In Russell	7020006	272519	S000-696	5/2001 - 9/2012	Calibration
Redwood R at CSAH-17, 3 miles SW of Redwood Falls	7020006	272872	S001-679	3/1996 - 9/2012	Calibration
Clear Ck Cr-56, 1/3 mi upst conflu Redwd R, NE Ed*	7020006	272541	S002-311	3/1996 - 9/2012	Corroboration
Three mile Ck at Cr-67, 1 mi No of Green Valley	7020006	273019	S002-313	3/1996 - 10/2011	Corroboration
Plum Creek at CSAH 10 Br, 4.75 mi NE of Walnut Gr*	7020008	273015	S001-913	4/1997 - 7/2012	Corroboration
Cottonwood R near MN-68 And Cottonwood St In New *	7020008	273017	S001-918	4/1997 - 10/2011	Calibration
Sleepy Eye Cr at CSAH 8 Br, 2.2 mi N of Leavenwor*	7020008	272478	S001-919	4/1997 - 9/2012	Corroboration
Cottonwood R at CSAH 8 Br, 0.4 mi N of Leavenwort*	7020008	272479	S001-920	4/1997 - 9/2012	Calibration
Cottonwood R at Us-14 Brg, 1 mi NE of Lamberton	7020008	272532	S002-247	5/2000 - 9/2012	Calibration
Watowwan R Br On CSAH-13, 1 mi W of Garden City	7020010	272526	S000-163	10/1996 - 3/2012	Calibration
Le Sueur R MN-66 1.5 mi NE of Rapidan	7020011	272867	S000-340	1/2005 - 7/2012	Calibration
Unn Trib To Big Cobb R, Sh22 0.5 mi N Beauford	7020011	273013	S001-210	1/2005 - 9/2012	Corroboration
Maple R at CSAH 35 5.2 mi S of Mankato, MN	7020011	272950	S002-427	4/2003 - 8/2012	Calibration
Cobb R at CSAH-16, 4.4 mi NE of Good Thunder, MN	7020011	272629	S003-446	3/2006 - 9/2011	Calibration
Le Sueur R at CSAH 28 in Saint Clair, MN	7020011	273029	S003-448	3/2007 - 6/2012	Corroboration
Little Cobb near CSAH-16, 6.3 mi W of Pemberton, *	7020011	272962	S003-574	1/2005 - 9/2012	Corroboration
Le Sueur R at CSAH-8, 5.1 mi SSE of Mankato, MN	7020011	272617	S003-860	3/2006 - 9/2011	Calibration
Maple R at CSAH-18, 2 miles North of Sterling Cen*	7020011	272627	S004-101	4/2006 - 9/2012	Corroboration
Blue Earth River 150 Ft dwst of Rapidan Dam	7020009	272948	S001-231	1/2005 - 3/2012	Calibration
Dutch Creek at 100th St, 0.5 miles W of Fairmont	7020009	272881	S003-000	4/2000 - 10/2008	Corroboration
Center Creek at 315th Avenue - 1 mi S of Huntley	7020009	272608	S003-024	2/2002 - 10/2008	Corroboration
Elm Creek at 290th Ave - 4.5 mi NE of Granada	7020009	272609	S003-025	2/2002 - 10/2008	Calibration
Minnesota River at Mankato, MN	7020007	273053	S325000	3/1996 - 8/2007	Calibration
Minnesota R Bridge On Us-71 And MN-19 at Morton	7020007	272517	S000-145	10/2000 - 10/2011	Calibration
Minnesota R at CSAH 42 at Judson	7020007	272509	S001-759	1/2005 - 2/2012	Calibration
Sevenmile Ck dwst of MN-99, 6 mi SW of St. Peter	7020007	272646	S002-934	4/1996 - 8/2011	Corroboration
Cty Dtch 46A dwst of CSAH-13, 6 mi SW of St. Peter	7020007	272880	S002-936	4/2000 - 9/2011	Corroboration
Sevenmile Ck in Sevenmile Ck Cty Pk, 5.5 mi SW of*	7020007	273028	S002-937	4/1996 - 9/2011	Calibration
Minnesota R at MN-99 in St. Peter, MN	7020007	273031	S004-130	1/2005 - 2/2012	Calibration
Little Cottonwood R at Apple Rd, 1.6 mi S of Courtland	7020007	273033	S004-609	4/1996 - 6/2010	Corroboration
High Island Cr., CSAH-6 By Henderson	7020012	272518	S000-676	6/1998 - 9/2012	Calibration

Site	HUC_8	HYDSTRA ID	STORET ID	Period of Record	Type
Rush River, Sh-93 By Henderson	7020012	272599	S000-822	6/1998 - 9/2012	Calibration
Bevens Cr.,CSAH-41 By East Union	7020012	272871	S000-825	2/1998 - 9/2011	Calibration
Silver Cr.,CSAH-41 By East Union	7020012	272600	S000-843	6/2000 - 8/2011	Corroboration
Buffalo Ck, at 270th St, 1.5 mi NW of Henderson	7020012	272468	S001-807	5/2000 - 9/2012	Corroboration
High Island Ck at CSAH 9, 1 mi NW of Arlington	7020012	272482	S001-891	5/2000 - 9/2012	Corroboration
Carver Ck at Us-212, 2.5 mi E of Cologne, MN	7020012	273022	S002-489	5/1997 - 9/2011	Corroboration
Carver Ck at Cr-140, 2.3 mi NE of Benton, MN	7020012	272489	S002-490	5/1997 - 9/2011	Corroboration
Bevens Ck at 321st Ave, 3 mi SE of Hamburg, MN	7020012	272503	S002-516	11/1999 - 9/2011	Corroboration
Bevens Ck at Rice Ave, 3.9 mi SE of Norwood Yng America	7020012	272470	S002-539	5/1997 - 9/2011	Corroboration
W Chaska Ck, 250' W of Cty Rd 10, behind VFW, in *	7020012	272472	S002-548	4/1998 - 9/2011	Calibration

* Name truncated in RESPEC database

4 Model Updates

4.1 MODEL STRUCTURAL RECONFIGURATION

After consultation with MPCA, a number of changes were made in the structure of the 2014 models. These included subdivision of agricultural land to separate hydrologic soil group (HSG) classes and separation of cropland areas receiving manure applications – both of which may be useful for development of model scenarios. The reconfiguration of the models is described below.

- Separation of cropland into two classes based on HSG.** Most of the agricultural land in the watershed incorporates tile drainage to improve spring water balance, with intensity of tile drainage generally being greatest in the lacustrine soils of the Le Sueur watershed and adjacent parts of the Blue Earth and Middle Minnesota 8-digit HUCs. The RESPEC (2014) models (exclusive of the Chippewa and Hawk-Yellow Medicine models developed by Tetra Tech) lumped all cropland into two conventional and conservation tillage groups regardless of soil type, which precludes identification of critical areas with marginal soil characteristics. This was rectified by reprocessing the land use information and generating four cropland classes representing Cropland – Conservation Till (HSG A,B), Cropland – Conservation Till (HSG C,D), Cropland – Conventional Till (HSG A,B), and Cropland – Conventional Till (HSG C,D), where the HSG class for cropland is the designation “with drainage” for dual classification soils (i.e., B/D soils are soils that have B characteristics when drained) under the assumption that tile drainage is ubiquitous where it is necessary to improve production performance in the corn belt. This change was implemented before the completion of the hydrology recalibration but not discussed in the November 2015 memo.
- Representation of manured lands.** For all models except Chippewa and Hawk Yellow Medicine, land receiving manure application was not explicitly represented in the RESPEC (2014) models. The models were set up with a land use called “Cropland – Reserved” for this purpose, but this land use was assigned no area in the 2014 models. The Cropland – Reserved category was changed to “Manure Application (conventional A,B)” and area from Cropland – Conventional Till (HSG A,B) was changed to the Manure Application land use to reflect the estimated acreage that receives manure application. We assumed that manure would primarily be applied to land with better drainage, as the (A,B) grouping (with drainage) is also the dominant component of the overall cropland area, and also that regular manure application is not generally consistent with conservation tillage maintenance of residue cover. The decision by MPCA to incorporate this change in the model structure occurred after the hydrology recalibration and most of the sediment recalibration was complete. To have no net impact on the hydrology and

sediment recalibrations, the manured land was reassigned solely from Cropland – Conventional Till (HSG A,B) and the hydrologic and sediment parameters for manured land were set equal to those for Cropland – Conventional Till (HSG A,B). This was the approach that used in the 2008 TMDL model as well.

- **Separation of Lower Minnesota model into two models.** The increase in the number of model pervious upland land units (PERLNDs) due to the cropland and manured area modifications increased the number of operations in the Lower Minnesota model beyond the upper limit for the current version of the HSPF model. The 2014 Lower Minnesota model was split into two separate linked models: a revised Lower Minnesota model incorporating all sub-basins upstream of and including reach 310 and a new “Metro” Minnesota that incorporates the portion of the original Lower Minnesota model downstream of reach 310.
- **Representation of bluff land area.** The RESPEC (2014) models include the land area in bluffs (as shown on a spatial coverage of bluff area developed in 2011-2012 and provided by MPCA) for all the models except for Chippewa and Hawk Yellow Medicine. There is newer work in progress to better delineate bluffs from LiDAR elevation data; however, those coverages are not yet suitable for use as they identify many small features, such as ditch banks, as bluffs, which is not consistent with the characterization of bluff areas in the model. Similarly, ravine land use has been identified as a separate coverage in the Le Sueur watershed, but work is not complete in other basins (although ravine loading is simulated as a part of the general crop land simulation). Both the bluff and ravine coverages should be updated when this ongoing work is completed. For the present round of models, bluff land use area (as shown on the 2011-12 bluff coverage) was incorporated into the Chippewa and Hawk Yellow Medicine models.
- **Representation of bluff collapse.** The RESPEC (2014) models removed the earlier models’ pseudo-random process of contribution from bluff collapse that was implemented via SPECIAL ACTIONS. The old approach, where the process of bluff collapse is simulated as an increase in the bed sediment that is available for transport in stream segments, was reincorporated in the updated models. Table 5-2 (*Bluff Erosion Contribution Rates to Available Stream Bed Sediment*) from Tetra Tech (2008) was used as a starting point along with information from the Le Sueur and Greater Blue Earth sediment mass balance studies (Gran et al., 2011; Bevis, 2015). The watershed-specific estimated total bluff loads were split by area-weighting the bluff contribution based on each individual sub-watershed bluff area for each of the watersheds and then that load was supplied as a constant replenishment to the bed via SPECIAL ACTIONS. This approach maintains the watershed-specific bluff contribution loads at the mouth of each model but proportionally modifies the amount of sediment load applied to a reach containing a bluff land use by the area of bluff contributing to the reach. In the Tetra Tech (2008) report, bluff loading was not represented in the Middle Minnesota and Lower Minnesota models and no specific information on bluff loading rates has been obtained. However, there is bluff land use area in those two models. To implement the SPECIAL ACTIONS in the Middle and Lower Minnesota models, the Le Sueur bluff contribution loads were used as a proxy at the recommendation of the MPCA project manager. First, the Le Sueur bluff loading rate was converted to a yield in tons/ac relative to the specified bluff acreage. Second, the converted Le Sueur rate was applied to the bluff area in the Middle, Lower, and Metro models to develop the bluff erosion contribution rates to available stream bed sediment.
- **Creation of PLTGEN outputs for models not having those outputs.** Most of the RESPEC (2014) models provided model output at instream monitoring locations by writing to PLTGEN’s. PLTGEN output was added to the Chippewa, Hawk-Yellow Medicine, Middle Minnesota, Lower Minnesota, and Metro Minnesota models. This allowed for a consistent set of tools to compare simulated and observed instream concentrations and load summaries.

4.2 UPLAND SEDIMENT SIMULATION

The RESPEC (2014) Minnesota River Basin HSPF models in most cases had upland sediment parameters similar to those calibrated in Tetra Tech (2008) and thus produce consistent loading rate estimates. This was not the case for the impervious land simulation, where the use of a high value of the washoff parameter (KEIM) resulting in extremely high loading rates from urban land, apparently accidentally set at ten times the previously calibrated value, resulted in urban impervious land generating about 1 ton per acre per year of solids and dominating total sediment load in some watersheds. Municipal Separate Storm Sewer System (MS4) monitoring results summarized by MPCA suggest that the sediment rate for urban developed land should, on average, be less than 0.1 ton/ac/yr.

The main parameters controlling upland sediment generation and transport to the stream are:

- KRER coefficient in the soil detachment equation for pervious land
- KSER coefficient in the detached sediment washoff equation for pervious land
- KEIM coefficient in the solids washoff equation for impervious land

The above parameters were the main PERLND and IMPLND parameters modified to bring consistency with the current constraining information and the simulated per acre sediment loading rates. There are other parameters that have a major influence specifically the exponential terms (JRER, JSER, and JEIM), although those were not modified from what RESPEC previously used because reasonable per acre sediment loading rates were obtained without modifying them. However, almost all sediment parameters were modified for Bluffs and Ravines. Since these land uses have small area and are large contributors of the overall sediment load in the stream, all of the parameters were set up so that the land areas have high loading rates.

Table 4 through Table 6 show the range of values used for each land use and each model for the three main parameters modified for the upland sediment simulation. KRER was calculated using the land use coverage and soils coverage and then area weighted to a value for each land use and weather station zone and was not further modified during calibration. KSER was the main parameter adjusted to control the sediment washoff and delivery. KEIM was the only parameter adjusted to control solids washoff and delivery. Table 7 provides the typical monthly erosion-related cover used for all models to provide some context to the calibrated values of KRER and KSER.

Table 4. KRER Values Used for Updated Models

Land Use	Redwood	Cottonwood	Watowan	Le Sueur	Blue Earth	Middle	Lower	Metro
Urban	0.241 - 0.287	0.233 - 0.27	0.233 - 0.266	0.237 - 0.278	0.239 - 0.289	0.228 - 0.268	0.229 - 0.271	0.207 - 0.281
Forest	0.24 - 0.281	0.234 - 0.273	0.211 - 0.253	0.209 - 0.287	0.24 - 0.292	0.165 - 0.269	0.2 - 0.274	0.177 - 0.261
Cropland - Conservation Till (HSG A,B)	0.243 - 0.277	0.233 - 0.27	0.232 - 0.265	0.225 - 0.272	0.217 - 0.284	0.23 - 0.251	0.217 - 0.256	0.04 - 0.305
Cropland - Conservation Till (HSG C,D)	0.314 - 0.363	0.312 - 0.362	0.127 - 0.331	0.106 - 0.286	0.15 - 0.336	0.192 - 0.339	0.219 - 0.357	0.02 - 0.313
Cropland - Conventional Till (HSG A,B)	0.243 - 0.277	0.233 - 0.27	0.232 - 0.265	0.225 - 0.272	0.217 - 0.284	0.23 - 0.251	0.217 - 0.256	0.04 - 0.305
Cropland - Conventional Till (HSG C,D)	0.314 - 0.363	0.312 - 0.362	0.127 - 0.331	0.106 - 0.286	0.15 - 0.336	0.192 - 0.339	0.219 - 0.357	0.02 - 0.313
Cropland - Manure Application (conv A,B)	0.243 - 0.277	0.233 - 0.27	0.232 - 0.265	0.225 - 0.272	0.217 - 0.284	0.23 - 0.251	0.217 - 0.256	0.04 - 0.305
Grassland	0.249 - 0.28	0.212 - 0.277	0.217 - 0.287	0.209 - 0.264	0.214 - 0.274	0.204 - 0.265	0.21 - 0.275	0.171 - 0.276
Pasture	0.211 - 0.288	0.22 - 0.284	0.211 - 0.261	0.192 - 0.282	0.227 - 0.279	0.208 - 0.27	0.217 - 0.268	0.113 - 0.274
Wetland	0.254 - 0.313	0.227 - 0.278	0.155 - 0.244	0.042 - 0.249	0.104 - 0.276	0.066 - 0.311	0.072 - 0.264	0.049 - 0.236
Feedlot	0.25	0.25	0.25	0.23 - 0.27	0.246	0.245	0.244	0.244
Bluff	0.24	0.24	0.24	0.23 - 0.27	0.243	0.243	0.174	0.174
Ravine	0.28	0.28	0.28	0.23	0.278	0.278	0.278	0.278

Notes: KRER estimates are derived from soil survey data on the Universal Soil Loss Equation erodibility (K) factor. Values for Chippewa and Hawk Yellow Medicine not presented here due to different PERLND configurations. Refer to their UCI files for their parameterization

Table 5. KSER Values Used for Updated Models

Land Use	Redwood	Cottonwood	Watowan	Le Sueur	Blue Earth	Middle	Lower	Metro
Urban	0.08	0.08	0.07	0.08	0.08	0.08	0.08	0.08
Forest	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Cropland - Conservation Till (HSG A,B)	0.2	0.3	0.08	0.2 & 0.05	0.25	0.3	0.15	0.15
Cropland - Conservation Till (HSG C,D)	0.15	0.3	0.08	0.2 & 0.05	0.1	0.3	0.15	0.15
Cropland - Conventional Till (HSG A,B)	0.25	0.4	0.11	0.3 & 0.1	0.3	0.4	0.2	0.2
Cropland - Conventional Till (HSG C,D)	0.2	0.4	0.11	0.3 & 0.1	0.15	0.4	0.2	0.2
Cropland - Manure Application (conv A,B)	0.25	0.4	0.09	0.3 & 0.1	0.3	0.4	0.2	0.2
Grassland	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04
Pasture	0.07	0.07	0.07	0.07	0.07	0.07	0.07	0.07
Wetland	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Feedlot	0.14	0.14	0.14	0.14	0.14	0.14	0.14	0.14
Bluff	0.75	0.75	0.75	0.75	0.75	0.75	0.75	0.75
Ravine	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5

Note: Values for Chippewa and Hawk Yellow Medicine not presented here due to different PERLND configurations. Refer to their UCI files for their parameterization

Table 6. KEIM Values Used for Updated Models

Land Use	Chippewa	HYM	Redwood	Cottonwood	Watonwan	Le Sueur	Blue Earth	Middle	Lower	Metro
Urban Impervious	0.03	0.02	0.015	0.015	0.015	0.015	0.015	0.015	0.015	0.015

Table 7. Typical Monthly Cover Values Used for Updated Models

Land Use	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
Urban	0.85	0.85	0.85	0.88	0.88	0.88	0.88	0.88	0.88	0.86	0.85	0.85
Forest	0.85	0.85	0.85	0.9	0.95	0.95	0.95	0.95	0.95	0.95	0.85	0.85
Cropland - Conservation Till A,B	0.2	0.2	0.2	0.35	0.35	0.3	0.4	0.85	0.85	0.7	0.55	0.35
Cropland - Conservation Till C,D	0.2	0.2	0.2	0.35	0.35	0.3	0.4	0.85	0.85	0.7	0.55	0.35
Cropland - Conventional Till A,B	0.05	0.05	0.05	0.15	0.15	0.2	0.4	0.85	0.85	0.6	0.4	0.15
Cropland - Conventional Till C,D	0.05	0.05	0.05	0.15	0.15	0.2	0.4	0.85	0.85	0.6	0.4	0.15
Cropland - Manure Application (conv A,B)	0.05	0.05	0.05	0.15	0.15	0.2	0.4	0.85	0.85	0.6	0.4	0.15
Grassland	0.75	0.75	0.75	0.8	0.85	0.9	0.9	0.9	0.9	0.9	0.85	0.8
Pasture	0.75	0.75	0.75	0.8	0.85	0.9	0.9	0.9	0.9	0.9	0.85	0.8
Wetland	0.9	0.9	0.9	0.92	0.97	0.97	0.97	0.97	0.97	0.97	0.92	0.9
Feedlot	0.1	0.1	0.1	0.03	0.03	0.1	0.6	0.85	0.85	0.7	0.2	0.15
Bluff	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
Ravine	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2

4.3 INSTREAM SEDIMENT SIMULATION

As previously discussed the 2014 Minnesota River Basin HSPF models had sediment source apportionment results that were inconsistent with the current constraining information. For example, the 2014 models of the Blue Earth and Le Sueur watersheds attributed over 70 percent of the total sediment load to upland sources compared to less than 30 percent based on radiometric analysis (see Table 1 above). This fact, along with the updated hydrology calibration, required adjustment of the instream simulation of sediment.

There are two types and three classes of sediment simulated in HSPF non-cohesive (sand) and cohesive (silt and clay). The three sediment classes are simulated independently of one another in the stream. Load delivered from the land surface is simulated as total sediment and partitioned into sand, silt, and clay fractions at the stream edge. As previously stated, the upland to instream partitioning of sediment was not modified from what was provided by RESPEC.

In HSPF, sand can be simulated by one of three approaches: 1) Toffaletti equation, 2) Colby method, or 3) power function of velocity. For the Minnesota River Basin HSPF the selected sand method is 3) power function of velocity. This was the method that RESPEC used and was unmodified for the recalibration.

The main parameters controlling the cohesive instream sediment simulation are listed below. These values are contained in the SILT-CLAY-PM block of the UCI and the data block is repeated twice. The first set in the UCI pertains to silt and the second set in the UCI pertains to clay.

- D effective diameter of the particles
- W particle fall velocity in still water
- RHO particle density
- TAUCD critical bed shear stress for deposition
- TAUCS critical bed shear stress for scour
- M erodibility coefficient of the sediment

D, W, and RHO were parameterized with values in range with those outlined in US EPA (2006) and following the approach laid out for MPCA One Water projects by AQUA TERRA (2012). Values for TAUCD, TAUCS, and M were calibrated by first outputting the hourly TAU (bed shear stress) for the simulation period. Second, the percentile ranges of TAU for each simulated reach were tabulated. Third, initial values TAUCD, TAUCS, were input by selecting a percentile used in previous model calibrations and finding each reaches TAU value corresponding to that percentile. Lastly, after the upland simulation was completed, TAUCD, TAUCS, and M were adjusted through an iterative process until an acceptable match was achieved between observed instream concentrations and loads and simulated concentrations and loads, and sediment source apportionment (percent and estimated load where available) were consistent with the current constraining information.

As noted above, the representation of sediment load associated with mass wasting of bluffs was reverted to the prior approach (Tetra Tech, 2008) where the process of bluff collapse is simulated as an increase in the bed sediment that is available for transport in stream segments. Table 8 shows the bluff erosion contribution rates to available stream bed sediment as a total rate above each models pour point or end point. The watershed-specific bluff contribution loads were split among identified bluff land uses based on the bluff area by sub-basin. That load was then supplied as a constant replenishment rate to the bed for the reaches containing upland bluff area via SPECIAL ACTIONS. The added sediment was then mobilized when higher flows occur (i.e., TAU values greater than TAUCS). The bluff reaches had higher values of the erodibility coefficient M specified to maintain proper stream bed balance.

Table 8. Total Sediment Loading to Stream Bed Storage from Bluff Mass Wasting Processes

Watershed	Bluff Contribution (tons/hr)
Blue Earth River	28
Chippewa River	0.1
Cottonwood River	2.1
Hawk Creek	0.97
Le Sueur River	11.2
Lower Minnesota River	0.05
Middle Minnesota River	0.13
Redwood River	1.6
Watowwan River	2.1
Yellow Medicine River	1.5

In the initial calibration the simulated TSS concentrations were generally lower than those observed at base flow conditions. To improve the baseflow simulation, a clay load associated with groundwater was supplied as a surrogate for a combination of fine material in actual groundwater discharges, and activity of fish, animals, and humans in the streams. The added clay load equated to 5 mg/L for all models except Hawk-Yellow Medicine, and Chippewa, which were assigned 1 mg/L.

Table 9 provides the range of values used in the SILT- and CLAY-PM blocks. Values for D, W, RHO, and M in this table are the actual values input into the UCI, while entries for TAUCD and TAUCS provide the percentile range of simulated TAU. Since each reach has its own model derived value for TAU providing the percentile range of TAU provides much more insight into the parameterization of TAUCD and TAUCS. For each basin, parameters other than the critical shear stresses were specified separately for stream, lake, and bluff-area reaches but otherwise held constant or varied only slightly (in the case of M) across the basin. The erodibility and critical shear stress parameters were varied within relatively constrained ranges to improve the calibration fit.

Table 9. SILT-CLAY-PM Block Values Used for Updated Models

Constituent	RCHRES Type	Parameter	Chippewa	HYM	Redwood	Cottonwood	Watonwan	Le Sueur	Blue Earth	Middle	Lower	Metro
Silt	Stream	D	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006
		W	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039
		RHO	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3
		TAUCD*	1-50	4-7	1-18	4-6	1-10	4-10	1-13	1-18	1-13	1-16
		TAUCS*	80-85	80-81	75-76	75-76	66-78	65-92	65-80	73-91	74-78	68-80
		M	0.004	0.004	0.015	0.015-0.025	0.01	0.006-0.03	0.025	0.01	0.02	0.02
	Bluff	D	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006
		W	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039
		RHO	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3
		TAUCD*	6	5-6	6	5-6	5-6	4-11	5-6	5-6	5-6	5-6
		TAUCS*	80-81	81	76	75-76	66-78	65-92	65-75	85-86	75-76	75-76
		M	0.01	0.07	0.1	0.05-0.1	0.03-0.05	0.008-0.07	0.1	0.1	0.1	0.1
	Lake	D	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006	0.0006
		W	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039	0.0039
		RHO	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3
		TAUCD*	97-99.9	97-98	97-99.9	97-99.9	98-99	97-99	95-99	97-99	97-99	97-99
		TAUCS*	99-99.9	99	99-99.9	97-99.9	99-99.9	99-99.9	96-99.9	99-99.9	99-99.9	99-99.9
		M	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005
Clay	Stream	D	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
		W	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001
		RHO	2	2	2	2	2	2	2	2	2	2
		TAUCD*	1-47	3-4	1-18	3-4	1-10	1-9	1-13	1-16	1-12	1-13
		TAUCS*	75-85	75-76	70-71	70-72	60-73	60-87	65-80	60-89	68-75	64-73
		M	0.004	0.004	0.015	0.015-0.025	0.01	0.006-0.03	0.025	0.01	0.02	0.02
	Bluff	D	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
		W	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001
		RHO	2	2	2	2	2	2	2	2	2	2
		TAUCD*	3-4	3-4	3-4	3-4	3-4	1-5	3-4	3-4	3-4	3-4
		TAUCS*	76	75-76	70	70-71	60-73	60-87	60-70	80-81	70-71	70-71
		M	0.01	0.07	0.1	0.05-0.1	0.03-0.05	0.008-0.07	0.1	0.1	0.1	0.1
	Lake	D	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
		W	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001
		RHO	2	2	2	2	2	2	2	2	2	2
		TAUCD*	97-99.9	97-98	97-99.9	97-99.9	98-99	97-99	95-99	97-99	97-99	97-99
		TAUCS*	99-99.9	99	99-99.9	97-99.9	99-99.9	99-99.9	96-99.9	99-99.9	99-99.9	99-99.9
		M	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005

* Value in table provided as a percentile of the hourly simulated TAU range

4.4 SEDIMENT SOURCE APPORTIONMENT

Sediment source data is primarily based on interpretation of radiometric data (^{210}Pb and ^{137}Cs) that provides an estimate of the fraction of sediment that has recently been in contact with the atmosphere (Schottler et al., 2010). To a first approximation, the percentage of “new” sediment is interpreted as the fraction of stream sediment load that derives from upland surface erosion, as opposed to load from channel erosion, ravine erosion, or bluffs. That interpretation is not exact, however, as each source contains some mixture of older, buried soil and exposed surface sediment. Another problem for interpretation is that upland sediment load may be temporarily stored and then re-scoured from the stream bed, so model output of channel scour does not necessarily represent only “old” sediment. A unique set of upland loading rates, bed erosion rates, and downstream sediment transport measures is thus not readily interpretable from the model output and the ratio of old to new sediment is not directly extractable from the model because individual sediment particles are not tracked as they move in and out of bed storage.

This issue was explored in some detail in Tetra Tech (2008), from which the following text is summarized:

Consider a case in which there is an external (upland) sediment load of X and a bank and bluff erosion load of B . The processes can be conceptually represented by a simple box model (Figure 1).

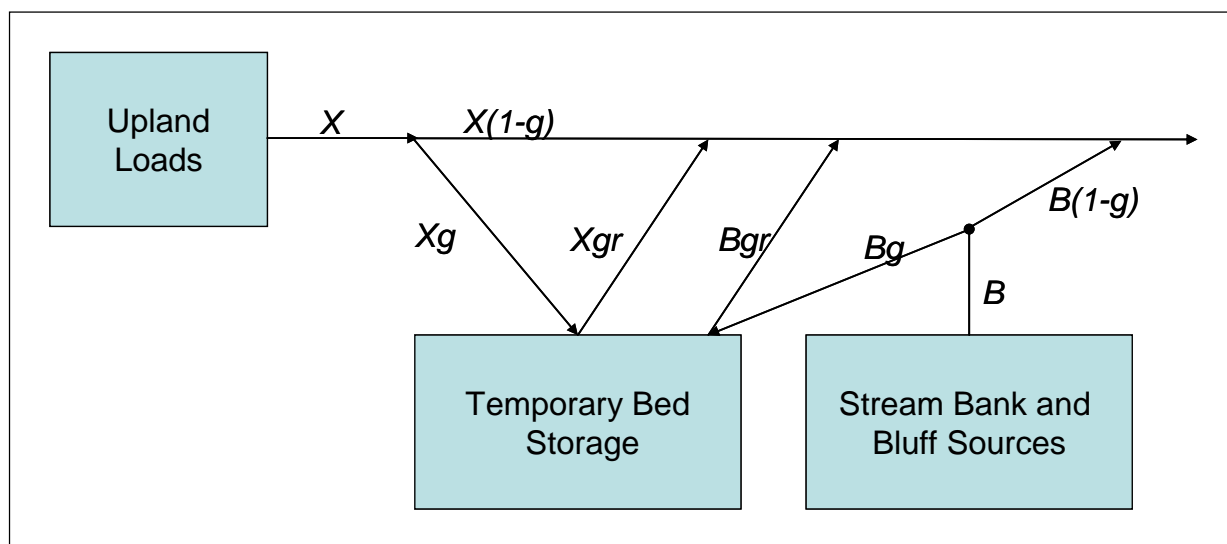


Figure 1. Conceptual Representation of Stream Sediment Processing

For an external sediment load X , a fraction g goes into temporary bed or floodplain storage. A fraction of this (r) is in turn resuspended and transported downstream as Xgr . Similarly, erosion of established stream banks and bluffs yields a total load B . This is assumed to be subject to the same physical processes as the upland load, X : A fraction g goes into temporary storage, of which a further fraction r is transported downstream. (The factor r may be thought of as a recycle rate. The total sediment load transported downstream, Y , is then:

$$Y = (X + B)(1 - g + gr).$$

The model output provides information on both gross bed scour (GS , resuspension flux only) and net bed scour (NS , balance of scour and deposition). Two additional equations can be written for GS and NS based on the simple box model:

$$GS = Xgr + B + Bgr$$

$$NS = X(gr - g) + B(1 + gr - g).$$

Given X, this appears to yield three equations in three unknowns. However, the system of equations is indeterminate, as the output, Y, is simply equal to the net scour (NS) + X. Therefore, there is not a unique solution unless additional constraints are imposed regarding the recycle rate, r.

Tetra Tech (2008) explored this issue further and concluded that the net effect of scour plus deposition was that the true upland-derived fraction at the outlet was likely to be about 95% of the simulated upland load divided by the downstream output load. Conducting the analysis is, however, difficult because the gross scour and net scour components need to be separated based on analysis of hourly simulation results and the results, in the end, remain uncertain because a value for r must be assumed.

To address these issues, a new approximate methodology was developed to generate simulated source apportionments in an efficient manner. For this purpose, Excel™ “Sediment Sources” workbooks were created with live equations that tabulate the simulated sediment source apportionment. The workbooks are provided for further investigation. The following discusses how to update the workbooks and the calculations that are being performed in the workbooks.

To use/update the workbook for any of the watershed models in the Minnesota River Basin HSPF the user must first generate yearly reach.HBN and wshd.HBN files for sediment. To do this the user must specify a flag of 5 for SED, SLD, and SED in the BINARY-INFO blocks for PERLND, IMPLND, and RCHRES respectively and then run the model. The needed HBN files can be found in the PLTGEN folder for the model that you are working with. Data for certain constituents contained in the reach.HBN and wshd.HBN are used to update the reachHBN and wshdHBN tabs in the EXCEL workbook. To access the data the user must open the reach.HBN and wshd.HBN files with the SARA Timeseries Utility. The reach.HBN file is populated with ISED-TOT (inflow of total sediment to each RCHRES by year), ROSED-TOT (outflow of total sediment from each RCHRES by year), and RSED-BED-TOT (average bed storage mass of sediment for each RCHRES by year). The wshd.HBN is populated with WSSD (washoff of detached sediment for each PERLND by year), SCRSD (scour of matrix soil for each PERLND by year), and SOSLD (washoff of solids for surface for each IMPLND per year). The user must select each constituent individually and also be sure to select the location attribute otherwise the workbook will not function properly. Copy/Paste the created list from SARA to the appropriate location in the attribution workbook and the pertinent information should be updated.

The All_Reach_Summary worksheet performs a series of tabulations that calculate the necessary information to determine the source apportionment. The workbook has comments associate with cells A4:A21 to provide the user with information about what is actually being calculated. The calculations use the information in the reachHBN and wshdHBN along with information in the SchemPLS_All, SchemPLS_RAV, SchemPLS_BLF, SchemPLS_OTH, SchemILS, and SchemRch tabs. All of the tabs listed in this paragraph contain live equations so please be very cautious about inserting, deleting, or modifying anything in all of the listed tabs.

The results of the All_Reach_Summary are then used to populate the Source_Attribution tab. For each workbook the Source_Attribution tab varies in the number of locations where source attributions are currently calculated, and the number of upstream reaches that are used to develop the source attribution. Basically, the source attribution is calculated by using the full 18 year simulation for all reaches upstream and including the reach pour point of interest. For each reach the sediment load of WSSD and SCOUR for Ravine, Bluff, and all other PERLND's are found in the All_Reach_Summary tab. Also found for each reach is the amount of sediment coming from IMPLND's as well as the deposition (positive value) or scour (negative value) from the instream simulation. Upland, Ravine, Bluff, and Stream mass are then approximated using the following calculations:

- Upland = Sum of WSSD Other, SCRSD Other, and SOSLD

- Ravine = Sum of WSSD Ravine and SCRSD Ravine
- Bluff = Sum of WSSD Bluff , SCRSD Bluff, and (-1* Deposition/Scour from Bluff Reaches)
- Stream = Sum of -1* Deposition/Scour from Non-Bluff Reaches (as scour is negative in the output).

Sediment source apportionments from upstream models are copy/pasted into the downstream model workbooks. For instance, for the Blue Earth at the mouth the workbook is theoretically only calculating the input from the Blue Earth model itself (the local drainage); however, when the Watonwan and Le Sueur source apportionment results are incorporated you can calculate the source apportionment at the mouth for the entire drainage basin. Additionally, the Chippewa model accounts for the Watson Sag Diversion to the Lac Qui Parle. The source apportionment calculations do not explicitly account for the sediment lost due to the diversion. Instead the apportionment is calculated on a percentage basis as though the diversion did not exist and then the calculated source fractions are applied to the Chippewa ROSED value at the mouth to calculate the source apportionment going into the Hawk Yellow Medicine model. That same source apportionment is applied to the Lac qui Parle input to the Hawk-Yellow Medicine model as simulation model results are not yet available for Lac qui Parle and its upstream watershed.

Based on comparison to a detailed (hourly) analysis of the Le Sueur River basin, this method, which includes only annual totals of scour and/or deposition, provides a close approximation to a more complex analysis using hourly data. However, as noted above, complete attribution of surface sediment sources would require correction for net storage/resuspension within the stream network, which would be expected to result in a small reduction in the estimated surface-derived fraction.

5 Results

5.1 UPLAND UNIT AREA LOADS

As described above, some of the existing (2014) models provided unrealistic results for the amount of sediment being generated from upland sources, especially from developed land. Table 10 displays the simulated upland sediment loading rates by basin and land use for the revised model. HSPF simulates urban pervious and impervious lands separately, so a combination result for 25 percent impervious (and 75 percent developed pervious) land is shown for comparison with MS4 loading rates. These results were calculated by taking the wshd.HBN outputs of WSSD, SCRSD, and SOSLD (discussed in section 4.4) and 1) calculating the average annual sediment load for each PERLND/IMPLND (combination of weather station zone and land use) and 2) averaging the PERLND/IMPLND average annual sediment load across all weather station zones to find the average annual sediment load for each land use. Note, the loads are not area weighted but are simply a tabulation of unit area load as provided by the wshd.HBN output.

Excel™ workbooks for each watershed model were created and are provided as a supplement to this memorandum to allow for further investigation.

Le Sueur, Blue Earth, and Watonwan watersheds had much more constraining information for the apportionment of sediment mass and percent contribution due to the Le Sueur sediment budget and Greater Blue Earth sediment budget efforts (Gran et al., 2011; Bevis, 2015). That information along with results of Schottler et al. (2010) as further updated in presentations by the investigators to MPCA (personal communication from Chuck Regan, MPCA) was used to constrain the upland sediment source apportionment.

A goal for the upland sediment simulation was to supply largely homogeneous parameterization throughout the entire suite of Minnesota River Basin HSPF. Simulated upland unit area loading rates are in general roughly consistent between basins, but differ according to the local meteorological forcing, soil characteristics, and hydrologic simulation. Some deviations between basins are intentional: Specifically, for the Watonwan basin, the unit area loadings were reduced to obtain a better match between simulated and observed upland source mass as provided in the Greater Blue Earth sediment budget (Bevis, 2015). Additionally, for the Blue Earth the unit area loading was increased to get a better match between simulated upland source mass and observed upland source mass provided in the Greater Blue Earth sediment budget. It is also worth noting that the Hawk-Yellow Medicine model shows less distinction between HSG A,B and C,D soils for agriculture. This basin contains primarily B and B/D (B when drained) soils so the difference is not of great practical importance for total load simulation. The similarity between loading rates for different soil groups appears to be due to the hydrology set up of the model, which specifies only a small difference in infiltration rates between the different HSG classes.

Table 10. Revised Annual Average Unit Area Sediment Loads, 1995-2012 pound/acre/year

Land Use	Chippewa	HawkYM	Redwood	Cottonwood	Watowan	Le Sueur	Blue Earth	Middle	Lower	Metro
Urban Pervious	31.3	129.6	72.1	86.1	89.6	195.7	147.2	46.1	38.4	70.5
Urban Impervious	325.7	285.3	292.9	304.9	338.1	364.4	361.0	318.5	318.9	349.9
Urban Combo (75% Pervious 25% Impervious)	104.9	168.5	127.3	140.8	151.7	238.9	200.7	114.2	108.5	140.4
Forest	0.6	7.5	6.0	6.8	14.2	13.6	16.5	4.4	3.7	7.0
Cropland - Conservation Till (HSG A,B)	61.3	47.5	36.8	55.6	31.0	85.3	77.4	107.0	45.3	81.4
Cropland - Conservation Till (HSG C,D)	126.4	52.5	247.1	375.8	198.1	350.0	266.1	244.3	283.4	347.7
Cropland - Conventional Till (HSG A,B)	63.5	71.2	51.0	79.2	48.2	138.9	104.4	150.8	67.4	115.5
Cropland - Conventional Till (HSG C,D)	160.3	77.4	312.6	497.7	260.5	512.1	359.0	301.1	355.2	426.9
Cropland - Manure Application (conv A,B)	148.3	77.1	51.0	79.1	48.2	138.4	104.4	150.3	67.4	114.5
Grassland	1.6	13.7	8.7	8.7	22.3	26.1	25.7	3.4	1.1	2.3
Pasture	28.2	NA	16.5	17.2	36.4	47.5	39.4	6.1	2.3	4.8
Wetland	0.6	0.0	0.5	0.3	2.9	1.5	1.2	0.6	0.5	0.9
Feedlot	NA	NA	233.5	294.8	367.5	570.8	563.7	167.7	129.7	239.4
Bluff	271	25	2,276	3,124	5,696	6,262	10,550	1,202	516	1,053
Ravine	NA	NA	7,827	16,369	95,117	31,237	393,722	8,996	1,097	2,198

Note: For Chippewa, results shown for Forest, Grass, and Pasture are for D soils. For Hawk-Yellow Medicine, results shown for Forest, Grass, and Pasture are for D soils on low slopes. Feedlot and Ravine land uses are not specified separately in the Chippewa and Hawk-Yellow Medicine models.

5.2 INSTREAM CALIBRATION AND VALIDATION

As previously discussed, separate calibration and validation tests were conducted based on a spatial and temporal distribution of stations (Table 3). These are summarized in electronic spreadsheets provided as a supplement to this memorandum. The statistical results below are reported according to the two groups of gages (calibration and validation) in the next two sub-sections. A representative station was selected for each group and graphical results are provided for those stations for example purposes. Comprehensive graphics for each gage are provided in the electronic files.

The summary statistics include concentration average error, concentration median error, load average error and load median error. All of the statistics are performed on paired comparisons of simulated daily average and observed instream instantaneous grab measurements. Also provided is the number of paired comparisons for each station.

5.2.1 Calibration Stations

Table 11 (in five parts) shows the statistical results for the calibration gages. The calibration strategy focused foremost on sediment source attribution and used harmonized parameter estimates instead of over-fitting individual gages, resulting in some relatively large errors, especially at some of the stations where there are limited data for accurate hydrologic calibration. The quality of fit for suspended sediment is generally in the good to very good range for concentration and load median errors. The quality of fit ranges from very good to poor for concentration and load average errors. Average errors are more susceptible to large deviations because they can be heavily influenced by extreme events and slight shifts in timing. Additionally, the stations that show large differences in the average error have a much more favorable comparison when looking at the graphical comparisons. It is advised to look at both the statistical comparison and graphical comparison when assessing the overall model fit to instream monitoring data.

Graphical examples of the calibration for Le Sueur River at MN-66 1.5 miles NE of Rapidan are provided in Figure 2 through Figure 6. Results for all other calibration gages are contained in the electronic files.

Table 11. Summary Statistics for Calibration Stations

Site	Chippewa R at 140th St, 7 mi N of Cyrus	Chippewa R at CSAH-22, 1 mi E Of Clontarf	Shakopee Ck, at Unn Twtnshp Rd, 1 mi W MN-29	Chippewa R, at MN-40, 5.5 mi E of Milan	Beaver Ck at CSAH-2 2.5 mi NE of North Redwood	Hawk Ck at CR 52 Br, 6.5 mi SE off Granite Falls	Hawk Ck, at MN-23, 2.2 mi SW of Maynard
STORET Code	S002-190	S002-193	S002-201	S002-203	S000-666	S002-012	S002-148
Count	243	322	314	367	374	408	375
Conc Ave Error	68.7%	-129.9%	-33.9%	-141.7%	-428.6%	-76.6%	-3.89074
Conc Median Error	1.6%	-26.3%	-52.5%	-26.9%	20.0%	14.1%	-1.0%
Load Ave Error	340.3%	39.1%	-62.1%	-23.3%	3.8%	62.0%	44.6%
Load Median Error	5.9%	-14.4%	-33.9%	-10.2%	0.2%	0.5%	-0.4%

(Table 11. Continued)

Site	Yellow Med R, 1 1/3 mi N CSAH-18	MN R 500 Ft S CSAH-13 near USGS Gage	Minnesota R, Ethanol Facility WS Intake*	Redwood R at CSAH-15 in Russell	Redwood R at CSAH-17, 3 Miles SW of Redwood Falls	Cottonwood R near MN-68 In New Ulm	Cottonwood R at CSAH 8 Br, 0.4 mi N Leavenworth
STORET Code	S002-316	S004-649	S007-748	S000-696	S001-679	S001-918	S001-920
Count	-7.7%	-59.8%	61.1%	47.1%	-21.0%	-37.8%	-18.7%
Conc Ave Error	7.7%	22.7%	8.7%	3.1%	-6.9%	0.2%	-1.6%
Conc Median Error	136.5%	-2.3%	-27.5%	-35.3%	76.2%	-3.2%	62.8%
Load Ave Error	0.4%	5.2%	1.7%	0.1%	-1.5%	0.0%	-0.1%
Load Median Error	-7.7%	-59.8%	61.1%	47.1%	-21.0%	-37.8%	-18.7%

(Table 11. Continued)

Site	Cottonwood R at US-14 Brg, 1 mi NE Lamberton	Watowan R Br on CSH-13, 1 mi W of Garden City	Le Sueur R Mn-66 1.5 mi NE of Rapidan	Maple R At CSAH 35 5.2 mi S of Mankato	Cobb R at CSAH-16, 4.4 mi NE of Good Thunder	Le Sueur R at CSAH-8, 5.1 mi SSE of Mankato	Blue Earth R 150 Ft dnst of Rapidan Dam
STORET Code	S002-247	S000-163	S000-340	S002-427	S003-446	S003-860	S001-231
Count	210	502	251	378	210	205	240
Conc Ave Error	17.5%	-423.8%	39.2%	14.6%	-162.7%	164.7%	-18.9%
Conc Median Error	5.7%	-13.5%	11.5%	-0.2%	51.0%	2.9%	4.9%
Load Ave Error	123.3%	15.6%	12.2%	19.0%	161.7%	-25.1%	-4.3%
Load Median Error	0.1%	-1.3%	0.6%	0.1%	15.3%	0.0%	0.7%

(Table 11. Continued)

Site	Elm Creek at 290th Ave - 4.5 mi NE of Granada	Minnesota River at Mankato	Minnesota R Bridge on US-71 and MN-19 at Morton	Minnesota R at CSAH 42 at Judson	Sevenmile Ck In Sevenmile Ck Cty Pk	Minnesota R at MN-99 in St. Peter	High Island Cr., CSAH-6, Henderson
STORET Code	213	45	165	199	261	239	297
Count	213	45	165	199	261	239	297
Conc Ave Error	-31.7%	77.6%	-43.1%	-58.8%	-710.8%	-39.3%	16.6%
Conc Median Error	-3.5%	9.6%	-1.5%	5.7%	2.5%	6.4%	1.3%
Load Ave Error	126.7%	34.7%	92.3%	66.8%	-43.5%	42.6%	-55.6%
Load Median Error	0.5%	0.6%	-0.5%	0.3%	0.0%	1.8%	-0.1%

(Table 11. Continued)

Site	Rush River, SH-93 by Henderson	Bevens Cr., CSAH-41 by East Union	W Chaska Ck, 250' W of Cty Rd 10
STORET Code	S000-822	S000-825	S002-548
Count	266	135	129
Conc Ave Error	1.1%	27.1%	-4.4%
Conc Median Error	-7.2%	-14.0%	3.0%
Load Ave Error	-81.5%	-34.4%	-56.0%
Load Median Error	-2.3%	-3.5%	0.2%

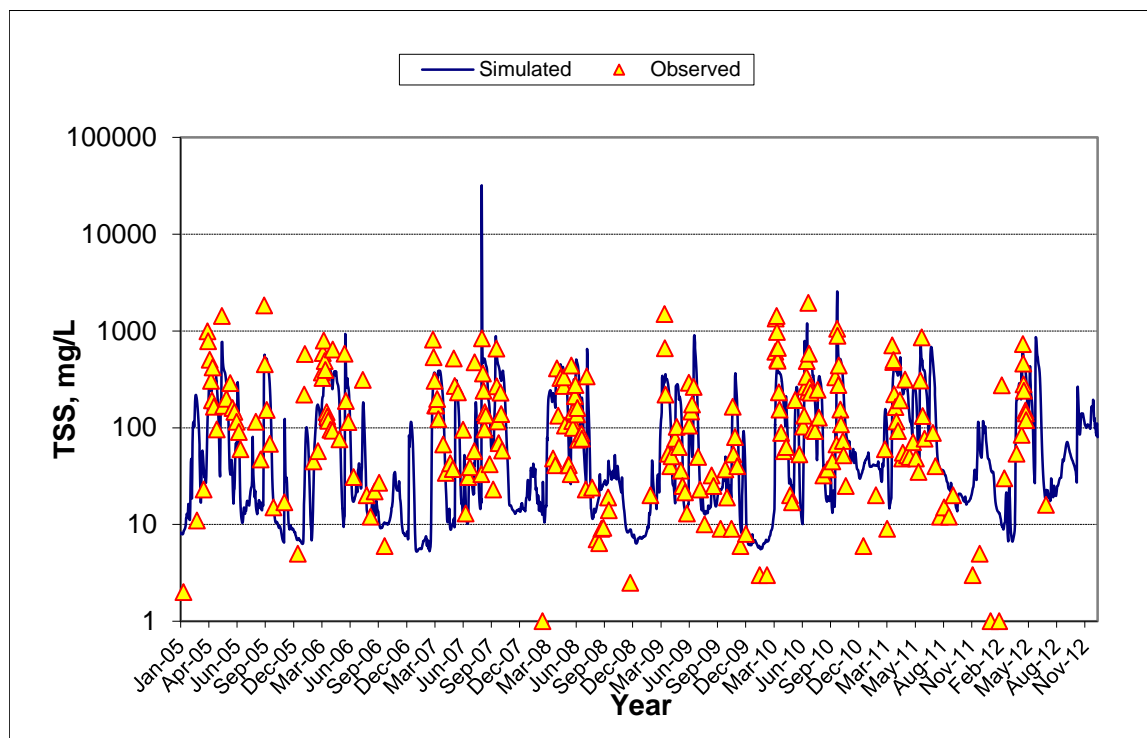


Figure 2. Timeseries Plot of Simulated and Observed TSS Concentration for Le Sueur River at MN-66 1.5 miles NE of Rapidan for 2005-2012

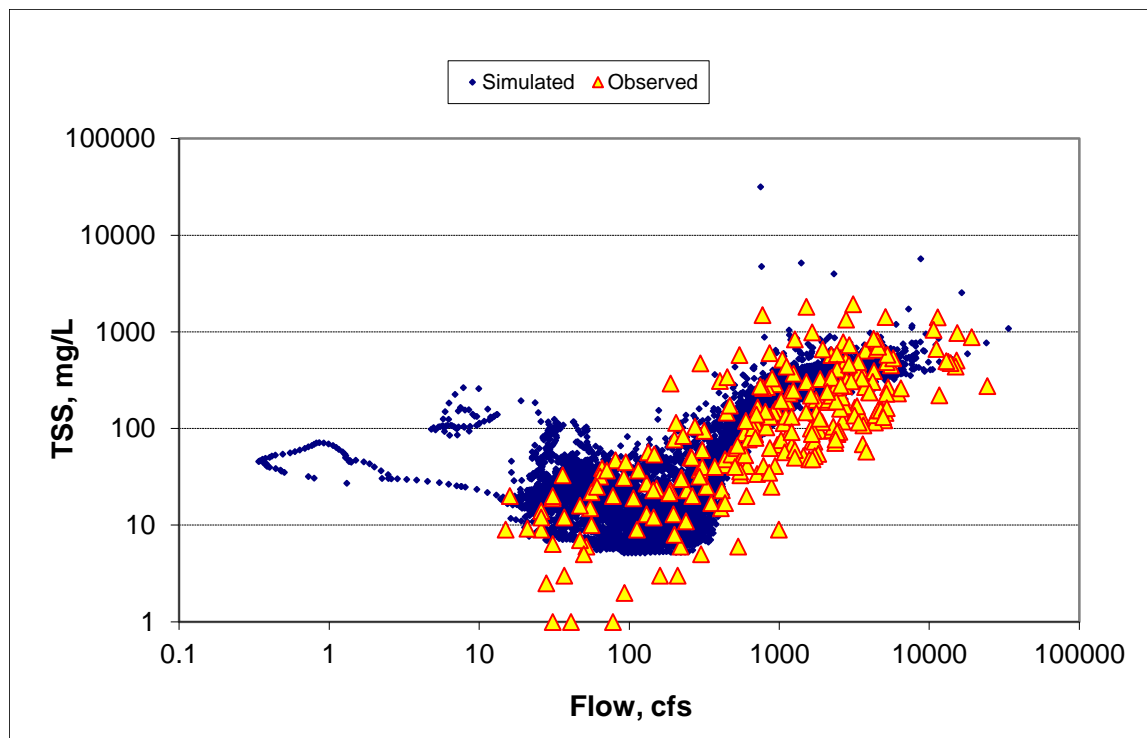


Figure 3. Concentration vs Flow Plot of Simulated and Observed TSS Concentration for Le Sueur River at MN-66 1.5 miles NE of Rapidan for 2005-2012

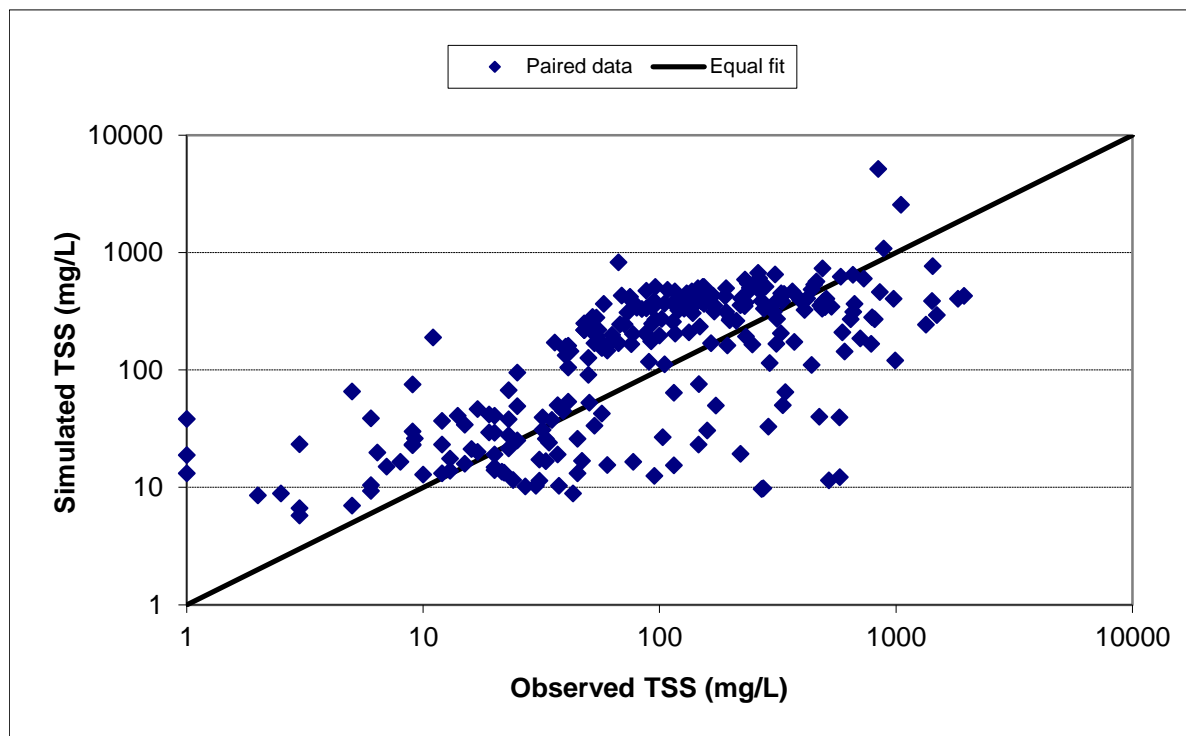


Figure 4. Simulated and Observed TSS Concentration Paired Regression Plot for Le Sueur River at MN-66 1.5 miles NE of Rapidan for 2005-2012

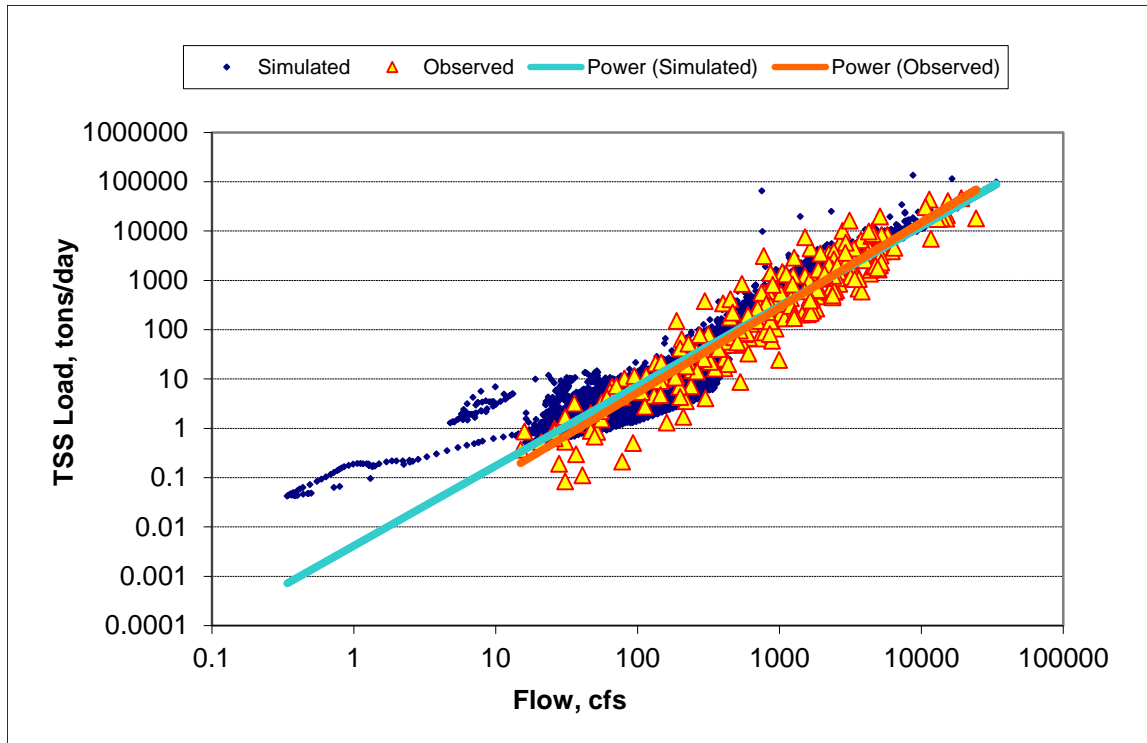


Figure 5. Load vs Flow Plot of Simulated and Observed TSS Load for Le Sueur River at MN-66 1.5 miles NE of Rapidan for 2005-2012

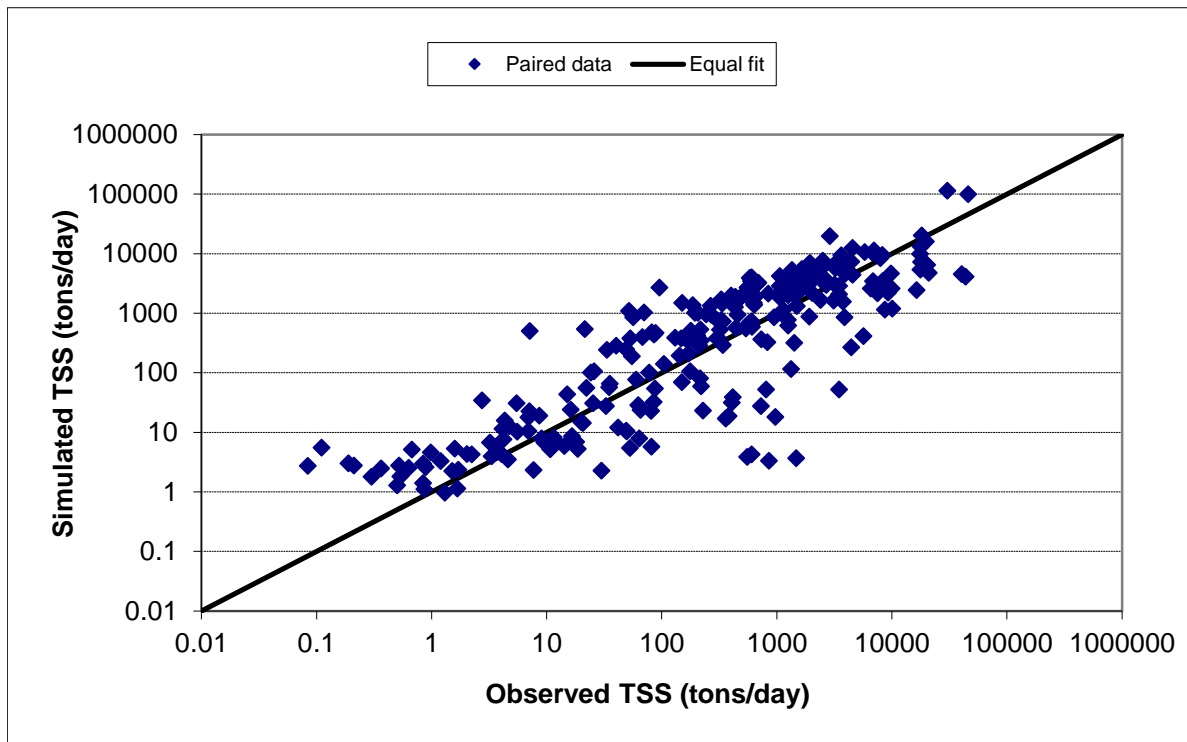


Figure 6. Simulated and Observed TSS Load Paired Regression Plot for Le Sueur River at MN-66 1.5 miles NE of Rapidan for 2005-2012

5.2.2 Validation Stations

The parameters developed during calibration were applied without modification to the validation stations. Table 12 (in five parts) shows the statistical results for the validation gages. Similar to the calibration stations the quality of fit is generally in the good to very good range for concentration and load median errors but from very good to poor for concentration and load average errors. There are a few validation stations that have poor fit for both averages and medians (e.g., Shakopee Creek S002-209 and High Island Creek S001-891). Model performance could likely be improved at individual stations; however, the parameters were not modified due to the desire to maintain spatial homogeneity across all models in the upland parameters and maintain reach homogeneity within each individual model.

Graphical examples of the calibration for Little Cottonwood River at Apple Road are provided in Figure 7 through Figure 11. While fit is reasonable at this station, the model appears to under-estimate suspended sediment concentrations observed at high flows. Results for all other validation gages are contained in the electronic files.

Table 12. Summary Statistics for Validation Stations

Site	Dry Weather Creek, at 85th Ave NW, 4 mi NE of Watson	Shakopee Ck, S Andrew Rd at Lk Andrew Otl	Little Chippewa R at Mn-28, 4 mi W of Starbuck	Chippewa R, EB, at 15th Ave NE, 2.5 mi N of Benson	W Fk Beaver Ck at CSAH-4 6.5 mi S of Olivia	Sacred Heart Ck at CSAH-15 Br, 5 mi NW of Delhi	Palmer Ck at 15th Ave SE, 2 mi NW of Granite Falls
STORET Code	S002-204	S002-209	S004-705	S005-364	S000-405	S001-341	S002-136
Count	322	116	64	307	234	131	126
Conc Ave Error	17.8%	715.2%	-96.4%	-4.0%	-189.5%	-321.7%	107.9%
Conc Median Error	-2.5%	258.1%	37.9%	1.0%	-14.9%	19.5%	6.9%
Load Ave Error	-63.0%	474.3%	-21.0%	25.2%	418.1%	-52.1%	-25.5%
Load Median Error	0.0%	182.3%	8.7%	0.3%	0.5%	0.4%	0.4%

(Table 12. Continued)

Site	Hawk Ck, at CR-116, 1.25 mi S of MN-40	Chetomba Ck, 5 mi SE of Maynard	S Br Yellow Medicine R on CSAH-26	CD-119 at CSAG-15, 5.6 mi S of Sacred Heart	Timms Ck at CSAG-15, 2.8 mi NNE of Delhi	Clear Ck Cr, 1/3 mi upst confl Redwd R	Three Mile Ck at CR-67, 1 mi N Green Valley
STORET Code	S002-140	S002-152	S002-320	S003-866	S003-867	S002-311	S002-313
Count	368	374	105	96	124	208	209
Conc Ave Error	-141.1%	35.7%	89.6%	33.2%	34.6%	-7.9%	-47.9%
Conc Median Error	-8.7%	17.0%	20.6%	8.2%	7.9%	-6.5%	-14.4%
Load Ave Error	60.7%	61.4%	36.8%	-69.3%	-62.6%	150.3%	-18.3%
Load Median Error	-2.1%	0.2%	0.8%	0.4%	0.1%	-0.1%	-0.4%

(Table 12. Continued)

Site	Plum Creek At CSAH 10 Br	Sleepy Eye Cr at CSAH 8 Br, 2.2 mi N of Leavenworth	Unn Trib To Big Cobb R, 0.5 mi N Beauford	Le Sueur R at CSAH 28 In Saint Clair	Little Cobb nr CSAH-16, 6.3 mi W of Pemberton	Maple R at CSAH-18, 2 mi N of Sterling Center	Dutch Creek at 100th St, 0.5 mi W of Fairmont
STORET Code	S001-913	S001-919	S001-210	S003-448	S003-574	S004-101	S003-000
Count	193	221	201	181	250	232	202
Conc Ave Error	-993.4%	-84.9%	-22.3%	-97.4%	-223.6%	-118.1%	-367.7%
Conc Median Error	-1.6%	1.5%	-1.2%	-5.2%	-19.4%	-11.6%	6.1%
Load Ave Error	-10.4%	20.4%	102.4%	84.1%	210.4%	280.2%	23.5%
Load Median Error	0.0%	0.1%	-0.1%	-0.3%	-0.8%	-0.5%	0.1%

(Table 12. Continued)

Site	Center Creek at 315th Avenue - 1 mi S of Huntley	Sevenmile Ck dwst of MN-99, 6 mi SW of St. Peter	CD 46A dwst of CSAH-13, 6 mi SW of St. Peter	Little Cottonwood R at Apple Rd, 1.6 mi S of Courtland*	Silver Cr., CSAH-41 by East Union	Buffalo Ck, at 270th St, 1.5 mi NW of Henderson	High Island Ck at CSAH 9, 1 mi NW of Arlington
STORET Code	S003-024	S002-934	S002-936	S004-609	S000-843	S001-807	S001-891
Count	220	197	188	212	113	276	274
Conc Ave Error	-39.4%	118.0%	474.9%	35.5%	17.0%	24.6%	987.1%
Conc Median Error	-15.2%	27.7%	5.7%	-0.6%	2.3%	3.0%	131.7%
Load Ave Error	28.0%	288.3%	15.3%	-9.9%	-15.0%	-91.1%	551.2%
Load Median Error	-1.1%	3.8%	0.1%	0.0%	0.3%	0.0%	75.3%

(Table 12. Continued)

Site	Carver Ck at US-212, 2.5 mi E of Cologne	Carver Ck at Cr-140, 2.3 mi NE of Benton	Bevens Ck at 321st Ave, 3 mi SE of Hamburg	Bevens Ck at Rice Ave, 3.9 mi SE of Norwood Yng America
STORET Code	S002-489	S002-490	S002-516	S002-539
Count	165	164	116	153
Conc Ave Error	-40.1%	-98.3%	41.2%	-73.0%
Conc Median Error	-16.2%	153.4%	3.2%	-5.4%
Load Ave Error	-47.8%	499.4%	-42.9%	3.3%
Load Median Error	-4.7%	42.0%	0.5%	-0.6%

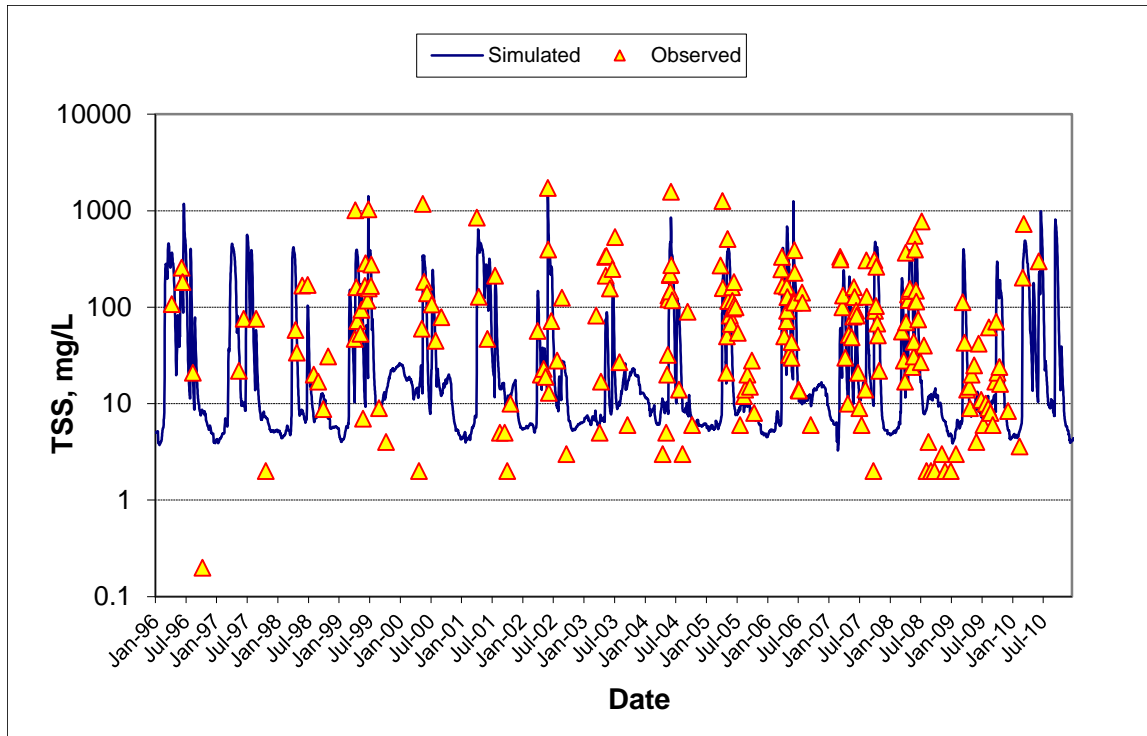


Figure 7. Timeseries Plot of Simulated and Observed TSS Concentration for Little Cottonwood River at Apple Road for 1996-2010

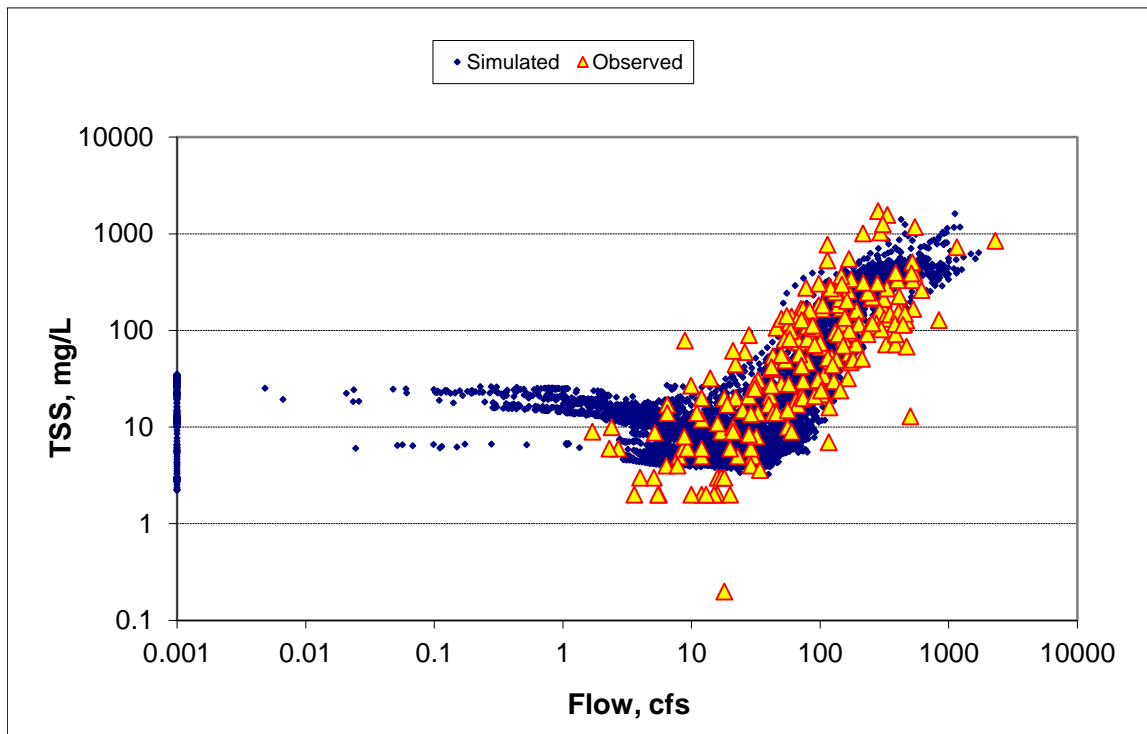


Figure 8. Concentration vs Flow Plot of Simulated and Observed TSS Concentration for Little Cottonwood River at Apple Road for 1996-2010

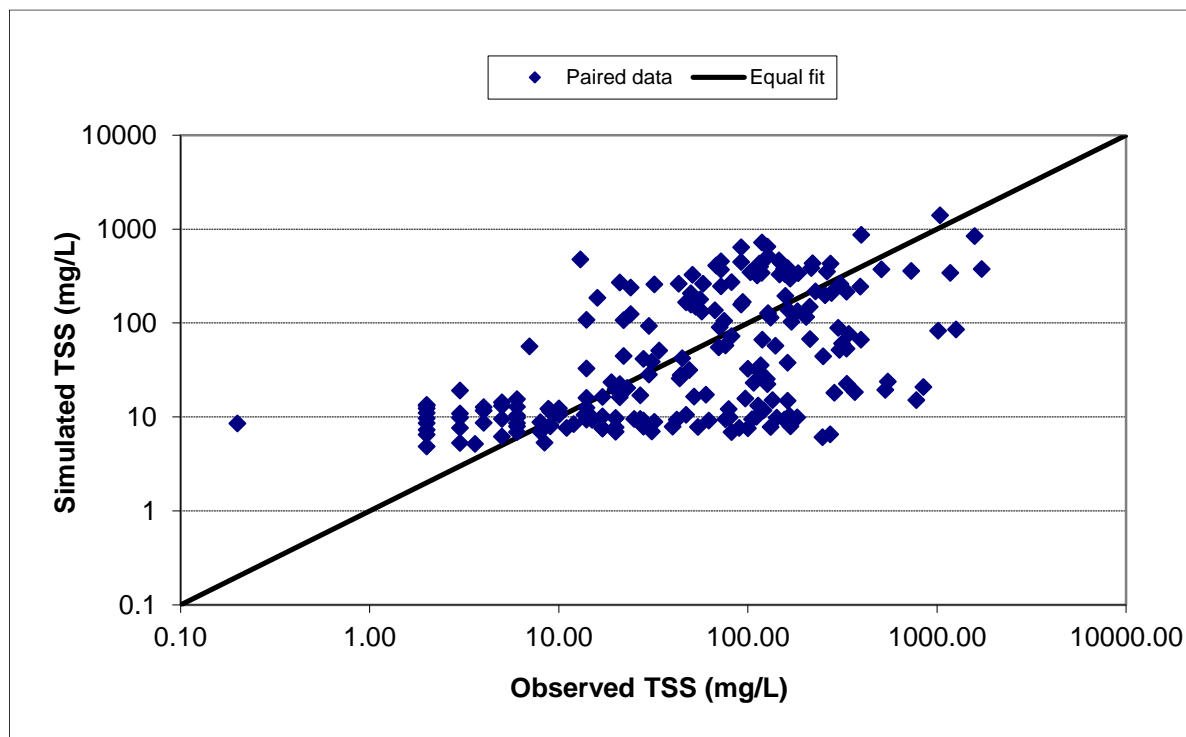


Figure 9. Simulated and Observed TSS Concentration Paired Regression Plot for Little Cottonwood River at Apple Road for 1996-2010

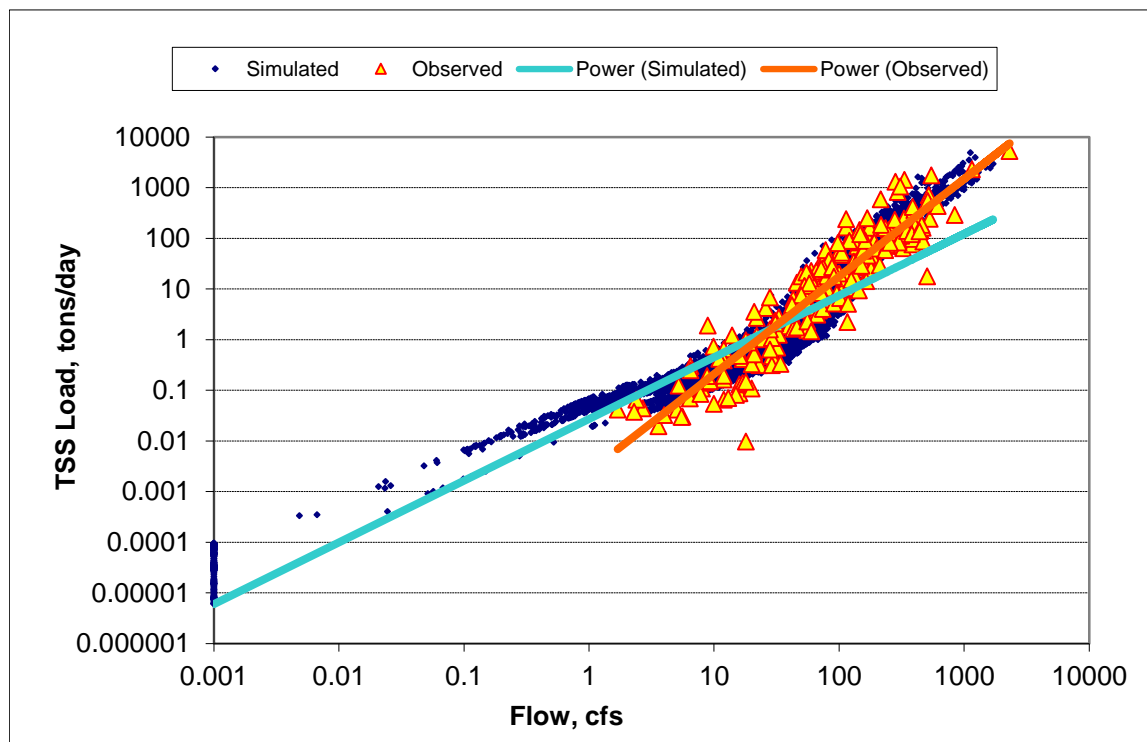


Figure 10. Load vs Flow Plot of Simulated and Observed TSS Load for Little Cottonwood River at Apple Road for 1996-2010

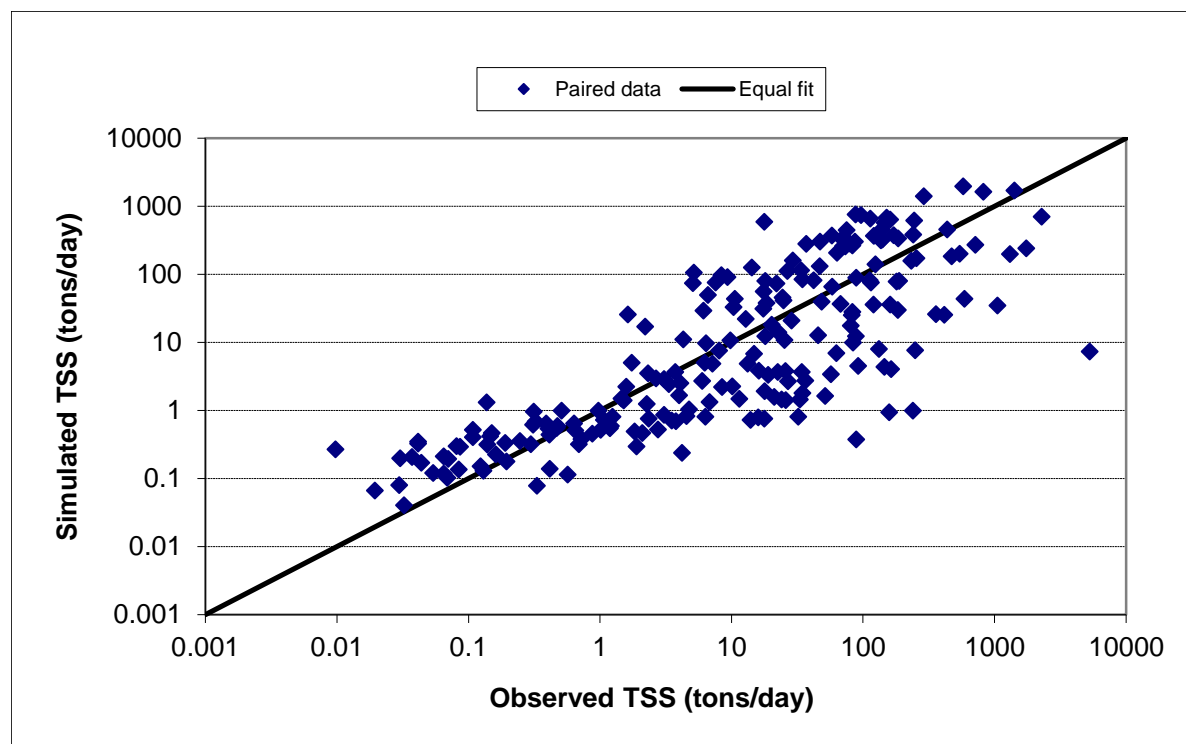


Figure 11. Simulated and Observed TSS Load Paired Regression Plot for Little Cottonwood River at Apple Road for 1996-2010

5.3 COMPARISON TO FLUX LOADS

MPCA's Watershed Pollutant Load Monitoring Network (WPLMN) is designed to obtain spatial and temporal pollutant load information from Minnesota's rivers and streams and track water quality trends. As part of this program, MPCA releases estimates of annual pollutant loads for each 8-digit hydrologic unit code basin. These "observed" monthly loads are estimated using the USACE FLUX32 program (a Windows-based update of the FLUX program developed by Walker, 1996; available at <https://www.pca.state.mn.us/water/watershed-pollutant-load-monitoring-network#flux32-8f1620f5>), and are themselves subject to significant uncertainty.

MPCA estimates at the downstream gage station on each of the HUC-8 watersheds within the Minnesota River basin are currently available for calendar years 2007 – 2011. The model and FLUX estimates are compared in Figure 12. While the fit is generally close, there are some discrepancies at individual stations during 2011 and 2012 where FLUX estimates are higher than loads produced by the model.



Figure 12. Comparison of Model and FLUX TSS Load Estimates, Calendar Years 2007 - 2011

5.4 SEDIMENT SOURCE APPORTIONMENT

Provided below are results for simulated source apportionment at the mouth of each 8-digit (HUC). Results at the mouth include the influence of upstream model(s) if one or more exist. As previously stated each model had its own unique processing workbook created and those are provided in electronic format as a supplement to this memorandum. Each electronic workbook contains source apportionment at additional locations in each watershed. Also include are the incremental or local drainage area contributions for those locations that receive influence of upstream model(s). Specifically for Le Sueur, the between stations (between upper and lower stations) source apportionment has been calculated. This allows you to see the proportion and amount of sediment generated in the nick zone area for each drainage basin. Table 13 provides the average annual sediment load and source percentage at the mouth of each model.

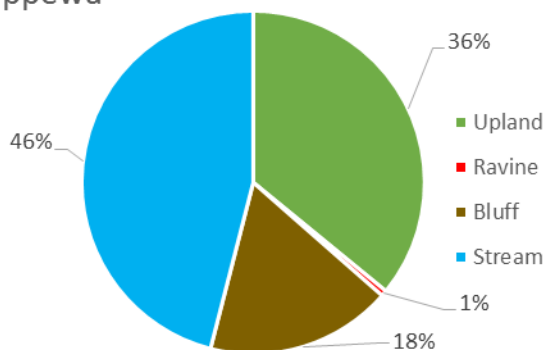
Figure 13 (in two parts) shows the source percentage as pie charts which are similar to how source apportionment was shown in the Le Sueur and Greater Blue Earth sediment budgets. The Le Sueur and greater Blue Earth produce sediment source apportionment (mass and percentage) that are consistent with the full sediment budgets, while the other basins approximately replicate the upland source fraction attribution provided in Table 1 (see Figure 13). An exact match is not expected because the model results are for 1995 – 2012, while the radiometric source data are primarily depositional sediment cores collected in 2007 and 2008 that integrate over an uncertain time period.

Also provided in Table 14 and Figure 15 is an apportionment of the annual average sediment load at the mouth of the Metro model for each HUC8 watershed contributing to that point. Note, the Lac Qui Parle is not explicitly modeled as part of the Minnesota River Basin HSPF model suite but it is represented like a point source input to the Hawk Yellow Medicine model.

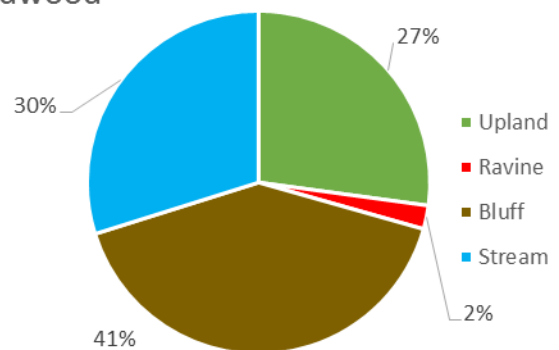
Table 13. Summary of Source Apportionment at the Mouth of each HUC8

HUC8	Metric	Upland	Ravine	Bluff	Stream	Total
Chippewa	Mass (ton/year)	4,309	66	2,107	5,518	12,000
	Source Percentage	36%	1%	18%	46%	100%
Redwood	Mass (ton/year)	11,438	937	17,180	12,572	42,127
	Source Percentage	27%	2%	41%	30%	100%
Hawk Yellow Medicine	Mass (ton/year)	71,513	2,564	64,997	67,262	206,336
	Source Percentage	35%	1%	32%	33%	100%
Cottonwood	Mass (ton/year)	31,846	1,492	75,227	50,067	158,633
	Source Percentage	20%	1%	47%	32%	100%
Watonwan	Mass (ton/year)	12,602	2,283	21,451	8,483	44,819
	Source Percentage	28%	5%	48%	19%	100%
Le Sueur	Mass (ton/year)	59,352	32,103	135,185	18,837	245,477
	Source Percentage	24%	13%	55%	8%	100%
Blue Earth	Mass (ton/year)	127,406	40,968	284,940	93,384	546,698
	Source Percentage	23%	7%	52%	17%	100%
Middle	Mass (ton/year)	289,417	48,976	482,842	297,839	1,119,074
	Source Percentage	26%	4%	43%	27%	100%
Lower/Metro	Mass (ton/year)	331,411	53,414	624,074	354,566	1,363,464
	Source Percentage	24%	4%	46%	26%	100%

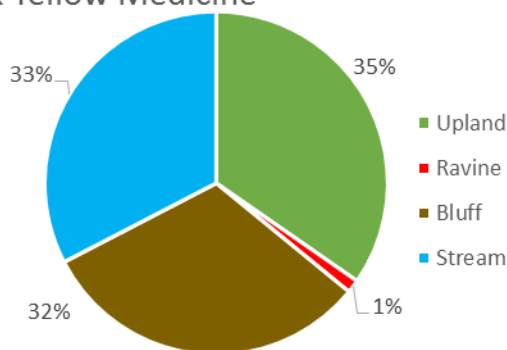
Chippewa



Redwood



Hawk Yellow Medicine



Cottonwood

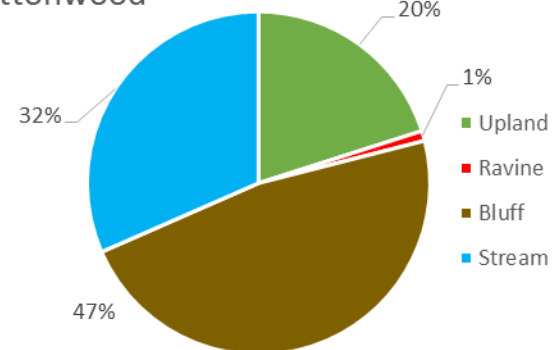
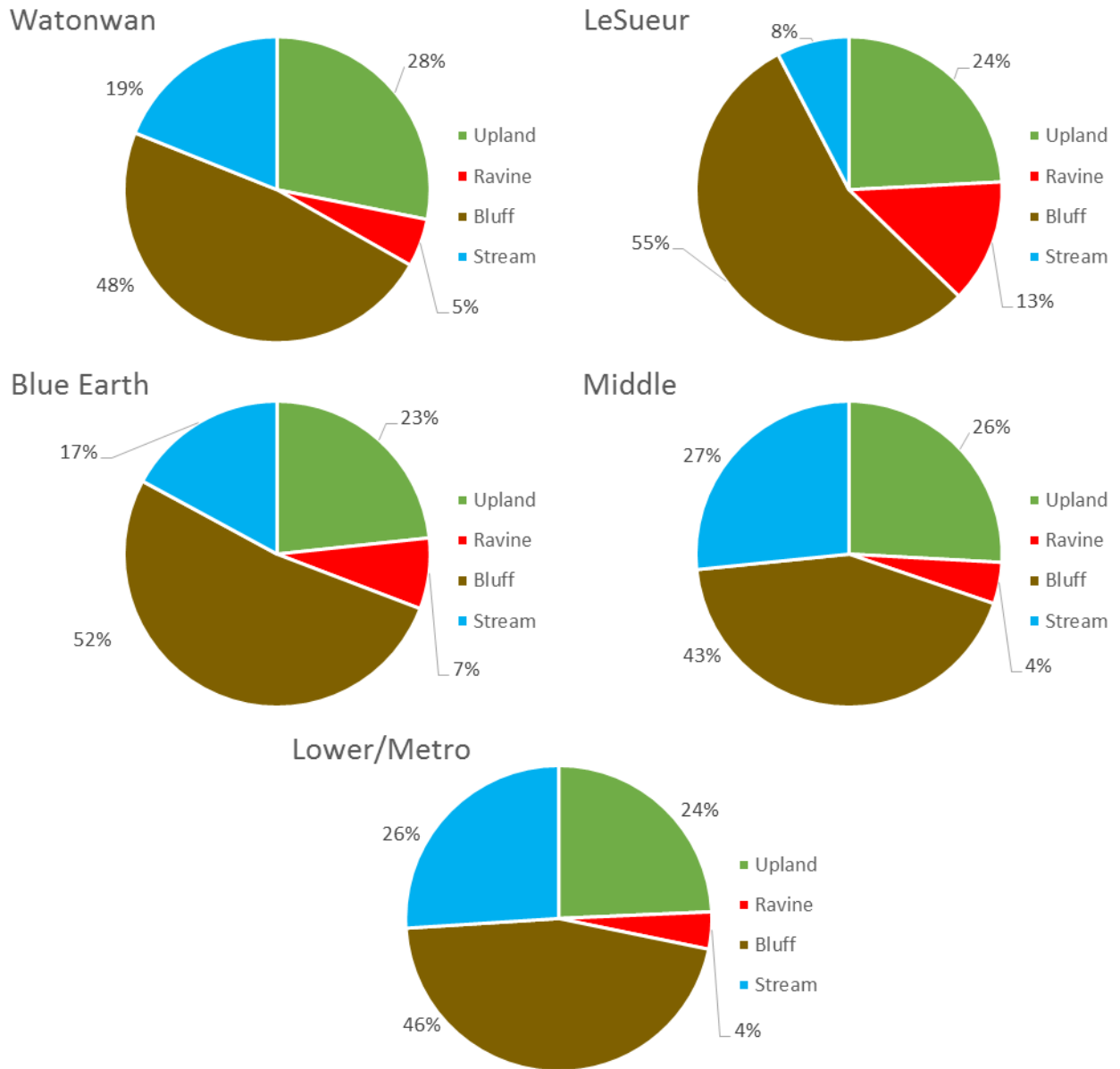


Figure 13. Instream Sediment Source Apportionment at HUC8 Outlets



(Figure 13 Continued, Instream Sediment Source Apportionment at HUC8 Outlets)

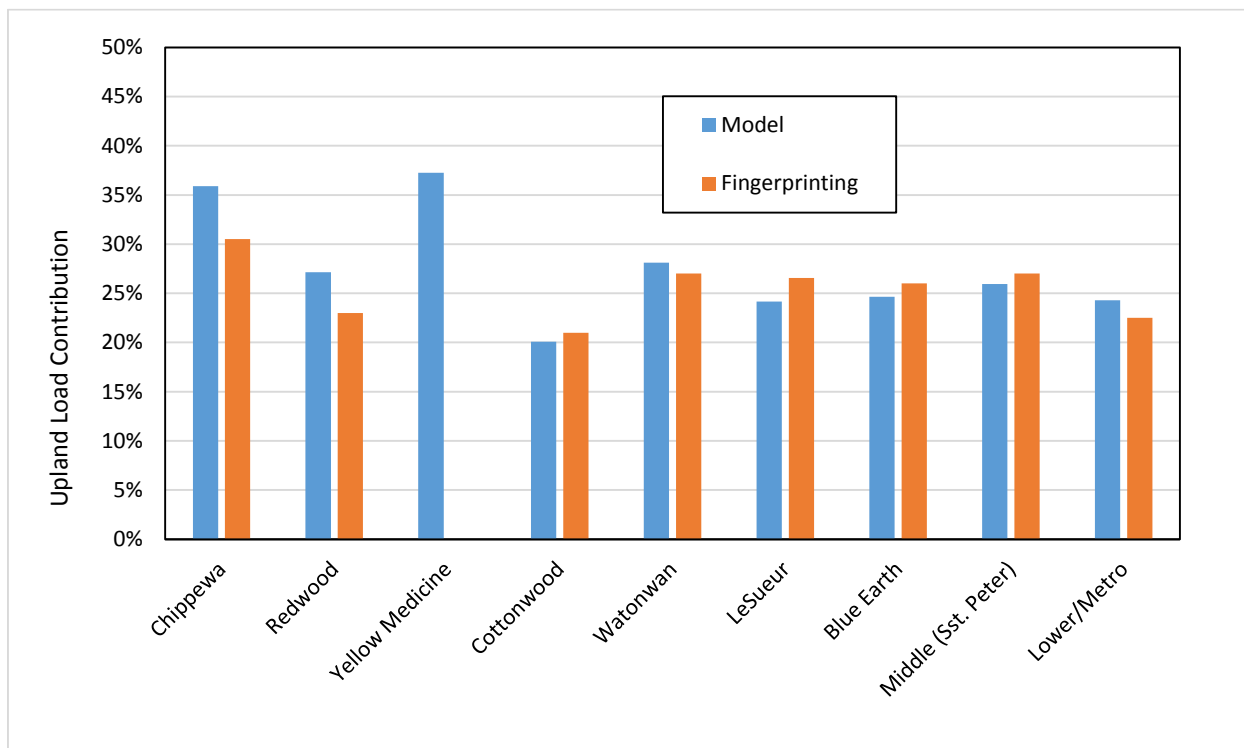


Figure 14. Comparison of Simulated Surface Washoff Loading to Surface Source Fraction from Sediment Fingerprinting Analysis

Note: Refer to Table 1 for sediment source attribution targets.

Table 14. HUC8 Contributions to Sediment Load at the Mouth of the Metro Model

Watershed	Sediment Ton/year	Percent of Total
Chippewa	12,000	0.9%
Redwood	42,127	3.1%
Hawk Yellow Medicine	104,604	7.7%
Lac Qui Parle	54,269	4.0%
Cottonwood	158,633	11.6%
Watonwan	44,819	3.3%
LeSueur	245,477	18.0%
Blue Earth	256,370	18.8%
Middle	200,776	14.7%
Lower	127,446	9.3%
Metro	116,948	8.6%
Total at Metro Mouth	1,363,464	100.0%

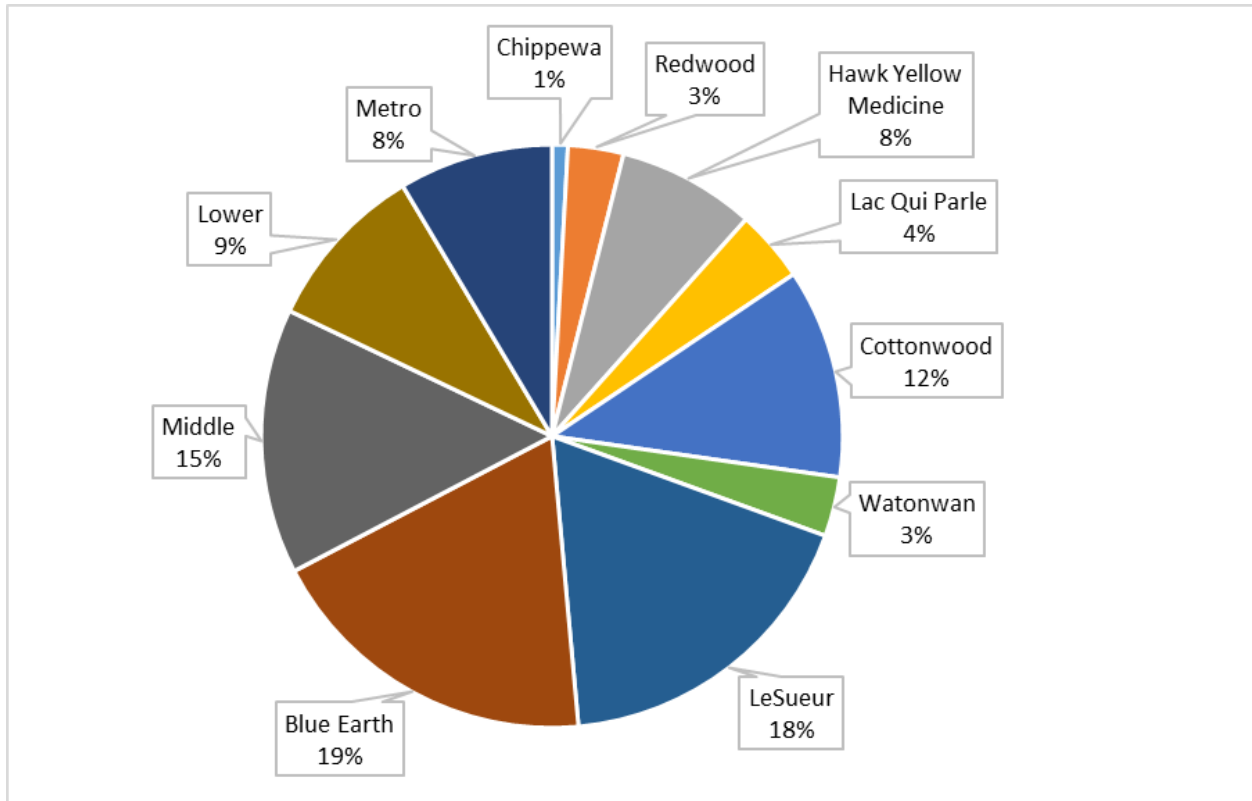


Figure 15. HUC8 Contributions to Sediment Load at the Mouth of the Metro Model

6 Summary and Potential Enhancements

The primary motivation for the sediment recalibration for the Minnesota River Basin was to better represent the source attribution information available from radiometric data and the detailed sediment source budgets for the Greater Blue Earth basin. Adjustments to the calibration to better simulate observed suspended sediment concentration data was also pursued, but under a constraint to use a relatively parsimonious parameter set that kept sediment parameters that are not based on observed soils and geological data at values that are generally constant across a basin for a given land use or waterbody type. Better fits to observed data could likely be obtained at many observation sites if more site-specific calibration with local parameter adjustments was pursued. While such an approach is likely to provide better model fit statistics it also raises the danger of over-calibration. Before taking such an approach it would be wise to consider several other factors that may be contributing to model uncertainty and potential enhancements that might improve overall model performance. Among other issues, the following items should be considered if the models are further developed:

1. **Meteorological Data:** The current model refinements make use of the meteorological time series developed by RESPEC (2014). These are based on point rainfall measurements and are often derived from volunteer daily total observations that have been disaggregated based on nearest available hourly station templates. We have seen through previous model applications that point gauges can be un-representative of the areal average precipitation depth over a model sub-basin, especially during summer convective storms, which often have local variability. The switch back to point gauge measurements appears to have resulted in a significant decline in hydrologic calibration performance in the model Chippewa basin, which has strong precipitation gradients but rather limited precipitation gauging. Further, temporal disaggregation to a template station that is some distance away can incorporate significant biases in the timing of major rainfall events, which in turn translates into apparent mismatches between model simulation and observed sediment concentrations. The newest generation of PRISM gridded precipitation products (which incorporate gage data, NEXRAD radar precipitation intensity information, and regressions against topographic characteristics) provide a potentially stronger approach to estimate the average precipitation characteristics on a reach. Downscaling to an hourly scale in the absence of nearby hourly template stations may be better achieved by using a fractal simulation approach to assign random intra-day intensities rather than assuming timing is synchronized with the template station. Potential evapotranspiration time series construction is also an issue as the energy inputs (e.g., solar radiation, dew point, wind) are often not available for rural areas and are translated from distant airport stations. The gridded NLDAS evapotranspiration estimates may provide a better means of estimation for areas far from first-order airport meteorological stations. Improvements in the representation of storm hydrology would lead directly to improvements in the simulation of sediment washoff and channel erosion during large storm events, which typically move the majority of sediment in a given year.
2. **Hydraulics:** The current models incorporate only limited information on channel hydraulics. RESPEC (2014) created much finer-scale models than the earlier Tetra Tech (2008) models. This required the development of new hydraulic functional tables (FTables), expressing the relationship between reach storage volume, outflow, surface area, and depth. These calculations in turn determine the shear stress exerted on the channel. As channel erosion has been identified as a major contributor to the total sediment load in the basin this component of the model is critical. The RESPEC memoranda say that for reaches where Tetra Tech previously calculated FTables using results of HEC-RAS models, those FTables “will be scaled by reach length and applied to corresponding reaches in order to maximize the use of the best available data.” For reaches that did not have HEC-RAS models, the documentation implies that cross-sectional measurements at USGS gage sites will be used, and, when field information on a gage is not

available, “the USGS maximum width, depth, and area data will be used to calculate cross-sections assuming a trapezoidal channel and a bank slope of 1/3.” Exact details of how FTables were developed for individual reaches are not provided. It is clear, however, that a scaling approach related to gage data can introduce problems because gage rating curves are often developed at constrictions, such as bridge crossings. Similarly, FTables derived from HEC models should be re-calculated based on new reach lengths (not scaled relative to coarser determinations) to incorporate the information available in the HEC models. Re-evaluation of HEC model output plus analysis of measured cross-sections would likely improve the hydraulic performance – and thus the channel sediment scour performance – of the models. Related to this topic, we noted that the 2014 models omit representation of Rapidan Dam on the Blue Earth River. While the pool behind Rapidan Dam is largely silted up, the dam does have an effect on hydraulics and sediment transport in the lower Blue Earth, which is a major source of sediment load to the lower Minnesota River. Therefore it should be important to incorporate the effects of this structure into the models.

3. **Ravine and Bluff Areas:** At the start of this work assignment it was anticipated that new information on the extent of ravine and bluff land use areas would be provided for each HUC8 watershed. Those coverages have not been finalized (and the current bluff coverage based on LiDAR appears to delineate features such as ditch banks as “bluffs,” which is not particularly useful to basin-scale modeling). When these delineation efforts are completed the models should be updated to incorporate the information.
4. **Parameters for Manured Land:** It required a considerable amount of time to reach an agreement with MPCA on the appropriate approach to determine the land area that received manure applications. Manure applications have impacts on nutrient loading, but also change the soil structure in somewhat subtle ways that can change runoff and sediment loading impacts. Due to the delay in resolving the manured land area representation, the definition of manured area was not finalized until after the hydrologic recalibration had been completed. To avoid disturbing the hydrologic calibration, the manure application areas were specified (and area shifted from) as equal to existing conventional tillage on A/B soils. In fact, evidence (summarized in Tetra Tech, 2008) suggests that land receiving manure application should have somewhat greater upper zone storage capacity (UZSN), which in turn affects runoff sediment transport capacity. This refinement should be incorporated into any revised models.
5. **Tile Drain Sediment:** RESPEC (2014) adopted a modified approach to the simulation of sediment transport through surface tile inlets that was much simpler and more efficient than the SPECIAL ACTIONS approach implemented by Tetra Tech (2008). The revised approach gives a similar estimate of total sediment load transported by this pathway, but the pollutograph is very different, with the load transmitted to the stream much more quickly. At this point it is not clear which representation is correct, although the approach earlier use by Tetra Tech did result in a good match between observed and simulated sediment concentrations. This topic appears worthy of further investigation.

7 References

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MEMORANDUM

To: Chuck Regan (MPCA)

Date: January 3, 2019

Cc: Jon Butcher, Jennifer Olson
(Tetra Tech)

Subject: Cottonwood and Redwood
Watersheds HSPF Model
Extension

From: Michelle Schmidt, Scott Job, and
Ryan Birkemeier (Tetra Tech)

1.0 INTRODUCTION

Two Hydrologic Simulation Program – FORTRAN (HSPF) models of the Cottonwood and Redwood watersheds in the Minnesota River Basin were refined and calibrated for hydrology and water quality by RESPEC (2012; 2014a; 2014b) and recalibrated by Tetra Tech (2015; 2016). HUC8 scale HSPF models have also been developed and calibrated for the other watersheds in the Minnesota River Basin. The Minnesota Pollution Control Agency (MPCA) is facilitating the effort to keep the Minnesota River Basin models up-to-date for various planning and management efforts, such as stressor identification, water quality implementation planning, and wastewater permit development. In addition, it is advantageous to keep the simulation periods of the HSPF models current to utilize recently collected monitoring data. Therefore, several of the Minnesota River Basin HSPF models (Minnesota River Headwaters, Lac qui Parle, Cottonwood, Redwood, Pomme de Terre, Le Sueur, Watonwan, and Blue Earth) are being extended through 2017. This memorandum documents updates to the HSPF models for the Cottonwood and Redwood watersheds.



Figure 1. Minnesota River Basin HSPF Model Domains

1.0 MODEL EXTENSION

The approaches used to extend the input time series for the Cottonwood and Redwood HSPF models through 2017 are discussed in the following subsections. As discussed in Section 1.1, the meteorological input series from the original models were derived from ground weather station data; these were replaced with hourly inputs for the full simulation period derived from gridded weather data sources. The point source discharge and pollutant load time series (Section 1.2) and wet and dry atmospheric deposition time series (Section 1.3) were also extended through 2017. Lastly, the hydrology calibration was reviewed following these updates for the period of 1995 – 2012. A few coarse updates were made to the parameterization following the review, and recommendations for future fine-tuning were identified.

1.1 METEOROLOGY

Weather forcing series for the original versions of the HSPF models were derived from ground weather station data. Gridded weather products, however, better represent climatic variations across a diverse landscape compared to point-in-space station weather data. Moreover, the gridded weather data products directly provide hourly air temperature, wind, and solar radiation data as well as parameters for computing cloud cover, dew point temperature, and potential evapotranspiration, which are inputs to HSPF.

PRISM (Parameter-elevation Relationships on Independent Slopes Model) provides annual, monthly, and daily gridded precipitation data for the conterminous United States (Daly et al., 2008, 2015; daily output was added to PRISM in 2015). PRISM calculates a climate-elevation regression function for each grid cell and the regression is used to distribute station-based precipitation data to the grid cell.

Approximately 13,000 precipitation stations are used in the analysis. For each grid cell, precipitation stations are assigned weights based on location, elevation, coastal proximity, topographic facet orientation, vertical atmospheric layer, topographic position, and orographic effectiveness of the terrain; the stations are then entered into the regression function to establish the gridded precipitation product.

Another gridded product is the North American Land Data Assimilation System (NLDAS-2) meteorological time-series (Mitchell et al., 2004). NLDAS-2 (<http://ldas.gsfc.nasa.gov/nldas/NLDAS2forcing.php>) provides continuous hourly data from 1979 to present on a 1/8-degree grid that has been processed to fill gaps. The precipitation data in NLDAS-2 are based on interpolation of daily gauge precipitation including orographic adjustments based on PRISM and temporally disaggregated using Doppler radar and satellite data. NLDAS-2 also provides solar radiation, wind at 10 m (which can be scaled to wind at 2 m), and absolute humidity plus air pressure, from which dew point can be calculated. Cloud cover (which is only needed to estimate long wave radiation exchange with the atmosphere) is not included in the NLDAS output, but can be back-calculated from the ratio of estimated incident solar radiation to cloud free solar radiation during daylight hours using the regression relationship developed by Davis (1996).

Meteorological data from both PRISM and NLDAS were used to develop hourly weather forcing series for the full simulation period for both models. The basic overview of each meteorological input, data source, and processing notes are provided in Table 1 and discussed in more detail in the following sections. Python scripts developed by Tetra Tech were used to download, extract, and process PRISM and NLDAS data for the grids intersecting the watershed. Data from the grids were processed and aggregated by weather zone.

Table 1. Summary of HSPF Meteorological Input Time Series

HSPF Model Input	Description (units)	Parameter Source	Base Data Series Number (DSN)	Processing Notes
PREC	Precipitation (in)	PPT (PRISM), APCP (NLDAS)	100	Daily PRISM precipitation data are disaggregated using the random cascade method
ATEM	Air Temperature (°F)	TMP (NLDAS)	200	Hourly air temperature, used directly
SOLR	Solar Radiation (Ly)	DSWRF (NLDAS)	500	Hourly short wave radiation, used directly
CLOU	Cloud Cover (tenths; 0-10)	DSWRF (NLDAS)	400	Inferred from hourly short wave radiation at 2 meters, and estimated cloudless-sky short wave radiation
DEWP	Dew Point Temperature (°F)	SPFH, PRES, TMP (NLDAS)	300	Function of hourly specific humidity, air pressure, and air temperature
WIND	Wind Travel (mi)	UGRD, VRGD (NLDAS)	600	Net wind travel from component vectors
PEVT	Potential Evapotranspiration (in)	DSWRF, TMP, WIND, SPFH, PRES (NLDAS)	700	Computed from solar radiation, air temperature, wind travel, and dew point temperature

1.1.1 Precipitation

PRISM has been shown to better represent precipitation than WorldClim and Daymet, which are other publicly available gridded meteorological products (Daly et al., 2008). Because of this PRISM was used to generate precipitation (PREC) series for the HSPF model. Daily precipitation series for grid cells aligning with the drainage area were retrieved from the PRISM database using Python scripts.

The HSPF model requires hourly precipitation, but direct observations of hourly precipitation are not available through PRISM. We used a statistical approach to develop estimates of hourly precipitation. Specifically, daily precipitation records for each of the model weather zones were disaggregated to an hourly time step using the random multiplicative cascade model, based on fractal theory. A Python code to implement the random multiplicative cascade method is available as AMBHAS rain_disagg.py at (https://github.com/neel9102/ambhas/blob/master/ambhas/rain_disagg.py). This method distributes mass of the initial time interval successively over regular subdivisions as a fractal process (usually subdivided by factors of two). The initial time scale rainfall depth is multiplied by a cascade generator at each subdivision (multiplied by more cascade generators as further subdivisions occur). The distribution of the

scaling generator(s) determine the scaling properties of the rainfall. Therefore, the main goal in the random cascade is to determine the distribution of the cascade generator. As explained in Kumar et al. (2009), this method first aggregates the provided time series by a factor of two, up to five times, to generate the moments, varying from zero to five. For example, the provided daily rainfall time series is aggregated in series to a two, four, eight, sixteen, and thirty two-day time step. Sample moments are defined as:

$$M_n(q) = \sum_{i=1}^{b^n} \mu_n^q(\Delta_n^i)$$

Here q is the moment order, the i^{th} interval after n level of subdivision is shown as Δ_n^i ($i=1, \dots, b^n$ intervals at level n).

The slope of the scaling relationship is called the Mandelbrot-Kahane-Peyriere (MKP) function (Mandelbrot, 1974; Kahane and Peyriere, 1976), calculated as:

$$X_b(q) = 1 - q + \log_b E(W^q)$$

The MKP contains information about the cascade generator (W) and, therefore, contains information about the scaling properties of the rainfall.

The slope of the sample moment is defined as:

$$\tau(q) = \lim_{\lambda_n \rightarrow 0} \frac{\log M_n(q)}{-\log \lambda_n}$$

Here λ_n is the dimensionless spatial scale defined as $\lambda_n = b^{-n}$.

$\tau(q)$ is used to approximate $X_b(q)$, and thus the distribution of a cascade generator can be determined by fitting τ as a function of sample moments, and then using the probability density function of that distribution. The cascade generator is then able to get an hourly timestep rainfall from a daily timestep rainfall.

The mass in “subcube” Δ_n^i (or i^{th} interval in the n^{th} subdivision) is defined as:

$$\mu_n(\Delta_n^i) = R_0 \lambda_n \prod_{j=1}^n W_j(i)$$

Where R_0 is the initial rainfall depth at level $n=0$.

The fractal approach produces realistic sub-daily precipitation patterns, but does not guarantee that estimated peak rainfall is matched in time with actual rainfall. This can create discrepancies between observed and simulated rainfall-runoff processes; however, a similar problem is also present when disaggregating daily total rainfall based on patterns observed outside the watershed.

1.1.2 Air Temperature

NLDAS directly provides estimation of hourly air temperature (TMP) at 2 meters above the surface. NLDAS reports temperatures in Kelvin and data retrieved for the HSPF model were converted to degrees Fahrenheit. The hourly temperature series are used to define daily minimum (TMIN) and maximum (TMAX) temperatures to support subsequent calculations.

1.1.3 Solar Radiation

NLDAS directly provides estimation of hourly shortwave solar radiation (DSWRF) at 2 meters above the surface (W/m^2) corrected for atmospheric conditions. The solar radiation data were converted to HSPF compatible units (Langleys).

1.1.4 Wind

NLDAS provides estimation of directional hourly wind speeds (m/s) at 10 meters above land surface as northing and easting vector components (UGRD and VGRD), which are used to compute total wind travel distance for the hour ($\sqrt{UGRD^2 + VGRD^2}$). The 10-meter wind travel is scaled to 2 meters above the ground using a wind speed power law:

$$W_{2-meters} = \left(\frac{z}{z_a}\right)^r \times W_{10-meters}, 0 \leq z \leq z_a$$

where, $W_{10-meters}$ is the wind travel at 10 meters above the ground in m/s, $\frac{z}{z_a}$ is an elevation ratio (0.2), r is a surface roughness exponent (0.143 for agricultural land with some houses, shrubs, and plants) and $W_{2-meters}$ is wind travel at 2 meters above the ground in m. Wind travel is then converted to miles for HSPF.

1.1.5 Cloud Cover

Cloud cover is not reported by NLDAS; however, it can be back-calculated during daylight hours from the relationship of Davis (1996) describing the ratio of ambient solar radiation at the surface (E_{surf}) to radiation from a cloudless sky ($E_{cloudless}$):

$$\frac{E_{surf}}{E_{cloudless}} = 1 - 0.6740 C^{2.854}$$

where, C is the fractional cloud cover and E_{surf} is obtained from NLDAS. $E_{cloudless}$ is a function of latitude and time of year and is calculated using an approach from Baig et al. (1991). HSPF requires cloud cover inputs to be specified as tenths, ranging from 0 to 10.

Baig et al. (1991) use a Gaussian distribution centered at solar noon, or local time $t = 12:00$ to estimate the fraction of daily solar radiation at different times of day as r_t . Their model is similar to that of Jain (1984), but with an additional correction factor.

$$r_t = \frac{1}{2\sigma\sqrt{2\pi}} \left\{ \exp\left(-\frac{(t-12)^2}{2\sigma^2}\right) + \cos\left(180^\circ \frac{(t-12)}{(S_0-1)}\right) \right\}$$

S_0 is the length of day in hours which is obtained from two standard NOAA equations, which are similarly implemented in the QUAL2Kw model code:

$$\delta = 23.45 * \sin\left(\frac{360^\circ(n+284)}{365}\right)$$

$$S_0 = \frac{2}{15} \arccos(-\tan(\phi) \tan(\delta))$$

Here, δ is the declination angle, n is day of year ($n=1$ for Jan 1), and ϕ is latitude. Note that for calculation purposes, 180° , 360° , and ϕ and δ in $\tan(\phi)\tan(\delta)$ should be converted to radians and the output from arccos should be converted to degrees.

σ is the standard deviation of the Gaussian distribution consistent with the day length pattern and is shown by Baig et al. (1991) to be equal to:

$$\sigma = \frac{1}{r_{t=12}\sqrt{2\pi}}$$

Baig et al. (1991) do note that the slight and occasional misfit between experimental data and theoretical values in their work can be improved if one uses data averaged over many years instead of single day data. With this in mind, the calculation of σ was done for each individual day over the period of record and then averaged per day of year to capture longer term averages while maintaining seasonal differences. The “experimental” or observed data used to obtain $r_{t=12}$ and subsequently σ was NLDAS data at daily and disaggregated to hourly timescales.

Once r_t is calculated for each hour of the entire period of interest, those fractions are applied to a daily time series of cloudless solar radiation using the methods to calculate $(E_{surf}/E_{cloudless})$, which is then used to calculate cloud cover via Davis (1996) above.

1.1.6 Dew Point Temperature

NLDAS does not provide dew point temperature, but does provide specific humidity, air temperature, and air pressure, which can be used to estimate dew point temperature. Dew point temperature was calculated following the approach presented in Chapter 4 (Water Vapor) in Stull, R., 2017: *Practical Meteorology: An Algebra-based Survey of Atmospheric Science -version 1.02b*. Univ. of British Columbia. This book is freely available online under a Creative Commons license at https://www.eoas.ubc.ca/books/Practical_Meteorology/. The Stull, R., 2017 method was applied to derive dew point temperature for the full simulation period:

First, the mixing ratio (r) is calculated from specific humidity (q ; unitless):

$$r = \frac{q}{(1 - q)}$$

Because specific humidity becomes extremely low under cold, dry conditions it is important to maintain full precision in this calculation. Then actual vapor pressure (e) is derived from atmospheric pressure (P ; in KPa):

$$e = \frac{r}{(0.622 + r)}P$$

Dew point temperature (D ; Kelvin) is then calculated with an assumed reference vapor pressure ($e_o = 0.6113$; kPa):

$$D = \frac{1}{\left(\frac{1}{273.15} - 0.0001844\right) \ln\left(\frac{e}{e_o}\right)}$$

Lastly, dew point temperature is converted to degrees Fahrenheit for HSPF. In general dew point temperature cannot exceed air temperature, except during transient supersaturated conditions; therefore, the dew point temperature is set equal to the air temperature when the calculated dew point temperature

is higher than the air temperature, which is a reasonable approximation for use in a watershed model that doesn't explicitly consider fog.

1.1.7 Potential Evapotranspiration (PET)

NLDAS provides an estimate of potential evapotranspiration (as PEVAP) calculated by the modified Penman method of Mahrt and Ek (1984). However, this is not a focus of NLDAS because NLDAS is designed to run a variety of Land Surface Models (LSMs; such as the NOAH model), most of which generate their own energy-based ET estimates. PEVAP is provided only because one of the LSMs (SAC-SMA, the Sacramento soil moisture accounting model) does require it as an input (<http://ldas.gsfc.nasa.gov/nldas/NLDAS2forcing.php>; accessed 9/2/2015). On investigation it turns out that the PEVAP that NLDAS reports is the PEVAP calculated by the North American Regional Reanalysis (NARR) dataset (Mesinger, et al., 2006). NARR is documented to have a large positive bias in the estimation of shortwave radiation (Xia, et al., 2012). NLDAS corrects the NARR shortwave radiation estimates using satellite-based estimates, but the PEVAP estimate ported from NARR is not corrected. In addition, NARR is at a coarser spatial scale than NLDAS and the PET estimates may be off in areas with strong edge effects.

Sensitivity analyses conducted by Tetra Tech in other Minnesota HSPF models concluded that the NLDAS/NARR reported PEVAP values were unreasonably high in some areas (due to the shortwave radiation bias) and exhibited too great a variation from the coastline to the interior (in part this is likely due to the downscaling of coarser-grid NARR data). Further, the PEVAP time series provided by NLDAS did not match the seasonal pattern of Penman Pan ET calculated at individual weather stations.

Based on these observations it is desirable to recalculate PET, rather than using the PEVAP reported by NLDAS/NARR. Therefore, Penman Pan PET was calculated for each model weather zone using inputs from NLDAS (including the corrected shortwave radiation) and applying the standard approach from BASINS that has been implemented in most other Minnesota HSPF models.

The PET time series requires dew point temperature as an input variable and because an alternative method was used to estimate dew point temperature for the full simulation period, PET was also updated for the full simulation period.

1.2 POINT SOURCES

Permitted point sources are present in the Cottonwood River and Redwood River watersheds and all were represented in the existing HSPF model (RESPEC 2012; 2014a; 2014b). A variety of municipal and industrial sources discharge to surface waters in the two watersheds (Table 2). All of the municipal dischargers are considered minor point sources, except for Marshall WWTP. ADM Corn Processing is an industrial facility, but its discharge is process wastewater and is assumed to behave like a Class A WWTP facility.

Inputs to the model include flow, heat content, and loads for DO, CBOD_u, nitrate, ammonia, refractory organic N, orthophosphate, refractory organic P, and sediment. Time series inputs to the model are represented on a daily basis, and conversion factors/statements are used within the model to convert daily rates to hourly rates, which match the model time-step.

To perform the time extension, point source data through 2017 were needed. MPCA provided data for Minnesota facilities from three different sources – a monthly Tempo database generally covering 1998

through 2017, a daily Tempo database generally beginning sometime in 2013 and ending in 2017, and the OnBase system to cover the remaining daily time period of 2012 - 2013.

In many cases, monitoring data were not available at a particular facility for a given parameter. This was frequently the case for nitrate and ammonia, and no data were available allowing for the calculation or estimation of refractory organic N and refractory organic P. When this occurred, a representative concentration was assumed. MPCA has developed a series of recommended surrogate values (Table 3), primarily from Weiss (2012), Helgen (1992), and a summary of wastewater effluent data provided in spreadsheet form by Dr. Ronald Jacobson (MPCA; provided in support of the 2002 updates to the Minnesota River models). Using the surrogate values requires knowing (or assuming) the type of facility. MPCA provided updated facility type information for Minnesota, which is shown in Table 2. The model input file was configured to calculate the product of the point source flow time series and the representative concentration (with appropriate conversion factor) to input pollutant load. The model was already configured this way prior to this time extension project. However, a review of the concentration assumptions in the original model found that in many cases the wrong facility type was assumed (likely due to facility type information not being available at the time of model development). When this occurred, the model input file was updated to reflect the revised concentration assumption.

As stated previously, a combination of daily and monthly point source monitoring data were available to specify the daily input time series to the models for the extension period, 2012 – 2017. Nearly all facilities had some months with complete daily flow records, and other months with only monthly flow volumes. This was the case for both continuous discharging facilities and intermittent discharging facilities (namely stabilization ponds). When daily flow data were available in a given calendar month, they were used directly in the model input time series. When daily flow data were not available, the monthly reported total flow volume was used, and distributed equally throughout the month (by dividing by the number of days in the month). Similarly, daily pollutant concentrations (and temperatures where monitored) were used when available; otherwise reported monthly average values were used. The product of flow and concentration was then used to calculate daily loads, with appropriate conversion factors.

Heat input time series were calculated in the original model using a daily varying water temperature obtained from a facility in the Sauk River Watershed, adjusted for differences between the Sauk and the Minnesota River (RESPEC, 2014a). Lacking recent monitoring data from the facility and details regarding the temperature adjustment, we instead calculated a mean monthly characteristic water temperature from the original model time series from 1995 – 2012 using temperature back-calculated from the BTU loads in the time series. We then used the product of flow and corresponding monthly temperature to calculate BTU load for the time extension period.

The HSPF model represents a single form of carbonaceous biochemical oxygen demand (CBOD), which should correspond to the CBOD that decays over a representative residence time within a reach. This means that a long-term or ultimate value of CBOD (CBOD_u) should be used, and both models were already configured with CBOD_u as the time series input. The point source monitoring data, however, report only 5-day CBOD (CBOD₅). BOD decay factors impact the ratio of CBOD_u to CBOD₅, which is important because almost all available data for BOD is in the form of CBOD₅ (at 20°C). Literature in this area suggests that a decay factor of 0.2 1/day is appropriate for treated effluent at 20 degrees Celsius, yielding a ratio of 1.58 (Table 6.5 in Thomann and Mueller, 1987). The use of the ratio of 1.58 is justified in the literature. Jayawardena (2014) states that 0.1 – 0.3 are typical decay rates for effluent that has gone through primary and secondary treatment. Lung (2001) states that 0.2 1/day is an appropriate value for BOD decay for wastewater effluent following secondary treatment, as does Sullivan et al. (2010). CBOD₅ point source data was multiplied by this ratio prior to entry in the updated (2013 – 2017) model

input time series. However, no changes were made to the CBODu time series prior to 2013. The ratio used in the original models to convert CBOD5 to CBODu is not documented in RESPEC 2014a, but comments in the model input file suggest that a ratio of 2.54 was used (corresponding to an assumed decay rate of 0.1 1/day).

HSPF considers both labile and refractory forms of organic nutrients. The refractory (non-decaying) portions are represented as separate state variables, but the labile portions are “hidden” with CBODu based on stoichiometric ratios for organic matter. The labile portions must be accounted for before calculating the refractory organic nutrient loads, which are model inputs. Refractory organic N is calculated as follows:

$$\text{Refractory Organic N} = \max \{ \text{Organic N} - \text{CVON} \times \text{CBODu}, 0 \}$$

where CVON is the assumed mass of labile organic N per mass of CBODu (equal to 0.052938 using default HSPF assumptions). A unique refractory organic N concentration was calculated for each facility using a) surrogate organic N concentrations by facility type from Table 3, and b) the mean of the monthly CBOD5 concentration reported in the Tempo database from 1999 – 2017, multiplied by the CBODu/CBOD5 ratio of 1.58. The refractory organic N concentrations were then used with a multiplier on the flow time series in the model input file to calculate load.

TP is reported by all the facilities in Cottonwood and Redwood, and orthophosphate is assumed to be 0.723 x TP (based on the MPCA default assumption). Organic P is assumed to be the remaining 0.277 of TP. Refractory organic P is calculated as follows:

$$\text{Refractory Organic P} = \max \{ 0.277 \times \text{Total P} - \text{CVOP} \times \text{CBODu}, 0 \}$$

where CVOP is the assumed mass of labile organic P per mass of CBODu (equal to 0.007326 using default HSPF assumptions). A unique refractory organic P concentration was calculated for each facility using a) the mean of the monthly TP concentration reported in the Tempo database from 1999 – 2017, multiplied by 0.277, and b) the mean of the monthly CBOD5 concentration reported in the Tempo database from 1999 – 2017, multiplied by the CBODu/CBOD5 ratio of 1.58. The refractory organic P concentrations were then used with a multiplier on the flow time series in the model input file to calculate load.

Two issues with the original point source time series were identified while performing the time extension update. First, we learned that the City of Storden operated a continuously discharging mechanical WWTP until October 2004, then a controlled discharge stabilization pond WWTP beginning in November 2004 through present. Prior to November 2004, daily influent flow was used as a proxy for effluent flow in the model point source time series. However, the change to operations was not accounted for, and thus daily influent flow was used through 2012 in the original model (rather than sporadic outflow from the stabilization pond). As a result, the model flow time series was updated to reflect the change in 2004 from continuous to occasional outflow per the point source monitoring data (note that heat is the only other model input time series used for Storden, and we updated it per the procedure discussed previously). Second, we determined that all the heat time series used in the original models were calculated incorrectly. The formula for BTU load (relative to freezing) is as follows:

$$\text{Flow (MGD)} \times [\text{Temperature (}^{\circ}\text{F)} - 32] \times 1.27 \times 10^{-7} \text{ (BTU/lb}^{\circ}\text{F)} = \text{BTU (1/day)}$$

The original calculations failed to subtract 32 from the water temperature, resulting in BTU loads corresponding to water temperatures in the high 80°F to low 90°F range, rather than high 50°F to low 60°F range. We corrected all the heat model input time series for all the facilities for the entire period of record.

Table 2. Summary of Point Sources

Watershed	Facility Name	Permit ID	Facility Type	Average Flow (MG/year)
Cottonwood River	ACME Brick Great Lakes Plant	MN0061646	NCCW	41.3
	August Schell Brewing Co	MN0022284	NCCW	5.4
	Balaton WWTP	MN0020559	Class D	32.3
	Clements WWTP	MNG580094	Class D	4.2
	Del Monte Foods Inc - Sleepy Eye Plant 114 (SD001)	MN0001171	NCCW	49.9
	Del Monte Foods Inc - Sleepy Eye Plant 114 (SD006)	MN0001171	NCCW	2.4
	Garvin WWTP	MNG580101	Class D	5.0
	Lamberton WWTP	MNG580100	Class D	33.8
	Lucan WWTP	MNG580112	Class D	5.6
	Revere WWTP	MNG580114	Class D	3.3
	Sanborn WWTP	MNG580115	Class D	9.8
	Sleepy Eye WWTP	MNG580041	Class D	155.2
	Springfield WWTP	MN0024953	Class B	124.4
	Storden WWTP	MNG580106	Class D	8.1
	Tracy WWTP (SD001)	MN0021725	Class D	36.8
	Tracy WWTP (SD002)	MN0021725	Class D	38.4
	Wabasso WWTP	MN0025151	Class C	27.1
	Walnut Grove WWTP	MN0021776	Class B	39.4
	Wanda WWTP	MNG580126	Class D	9.2
Westbrook WWTP	MNG580127	Class D	33.5	

Watershed	Facility Name	Permit ID	Facility Type	Average Flow (MG/year)
Redwood River	ADM Corn Processing - Marshall	MN0057037	Class A	501.6
	Ghent WWTP	MNG580121	Class D	7.7
	Lynd WWTP	MNG580030	Class D	8.2
	Marshall WWTP	MN0022179	Class A	955.2
	Milroy WWTP	MNG580124	Class D	5.0
	Russell WWTP	MNG580062	Class D	19.3
	Ruthton WWTP	MNG580105	Class D	18.1
	Tyler WWTP	MNG580116	Class D	47.5
	Vesta WWTP	MNG580043	Class D	6.0

Facility type descriptions: Class A – municipal, large mechanical, Class B – municipal, medium mechanical, Class C – municipal, small mechanical/pond mix; Class D – municipal, mostly small ponds, NCCW – non-contact cooling water.

Table 3. Surrogate assumptions by facility type (mg/L)

Discharge Type	CBOD5	DO	NO ₃ -N	NH ₄ -N	Org-N
Class A municipal - large mechanical	3	5	15	3	1
Class B municipal - medium mechanical	12	5	10	4	3
Class C municipal- small mechanical/pond mix	6	5	7	1	2
Class D municipal - mostly small ponds	6	5	3	1	2
Non-contact cooling	0.5	7	1	2	1

1.3 ATMOSPHERIC DEPOSITION

The original Cottonwood and Redwood watersheds HSPF models included wet and dry deposition of ammonia-N and nitrate-N to pervious surfaces, impervious surfaces, and water bodies that were extended through 2017. Wet deposition concentrations of ammonia and nitrate N (as mg-N/L) from seasonal data recorded at NADP station MN27 (Lamberton), which is located southeast of the modeled watersheds, were applied for the extension period. Dry deposition rates of ammonia and nitrate N (as

lb/ac) were taken from CASTNET monitoring. There are not CASTNET stations within or particularly close to the watersheds studied here, so data from the Perkinstown, WI (PRK134) station were applied. Reported data were converted from molar units to mass or mass-based concentration as nitrogen to generate the input time series. The entire time series for both wet and dry deposition of ammonia and nitrate N were updated and replaced (i.e., beginning in 1995), for a number of reasons. An examination of wet deposition values in the original model revealed that source monitoring stations changed during the modeling time period (i.e., the same station was not used from 1995 – 2012). For dry deposition, it appeared that the previous time series did not include the molar conversion to nitrogen mass. In addition, all the historic dry deposition values changed somewhat, likely due to advances in the modeling used to estimate dry deposition flux.

In addition to the extension and replacement of the wet and dry deposition series for N species, representation of both dry and wet deposition of phosphorus to surface water were maintained in the model. These are represented as constant monthly values through the MONTH-DATA block. The values were interpolated from Twaroski et al. (2007); for both Cottonwood and Redwood, the values were 0.27 kg/ha/yr for PO₄ dry deposition flux and 0.024 mg/L for PO₄ wet deposition concentration. Atmospheric deposition of phosphorus to the uplands is not included because it is assumed to be implicit in the sediment potency representation of pervious land loading and the buildup/washoff representation of impervious land loading of phosphorus.

2.0 HYDROLOGY PERFORMANCE REVIEW

The hydrology calibration was reviewed following the updates to the Cottonwood and Redwood HSPF models. The performance was evaluated based on relative flow volume error (assessed for annual, high, low, and seasonal flows), daily and monthly Nash-Sutcliffe Efficiency, and visual plots comparing simulated and observed flows (e.g., scatterplots of simulated versus observed monthly flow volumes). The updates to the meteorological time series (i.e., converting from time series derived from station-based data to time series derived from gridded weather data) did not significantly alter the performance of the models described in the previous hydrology recalibration report (Tetra Tech, 2015). However, a few coarse revisions to the hydrology parameters were implemented following the updates to the input time series. These adjustments included refining potential evapotranspiration factors, baseflow evapotranspiration, snow catch factors, infiltration rates, and upper soil zone nominal storage parameters.

Summary metrics are provided for the updated models in Table 4 and Table 5 and for the models prior to the updates following the 2015 hydrology recalibration in Table 6 and Table 7 (Tetra Tech, 2015). Errors in total streamflow volume were reduced at most sites in both watersheds following the input time series and parameter updates. The fraction of annual precipitation that evaporates or transpires remained about the same as the previous iterations of the models, about 79% for Cottonwood and 80% for Redwood. However, the representation of the 50% lowest flows were generally not improved and tend to be overestimated by the Cottonwood model; low flows tend to occur in the late fall and early winter when precipitation is often in the form of snow. Future recalibration efforts for both models should switch the snow accumulation and melt method from the degree-day method to the full energy balance method as recommended by MPCA and then the snow simulation should be recalibrated using gridded snow depth and/or snow water equivalent data. Daily and monthly NSEs were also improved at most tributary sites in the Cottonwood and Redwood watersheds. NSEs weren't improved at the most downstream gage in the Cottonwood watershed, although total, low and high flow volume errors were consistently reduced at that location (Cottonwood River near New Ulm).

Table 4. Summary Metrics for the Cottonwood HSPF Model Hydrology Performance, 1996-2012

Site	HSPF Reach	Error in Total Volume (%)	Error in 50% Low Flows (%)	Error in 10% High Flows (%)	Daily NSE	Monthly NSE
Plum Creek near Walnut Grove, CSAH10 (MN29048001)	189	-0.07	57.0	-10.5	0.808	0.858
Cottonwood River near Lamberton, US14 (MN29062002)	230	-10.6	34.4	-13.5	0.801	0.881
Cottonwood River near Springfield, CR2 (MN29015001)	330	5.03	42.0	2.61	0.833	0.821
Cottonwood River near Leavenworth, CR8 (MN29022001)	370	3.11	41.9	-3.55	0.857	0.875
Sleepy Eye Creek near Cobden, CR8 (MN29011001)	407	2.04	81.1	-9.93	0.825	0.874
Cottonwood River near New Ulm, MN (MN29001001)	490	-0.97	-3.19	-5.25	0.766	0.860

Table 5. Summary Metrics for the Redwood HSPF Model Hydrology Performance, 1996-2012

Site	HSPF Reach	Error in Total Volume (%)	Error in 50% Low Flows (%)	Error in 10% High Flows (%)	Daily NSE	Monthly NSE
Redwood River at Russell, CR15 (MN27043001)	190	-1.74	20.9	-10.9	0.802	0.863
Redwood River near Marshall, MN (MN27043002)	210	-2.36	-24.8	-3.77	0.801	0.880
Threemile Creek near Green Valley, CR67 (MN27039001)	313	8.81	10.1	-2.52	0.690	0.753
Clear Creek near Seaforth, CR56 (MN27030001)	443	-2.78	24.4	-11.7	0.791	0.836
Redwood River near Redwood Falls, MN (MN27035001)	450	3.98	-9.63	5.36	0.769	0.863

Table 6. Summary Metrics for the Cottonwood HSPF Model Hydrology Performance – Previously Recalibrated Model, 1996-2012 (Tetra Tech, 2015)

Site	HSPF Reach	Error in Total Volume (%)	Error in 50% Low Flows (%)	Error in 10% High Flows (%)	Daily NSE	Monthly NSE
Plum Creek near Walnut Grove, CSAH10 (MN29048001)	189	3.79	86.1	-9.11	0.866	0.904
Cottonwood River near Lamberton, US14 (MN29062002)	230	-15.9	45.7	-18.1	0.719	0.848
Cottonwood River near Springfield, CR2 (MN29015001)	330	-0.39	42.1	0.38	0.752	0.671
Cottonwood River near Leavenworth, CR8 (MN29022001)	370	-7.34	38.6	-11.4	0.839	0.838
Sleepy Eye Creek near Cobden, CR8 (MN29011001)	407	-8.41	58.9	-14.5	0.757	0.788
Cottonwood River near New Ulm, MN (MN29001001)	490	-4.15	7.77	-7.76	0.815	0.888

Table 7. Summary Metrics for the Redwood HSPF Model Hydrology Performance – Previously Recalibrated Model, 1996-2012 (Tetra Tech, 2015)

Site	HSPF Reach	Error in Total Volume (%)	Error in 50% Low Flows (%)	Error in 10% High Flows (%)	Daily NSE	Monthly NSE
Redwood River at Russell, CR15 (MN27043001)	190	-5.99	7.54	-10.0	0.714	0.851
Redwood River near Marshall, MN (MN27043002)	210	-4.19	-8.45	-5.96	0.772	0.876
Threemile Creek near Green Valley, CR67 (MN27039001)	313	5.56	28.3	-6.41	0.533	0.664
Clear Creek near Seaforth, CR56 (MN27030001)	443	-9.86	8.16	-9.39	0.623	0.568
Redwood River near Redwood Falls, MN (MN27035001)	450	1.75	9.63	-0.89	0.789	0.860

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Appendix E – CAFO List and Watershed Summary

Table E- 1. List of CAFOs by HUC-10 subwatershed in the Cottonwood River Watershed.

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
Headwaters – Cottonwood River	083-50002	973	N
	083-50003	1440	N
	083-50015	300	N
	083-60847	140	N
	083-62344	400	N
	083-62428	473.5	N
	083-62444	650	N
	083-62543	285	N
	083-62553	693	N
	083-62704	57.8	N
	083-62734	150	N
	083-62825	1080	N
	083-62848	602.5	Y
	083-62856	490	N
	083-62862	386	N
	083-62863	300	N
	083-62926	999	N
	083-62928	660	N
	083-63509	138	N
	083-63783	169	N
	083-65527	297.5	N
	083-80220	980	N
	083-83840	711	N
	083-89079	600	N
	083-98301	1248	N
	083-100060	600	N
	083-104800	210	N
	083-105640	66	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	083-109880	2700	N
	083-113093	980	N
	083-113278	720	N
	083-119803	820	N
	083-121082	720	N
	083-121083	60	N
	083-124355	600	N
	083-125550	299	N
Meadow Creek	083-50012	700	N
	083-50014	840	N
	083-50024	1248	N
	083-60844	500	N
	083-61769	88	N
	083-61770	540	Y
	083-61803	373	N
	083-62112	177	N
	083-62170	500	N
	083-62425	395	N
	083-62427	500	N
	083-62441	165	N
	083-62541	210	Y
	083-62542	210	Y
	083-62563	525	N
	083-62691	200	N
	083-62709	720	N
	083-62737	238.6	N
	083-62842	880	N
	083-65081	397	N
	083-68166	485	N
	083-87104	4500	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	083-106440	72	N
	083-111440	285	N
	083-121434	202.5	N
	083-121438	190	N
	083-125701	720	
	083-125800	1440	
	083-125999	720	
	083-126540	720	N
Plum Creek	083-50007	2520	
	101-68937	590	N
	101-68950	54	N
	101-77051	50	N
	101-77080	270	N
	101-77154	160.2	N
	101-77185	74	N
	101-77400	231	N
	101-88975	171	N
	101-88981	660	N
	101-88985	120	N
	101-88990	133	N
	101-89012	132	Y
	101-89021	420	N
	101-89037	340	N
	101-107508	85	N
	101-107847	110	N
	101-107848	30	Y
	101-107849	56	N
	101-107853	75.9	N
	101-119167	150	N
	101-121921	200	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	101-126420	720	N
	127-50083	240	N
	127-50084	845	N
	127-50085	620	N
	127-62486	95	N
	127-62506	60	N
	127-62745	158	N
	127-62750	222	N
	127-63074	999	N
	127-63123	84	N
	127-63790	268	N
	127-105560	390	N
	127-114503	97.5	N
Pell Creek – Cottonwood River	033-97854	23.5	Y
	033-97989	60	N
	083-50010	20	Y
	083-50011	48	Y
	083-50029	1200	N
	083-50030	750	N
	083-62706	195	N
	083-62836	20.6	Y
	083-63796	50	N
	083-65618	71	N
	083-119884	1440	N
	101-107850	1470.5	N
	127-50031	888.5	N
	127-50056	295	N
	127-50061	698.4	N
	127-50063	1728	Y
	127-50066	166	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	127-50080	632.5	N
	127-50097	90	N
	127-60086	95	N
	127-62328	141	N
	127-62472	180	N
	127-62507	321.5	N
	127-62694	350	N
	127-62954	154	N
	127-62959	62	N
	127-62969	162	N
	127-65083	346	N
	127-65084	142.5	N
	127-65520	270	N
	127-80028	131	N
	127-80102	1200	N
	127-98160	990	N
	127-99980	936	N
	127-105720	600	N
	127-117681	735	N
	127-125907	375	
Dutch Charley Creek	033-50001	1177	N
	033-50006	4480	Y
	033-60187	1715	N
	033-97860	720	N
	033-97879	265	N
	033-97881	845	N
	033-97882	210	N
	033-97908	600	N
	033-97910	291	Y
	033-97912	80	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	033-97914	200	N
	033-97915	140	N
	033-97918	82	N
	033-97919	80	N
	033-97929	139	N
	033-97935	60	N
	033-97938	60	N
	033-97939	135	N
	033-97940	90	N
	033-97965	42	Y
	033-97970	150	N
	033-97974	980	N
	033-97976	220	N
	033-97978	122.765	N
	033-97981	290.5	N
	033-97992	139.25	N
	033-97993	150	N
	033-97997	990	N
	033-97999	150	N
	033-98002	38	Y
	033-98005	280	N
	033-98032	705	N
	033-98033	570	N
	033-98035	310.5	N
	033-98047	183	N
	033-98061	89	N
	033-98063	150	N
	033-98065	84	N
	033-98078	150	N
	033-98080	150	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	033-98081	990	N
	033-98088	200	N
	033-98095	588	N
	033-98102	141	N
	033-98107	90	N
	033-102342	990	N
	033-102566	250.3	N
	033-102577	530	N
	033-103543	60	N
	033-103552	960	N
	033-104200	1342.5	
	033-104201	990	N
	033-107458	56	N
	033-108225	250	N
	033-108322	120	N
	033-110360	1342.5	N
	033-117658	930	N
	033-120691	750	N
	033-125533	60	N
	033-125751	1290	N
	033-125896	360	N
	033-126396	720	
	101-50005	2126.4	
	101-68939	50	Y
	101-77068	399	N
	101-77069	119	N
	101-77135	120	N
	101-77141	16.3	Y
	101-77169	95	N
	101-77170	53.5	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	101-77388	180	N
	101-77389	100	N
	101-88997	50	N
	101-89033	193	Y
	101-108062	128	N
	101-108064	325	N
	101-108066	16	Y
	101-108076	60	
	101-114832	480	N
	127-50034	180.7	N
	127-62710	110	N
	127-122138	100	N
Mound Creek – Cottonwood River	015-50005	1872	N
	015-71652	33	Y
	015-71655	450	N
	015-71671	1125	N
	015-71702	497.4	Y
	015-71716	350	N
	015-71727	2936.3	N
	015-71740	171	N
	015-71744	160	N
	015-71757	120	N
	015-71787	90	N
	015-71794	195	N
	015-71810	195	N
	015-71824	192.5	N
	015-71856	285	N
	015-71872	160	N
	015-71876	78	N
	015-71889	90	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	015-71921	295	N
	015-71933	590	N
	015-71966	125.5	N
	015-72003	216	N
	015-72024	115	N
	015-72032	160	N
	015-72035	182	Y
	015-72041	900	N
	015-72075	624	N
	015-72094	91	N
	015-72098	735	N
	015-72107	900	N
	015-72127	163	N
	015-72138	225	N
	015-72147	400	N
	015-72162	990	N
	015-72168	242	N
	015-72171	55	Y
	015-72178	110	N
	015-72200	325	N
	015-72204	300	N
	015-72210	138.07	Y
	015-72217	112	Y
	015-72218	180	Y
	015-72223	315	N
	015-72233	50	N
	015-72244	840	N
	015-72246	90	Y
	015-72273	992	N
	015-72285	96.12	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	015-72315	213.6	N
	015-72317	500	N
	015-72324	50	N
	015-72328	1106	
	015-72332	160	N
	015-80242	258	N
	015-82445	85	N
	015-82469	102	Y
	015-82477	300	N
	015-93741	360	N
	015-95050	144	N
	015-95133	84	Y
	015-95136	125	N
	015-95141	300	N
	015-95145	565.5	Y
	015-95148	1106	
	015-105820	900	N
	015-105961	900	N
	015-107460	1600	N
	015-107461	295	N
	015-108312	620	N
	015-109414	810	N
	015-115876	595	N
	015-117075	421	N
	015-119172	250	Y
	015-125529	900	
	015-126342	748.5	N
	015-127146	270	N
	015-127195	990	N
	033-50011	1682	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	033-97856	480	N
	033-97885	73.126	N
	033-97894	100	N
	033-97909	210	N
	033-97922	94	N
	033-97925	56	N
	033-97926	60	N
	033-97932	217	N
	033-97933	789	N
	033-97934	60.3	N
	033-97944	72	N
	033-97948	250	N
	033-97952	343.5	N
	033-97954	265.4	N
	033-97959	211	N
	033-97962	133	N
	033-97968	950	N
	033-97975	180	N
	033-97998	300	N
	033-98016	900	N
	033-98024	55.725	N
	033-98025	209	N
	033-98038	450	N
	033-98048	482.5	N
	033-98051	61.4	N
	033-98068	780	N
	033-98069	75	N
	033-98076	930	N
	033-98089	117	N
	033-98098	998.9	Y

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	033-98099	900	N
	033-98103	999	N
	033-103542	50	N
	033-103546	240	N
	033-103548	500	N
	033-105840	900	N
	033-108226	57.7	N
	033-110813	600	N
	033-112558	900	N
	033-121655	84	Y
	127-50079	128	N
	127-62535	78.53	N
	127-62536	102	N
	127-63134	225	N
	127-98660	900	N
	127-111220	750	N
	127-125865	720	
	127-126355	990	N
Sleepy Eye Creek	015-50009	2092	N
	015-50013	1200	N
	015-60703	1640	N
	015-71726	900	N
	015-71769	390	N
	015-71982	325	N
	015-72159	315	N
	015-72207	290	N
	015-72278	65.3	N
	015-82450	70	N
	015-82459	608	N
	015-82459	608	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	015-82460	750	N
	015-82476	750	N
	015-82840	612	N
	015-125789	744	N
	015-126350	30.66	Y
	127-50001	576	N
	127-50009	120	N
	127-50010	77	N
	127-50014	427	N
	127-50023	150	N
	127-50027	1420	N
	127-50029	500	N
	127-50032	600	N
	127-50033	54.08	N
	127-50036	198	N
	127-50042	902.5	N
	127-50046	499	N
	127-50047	912.5	N
	127-50049	80	N
	127-50051	1872	N
	127-50058	553	N
	127-50059	420.1	N
	127-50060	52	N
	127-50074	290	N
	127-50086	173.5	N
	127-60040	110.4	N
	127-60085	120.5	N
	127-60520	104	N
	127-60564	57.5	N
	127-60848	350	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	127-61729	177.5	N
	127-61738	660	N
	127-61742	180	N
	127-61761	54	N
	127-62182	97.5	N
	127-62466	200	N
	127-62475	226.5	N
	127-62523	92.5	N
	127-62695	480	N
	127-62697	165	N
	127-62699	390	N
	127-62872	272.8	N
	127-62875	14.4	Y
	127-62886	312.5	N
	127-62891	150	N
	127-62899	50	N
	127-62904	268	N
	127-63122	480	N
	127-63124	83	N
	127-63151	87.5	N
	127-63155	60	N
	127-63190	96.7	N
	127-63529	299	N
	127-63758	401.4	N
	127-63781	515	N
	127-64986	90	N
	127-65613	135	N
	127-65616	660	N
	127-101040	624	N
	127-105900	900	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	127-106300	936	N
	127-106840	177.1	N
	127-107260	760	N
	127-109480	270	N
	127-109820	432	N
	127-110620	936	N
	127-112698	360	N
	127-120771	720	N
	127-124541	1440	N
	127-125564	840	N
	127-125590	744	N
	127-125731	720	N
	127-126807	133.9	N
	127-127020	990	N
Cottonwood River	015-50002	1575	N
	015-50008	1200	
	015-71647	600	N
	015-71650	93.5	Y
	015-71654	153	N
	015-71673	70.6	N
	015-71675	624	N
	015-71678	41	Y
	015-71698	78.1	N
	015-71703	495.5	N
	015-71720	306	N
	015-71737	125	N
	015-71745	59.5	N
	015-71816	120	N
	015-71852	97.9	Y
	015-71853	17	Y

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	015-71857	295	N
	015-71866	101.5	N
	015-71880	68.6	N
	015-71890	147	N
	015-71892	36	Y
	015-71905	311.8	Y
	015-71919	510	N
	015-71948	108	N
	015-71949	129.6	N
	015-71964	50	Y
	015-71968	70	N
	015-71973	57.425	N
	015-71987	98.2	N
	015-71999	60	N
	015-72029	194	N
	015-72049	108	N
	015-72059	465	N
	015-72066	163.9	N
	015-72068	80	N
	015-72074	645	N
	015-72139	1690	N
	015-72155	294	N
	015-72165	832	N
	015-72175	60	N
	015-72197	247.9	Y
	015-72226	61.075	N
	015-72236	75	N
	015-72238	675	N
	015-72282	75	N
	015-72283	60	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	015-72304	50.05	N
	015-72331	149	N
	015-72336	10.2	Y
	015-72353	95	N
	015-72357	81	N
	015-72369	128.6	N
	015-72375	196	N
	015-72395	62	N
	015-95056	318.5	N
	015-95134	72	Y
	015-95138	22.8	Y
	015-95147	247.1	N
	015-100000	1440	N
	015-107462	1200	N
	015-107843	170	N
	015-107846	123	N
	015-109481	936	N
	015-115641	80	N
	015-120278	97	N
	015-126352	102	N
	015-126800	100	N
	015--126427	85	N
	127-50088	2053	N
	127-50092	180	N
	127-50093	576	N
	127-60702	70	N
	127-61745	350	N
	127-61762	1895	
	127-62180	330	N
	127-63144	735	N

HUC10 Watershed	Reg Number	Animal Unit (AU) Count	Within Shoreland
	127-65511	660	N
	127-112251	800	N
	127-112801	720	N
	127-117156	945	N
	127-124992	412	

Table E- 2. Cottonwood River Watershed CAFO Summary.

General	
Total Feedlots	513
Total Permitted CAFO's	64
Total Animal Units (AUs)	228,065
Primary Animal Type ¹	Swine (53%)
	Cattle (45%)
Sensitive Areas	
Open Lot Feedlots	322
Feedlots in Shoreland	46
Open Lot Feedlots in Shoreland	37

¹Percentages are based on animal units.